

# A Data-Driven, Physics-Informed Approach Towards *Predictive Turbulence Modeling*

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# Acknowledgment of Collaborators

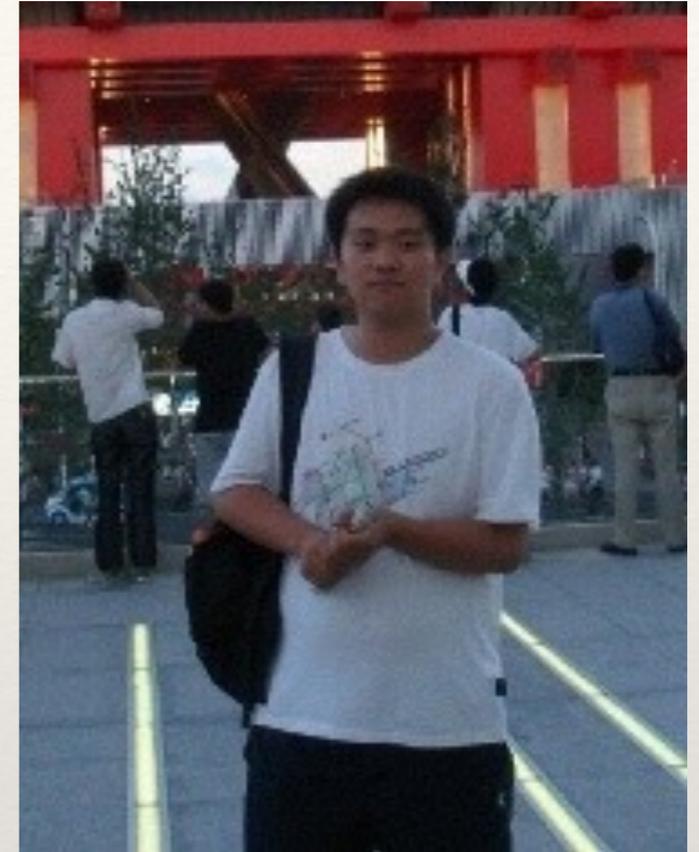
- ❖ My graduate students:



Jianxun Wang



Jinlong Wu



Rui Sun

- ❖ Colleague & collaborator: Chris J. Roy (Virginia Tech)

# Publications Related to This Talk

- [1]. H. Xiao, J.-L. Wu, J.-X. Wang, R. Sun, and C. J. Roy. Quantifying and reducing model-form uncertainties in Reynolds averaged Navier-Stokes equations: An open-box, physics-based, Bayesian approach. Submitted to JCP, 2015. Also available at [arxiv:1508.06315](https://arxiv.org/abs/1508.06315)
- [2]. J.-X. Wang, J.-L. Wu, and H. Xiao. Incorporating prior knowledge for quantifying and reducing model-form uncertainty in RANS simulations. Submitted to IJUQ, 2015. Also available at [arxiv:1512.01750](https://arxiv.org/abs/1512.01750)
- [3]. J.-L. Wu, J.-X. Wang, and H. Xiao. A Bayesian calibration-prediction method for reducing model-form uncertainties with application in RANS simulations. *Flow, Turbulence and Combustion*, 2016. In press. DOI: 10.1007/s10494-016-9725-6  
Also available at [arxiv: 1510.06040](https://arxiv.org/abs/1510.06040)
- [4]. H. Xiao, J. X. Wang and R. G. Gahnem. A Random Matrix Approach for Quantifying Model-Form Uncertainties in Turbulence Modeling. Submitted to CMAME, 2016. Available at [arxiv:1603.09656](https://arxiv.org/abs/1603.09656)
- [5]. J. X. Wang, R. Sun, H. Xiao. Quantification of Uncertainty in RANS Models: A Comparison of Physics-Based and Random Matrix Theoretic Approaches. Submitted, 2016. Available at [arxiv:1603.05549](https://arxiv.org/abs/1603.05549)
- [6]. J.-L. Wu, J.-X. Wang, and H. Xiao. Quantifying Model Form Uncertainty in RANS Simulation of Wing–Body Junction Flow. Submitted to FTC.

# RANS as Work-Horse Tool in CFD

- ❖ Turbulence are everywhere in natural and industrial flows (see examples below).
- ❖ RANS (Reynolds Averaged Navier-Stokes) models are still the work-horse tool in practical applications, because high-fidelity methods (LES and DNS) are still too expensive for practical flows.



# Landscape of Turbulence Modeling

- ❖ Standard (one/two eqn) RANS models: k-e, k-w, SA
- ❖ Advanced turbulence model: RSTM, EARSM
- ❖ Hybrid LES/RANS: DES and its variants, PANS, among others
- ❖ Wall-modeled LES (WALEs)
- ❖ Fully resolved LES or DNS

The drawback of RANS: poor performance in flows with *separation, mean pressure gradient, mean flow curvature*. Need to quantify the uncertainties in the RANS predictions for high-consequence applications (e.g., nuclear power plants or airplanes).

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  - ❖ Fully resolved LES or DNS
- The drawback of RANS is that it is not accurate for flows with *separation, mean curvature*. Need to quantify the accuracy of RANS predictions for complex flows (e.g., nuclear power plants or airplanes).

**ETH**

Eidgenössische Technische Hochschule Zürich  
Swiss Federal Institute of Technology Zurich

## A Consistent Hybrid LES/RANS Framework with High-Order LES Solver on Cartesian Mesh

Heng Xiao\* and Patrick Jenny

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\*Currently at: Department of Aerospace & Ocean  
Engineering, Virginia Tech, Blacksburg, VA

The 34th NIA CFD Seminar May 20th, 2013

# Landscape of RANS Model Uncertainty

- ❖ Parametric and Bayesian model averaging approaches [Oliver & Moser et al.; Edling, Cinnella & Dwight]

## Nonparametric Approaches.

### with uncertainties injected in:

- ❖ RANS predicted turbulent viscosity [Dow and Wang]
- ❖ Source terms discrepancy in turbulent transport equations, e.g.,  $\nu_t$  in SA model,  $\omega$  in k- $\omega$  model [Duraismy et al.]
- ❖ RANS predicted Reynolds stresses [Oliver & Moser]
- ❖ Decomposed RANS-predicted Reynolds stresses: TKE, anisotropy, orientation. [Emory, Gorle, Iaccarino et al.]
- ❖ Dynamics (time derivatives) of Reynolds stresses (Mishra & Girimaji): preliminary studies.

# RANS Model Uncertainty: Black-Box vs. Openbox

- ❖ **Kennedy & O'Hagan approach:** introduce a discrepancy term to the QoI (e.g., drag and lift), and then calibrate the discrepancy with data => **band-aid approach**.
- ❖ Drawback: **black-box, physics-neutral**, not an efficient use of data; difficult to incorporate prior knowledge.
- ❖ Most of the methods discussed in this talk (except for the parametric approaches) are open-box, physics informed.

# Parametric/Model Averaging Approaches

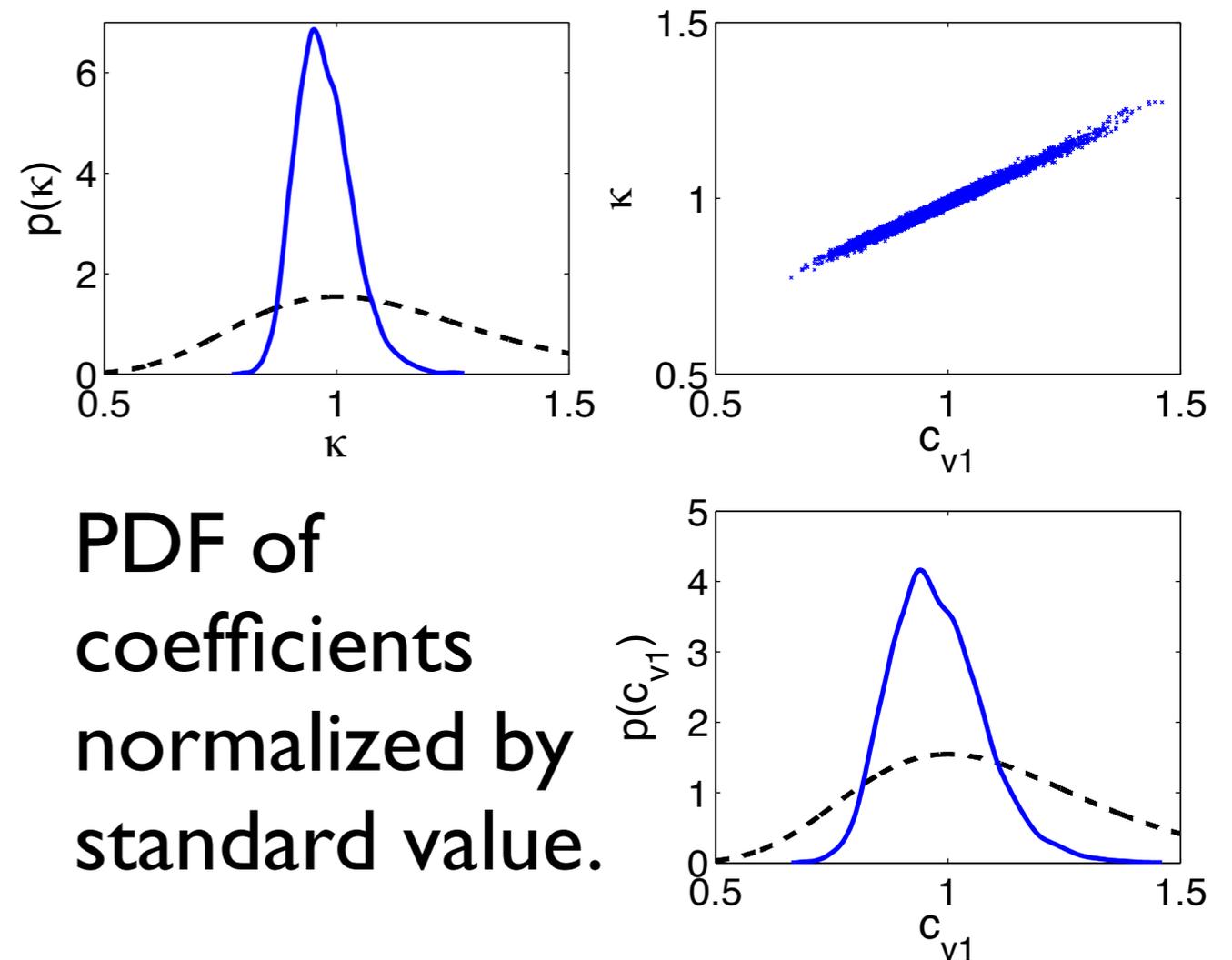
Simply stated: given experimental data, Bayesian inference methods are used to infer:

- ❖ How likely is each model (e.g., SA, Chien, v2f) correct?
- ❖ For a given model, what are the possible values/likelihood of the coefficients?

# Bayesian Inference with Data

**Table 2.**  $\log(E)$  value for each model.

	BL	SA	Chien	$v^2-f$
IND	44.19	8.862	21.78	20.23
SE	41.71	8.045	19.94	40.45
VLSE	159.5	164.0	175.5	169.8
ARSM	135.0	169.0	157.5	158.9

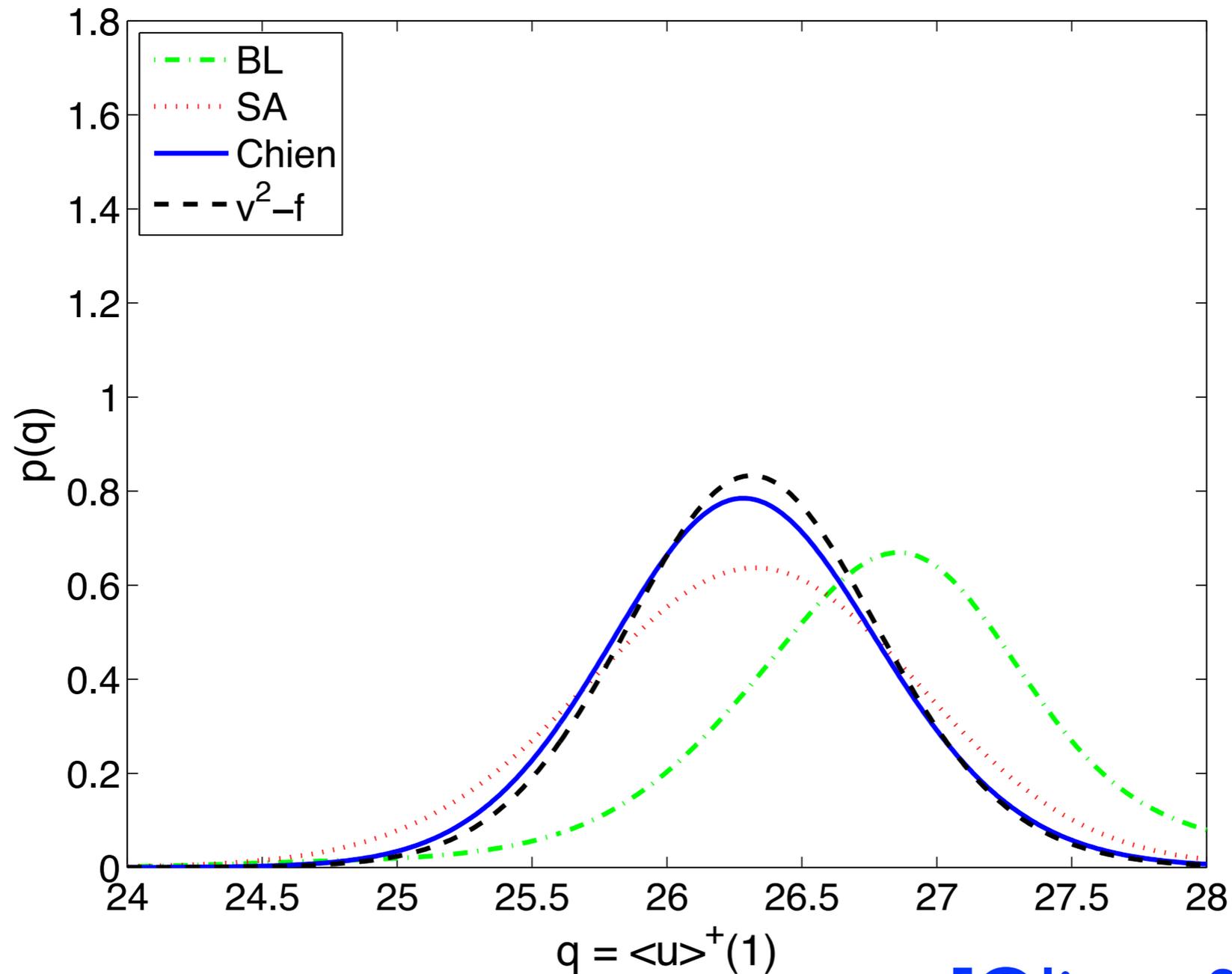


(a) SA:  $\kappa$  and  $c_{v1}$

[Oliver & Moser]

# Prediction with Posterior of Models/Coefficients

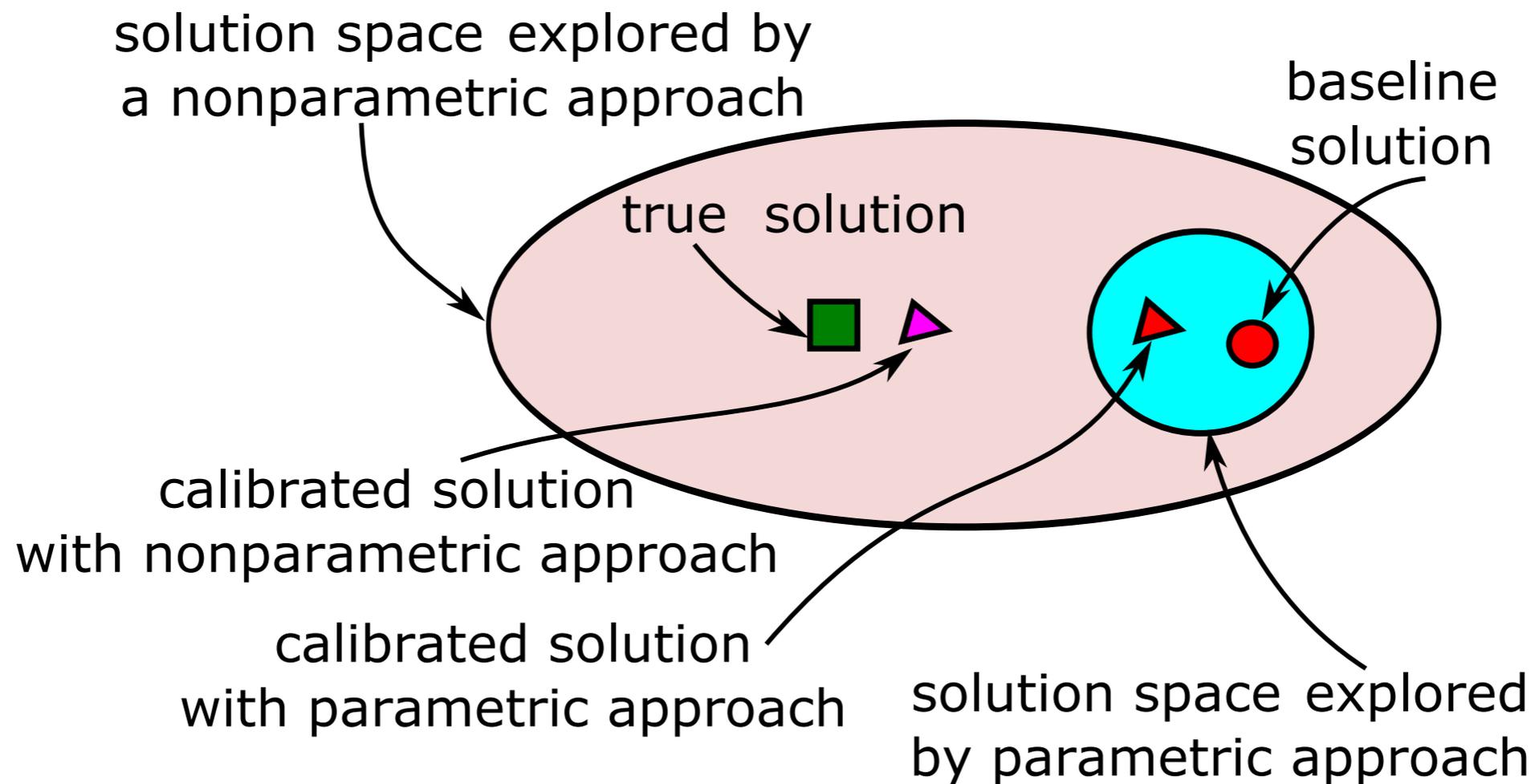
- ❖ Probability of predicted Quantity of Interest (mean velocity at a given location)



[Oliver & Moser]

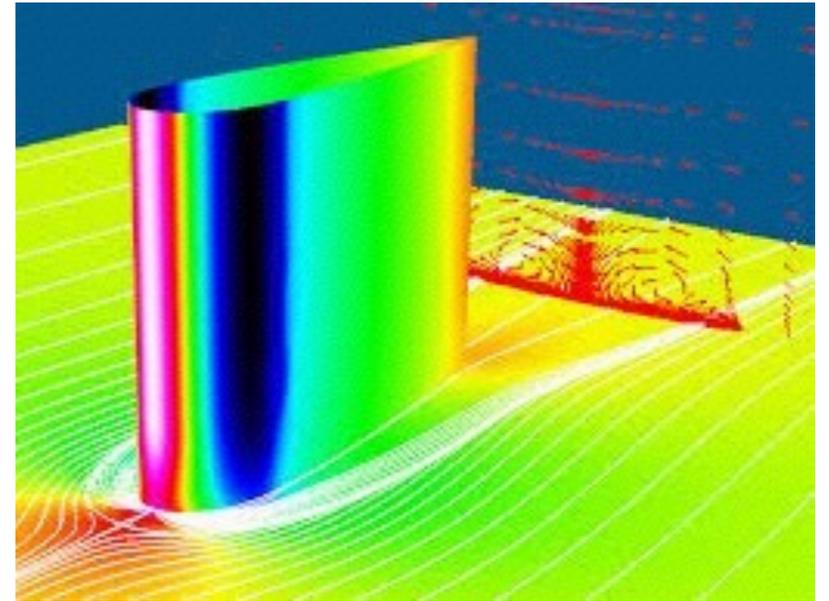
# Parametric vs. Non-parametric Approaches

- ❖ + Parametric approaches are easy to implement.
- ❖ – Restricted by the model(s): e.g., Bousinessq assumption if all candidate models are EVM. Cannot explore the solution manifold outside the assumption!

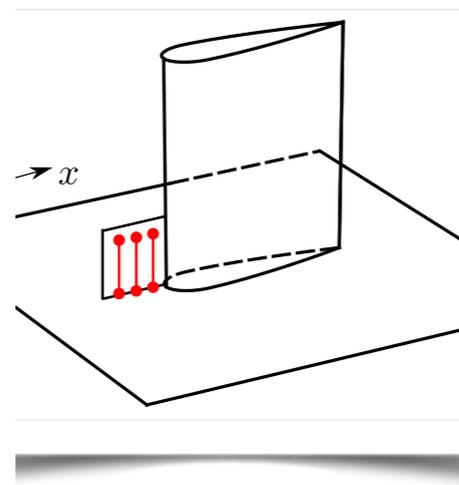
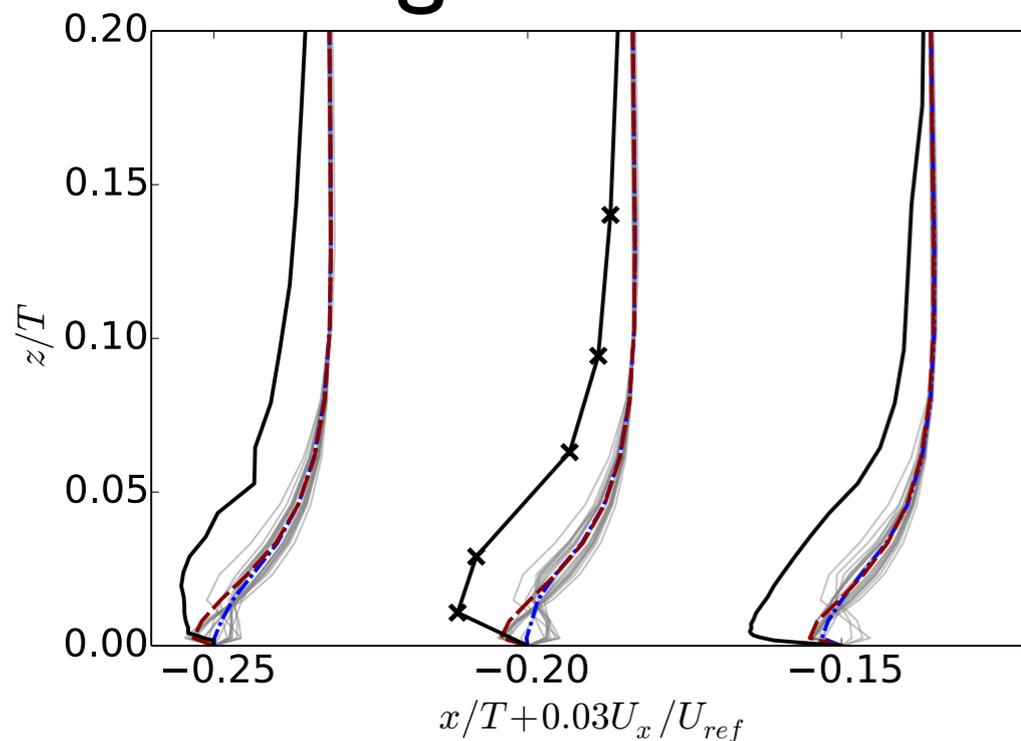


# Example: Wing-Body Junction Flow

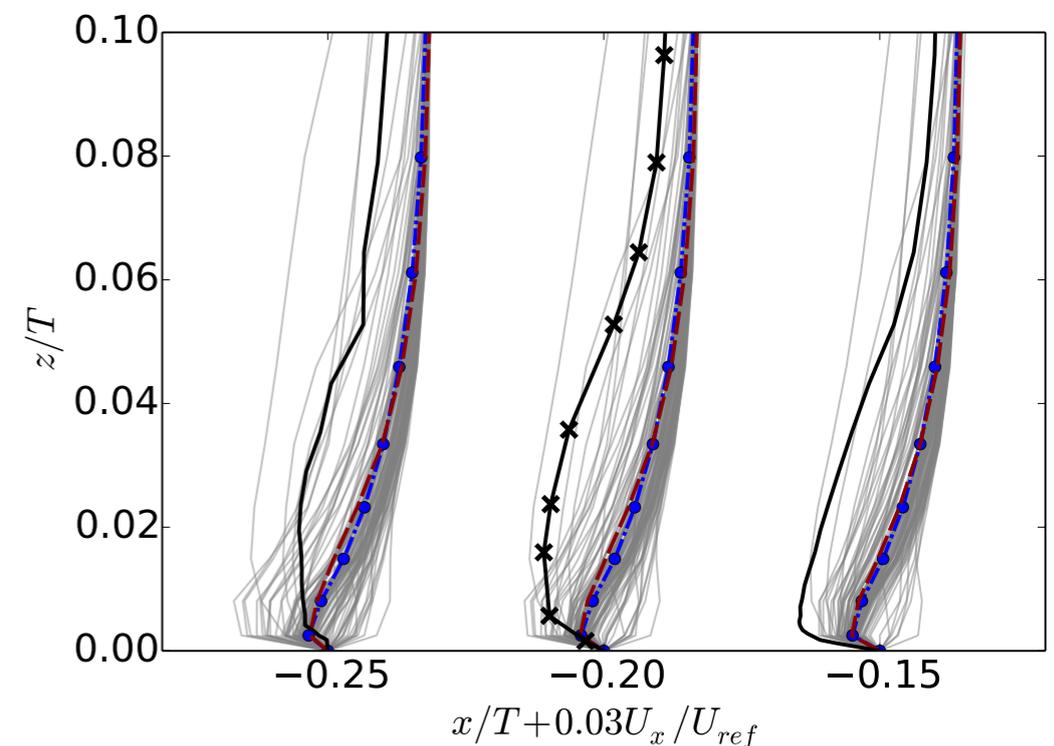
- ❖ In the leading edge region, scatter in velocity is very limited as long as the Reynolds stress is aligned with the mean rate of strain tensor  $\mathbf{S}$ .



## Aligned w/ $\mathbf{S}$



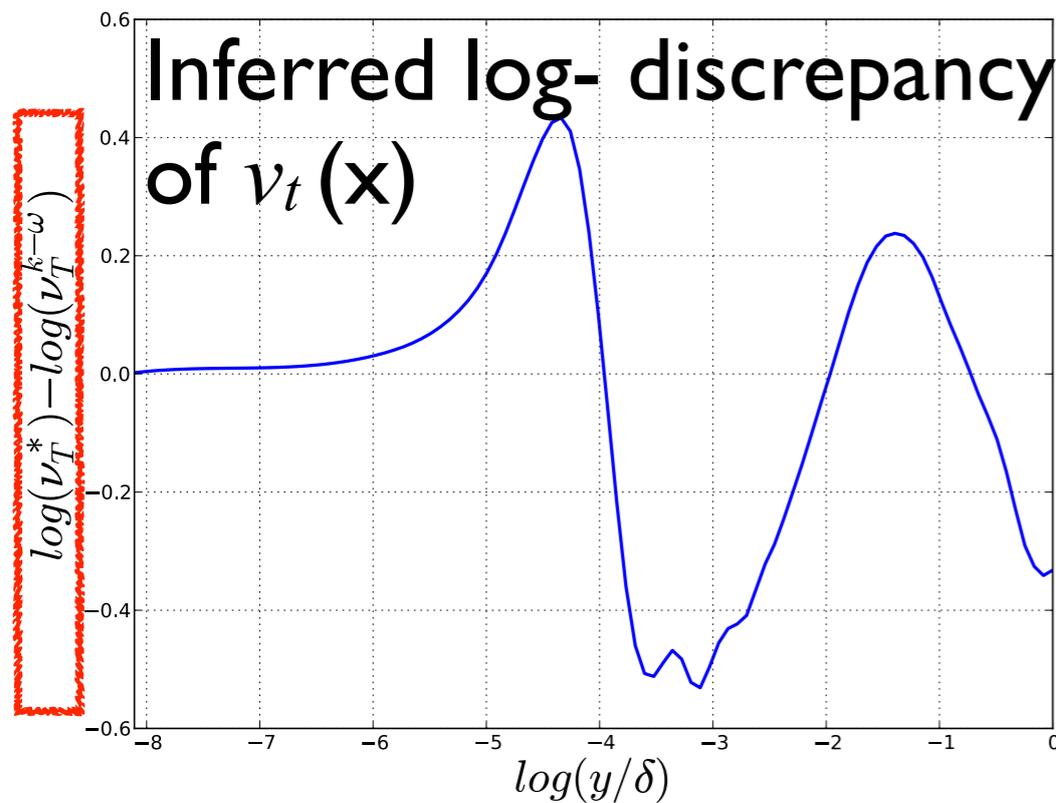
## Not aligned w/ $\mathbf{S}$



[6]. J.-L. Wu, J.-X. Wang, and H. Xiao. Quantifying Model Form Uncertainty in RANS Simulation of Wing-Body Junction Flow. Submitted to FTC, 2016.

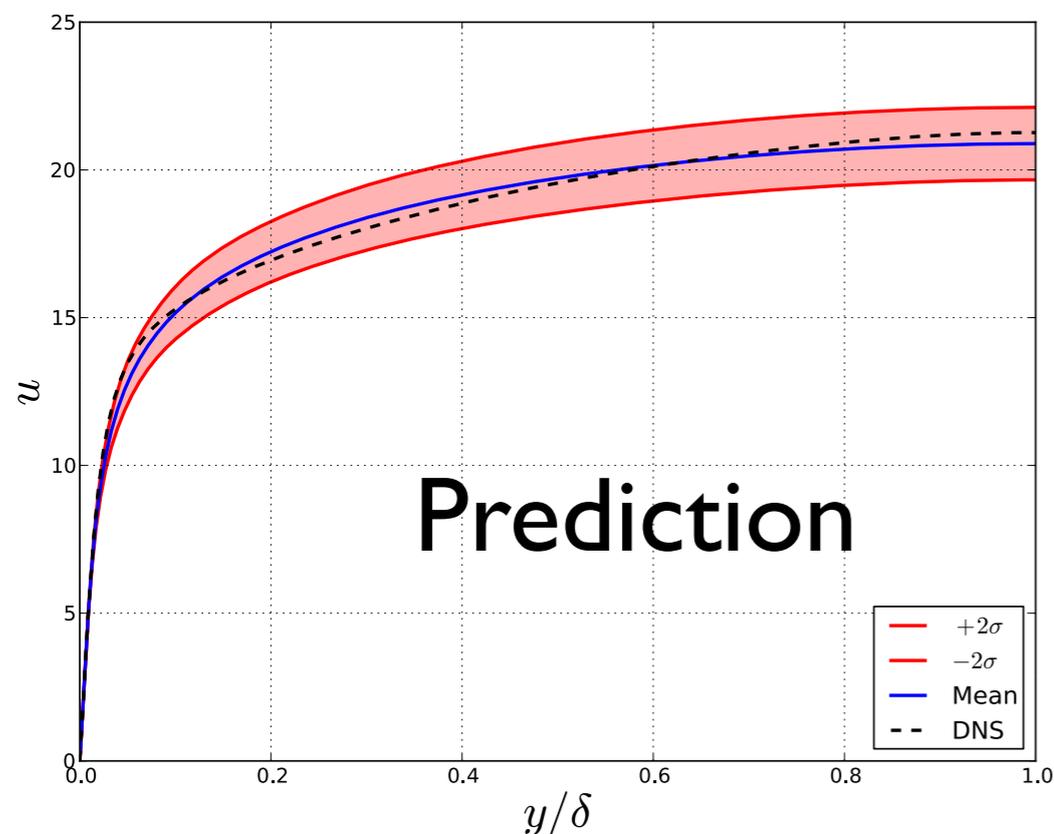
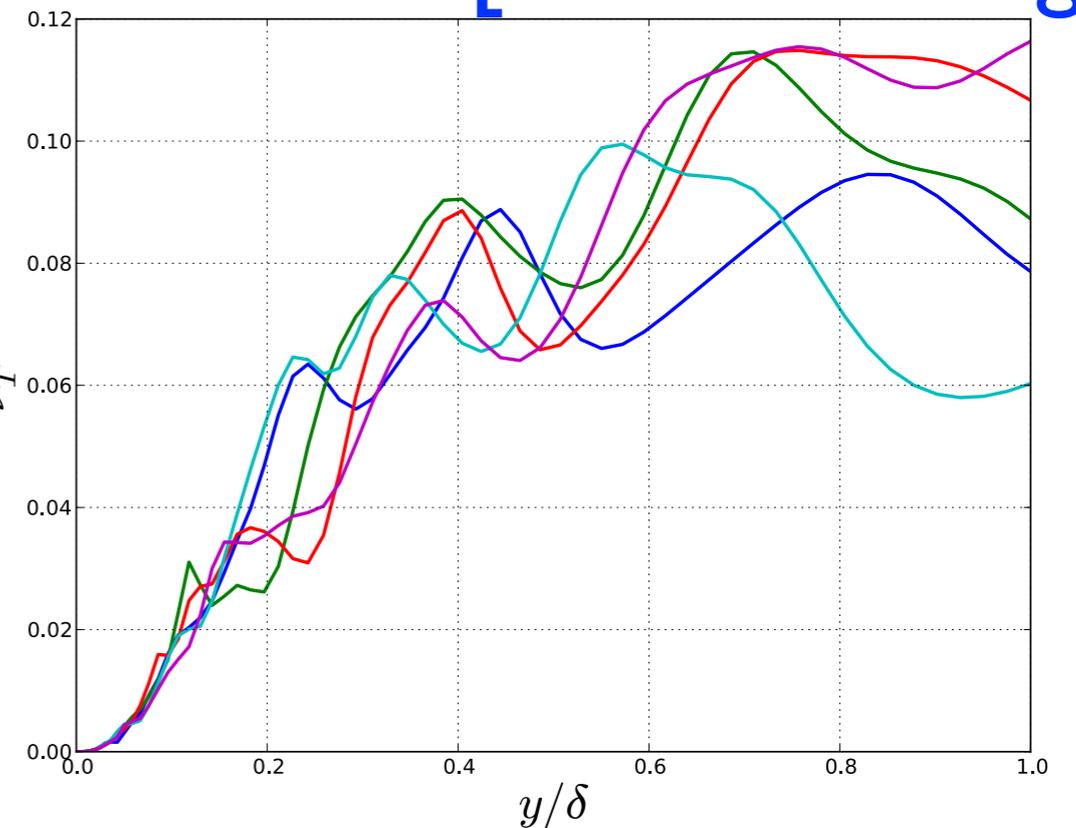
# Inferring Turbulent Viscosity Field

[Dow & Wang]



Gaussian Process

Sampling



- ❖ +++ Full field inversion with adjoint model!!
- ❖ Constrained by Boussinesq assumption.
- ❖ \* Uncertainty estimation (vs. reduction.)

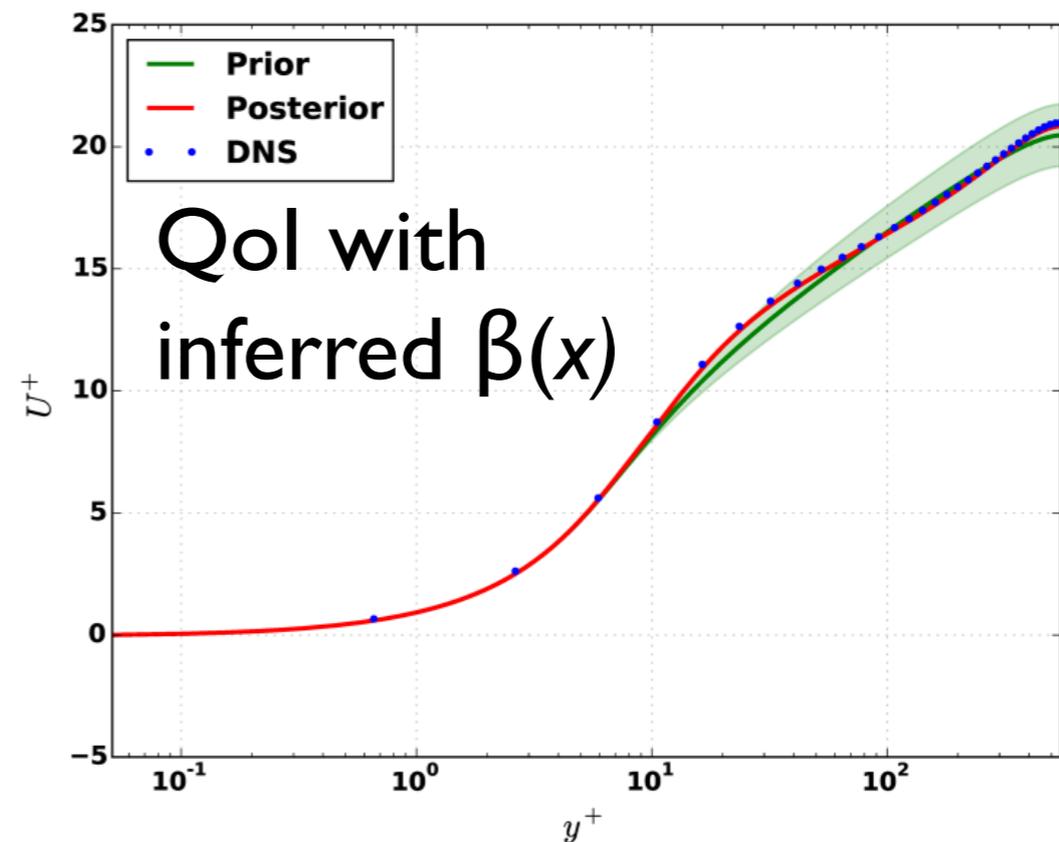
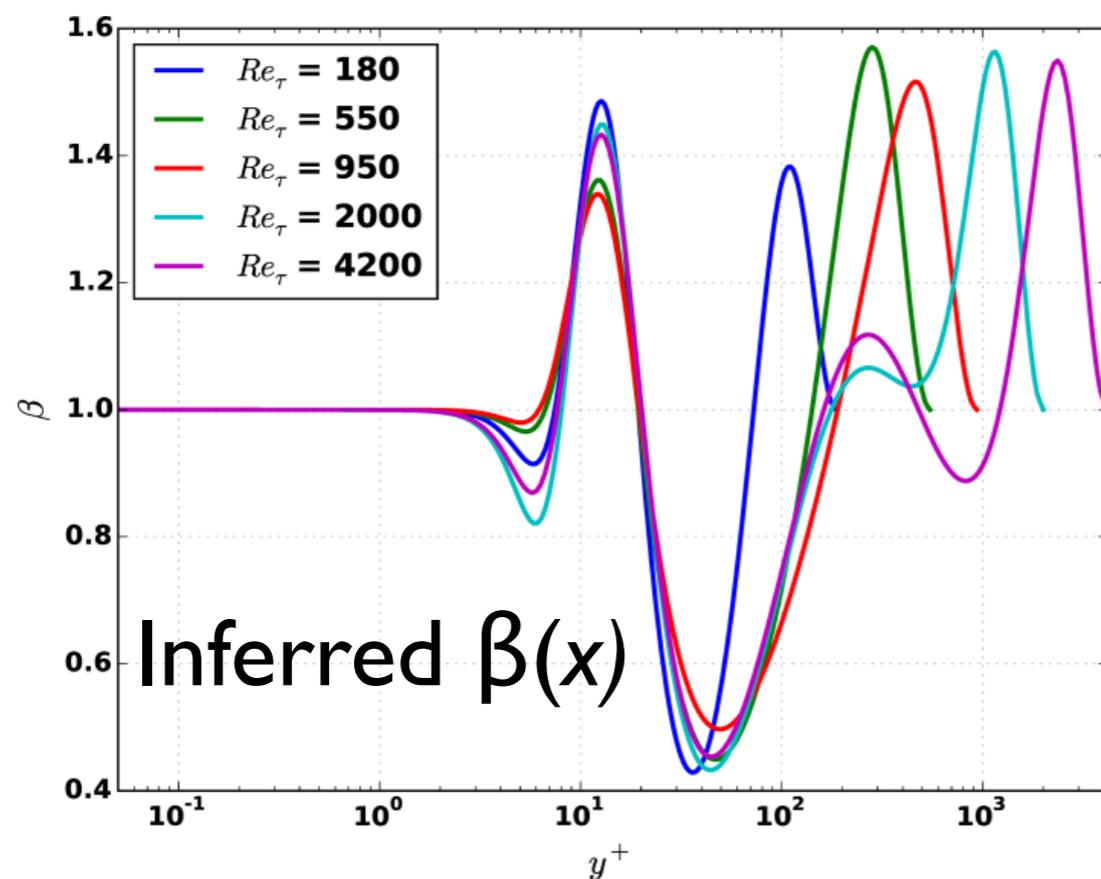
Dow & Wang, Quantification of Structural Uncertainties in the k-w Turbulence Model, AIAA 2011-1762

# Inferring Discrepancy in Turb. Quantity Equations

[Duraisamy et al.]

$$\frac{D\tilde{\nu}_t}{Dt} = \beta(x)P(\tilde{\nu}_t, \mathbf{U}) - D(\tilde{\nu}_t, \mathbf{U}) + T(\tilde{\nu}_t, \mathbf{U})$$

$$\frac{D\omega}{Dt} = \beta(x)P(\omega, \mathbf{U}) - D(\omega, \mathbf{U}) + T(\omega, \mathbf{U})$$



Singh & Duraisamy. Using field inversion to quantify functional errors in turbulence closures. POF, 28, 045110, 2016.

# Assessment: Novelty

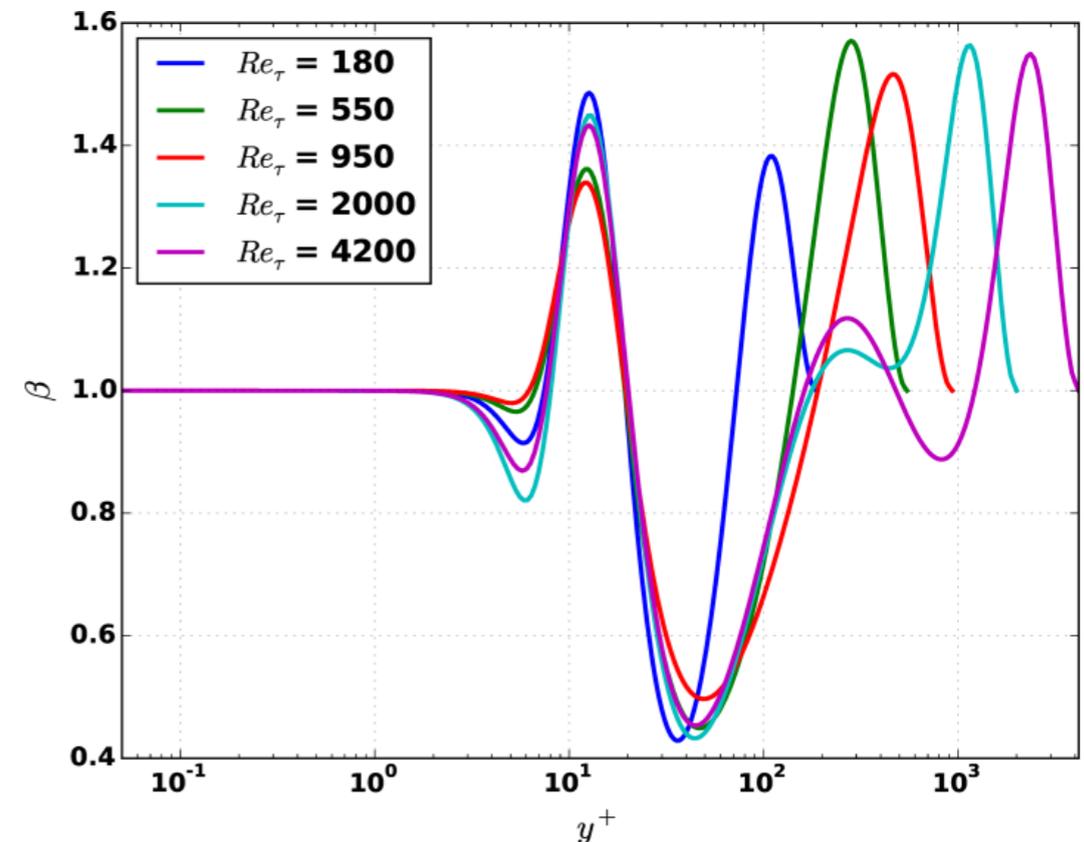
$$\frac{D\tilde{\nu}_t}{Dt} = \beta(x)P(\tilde{\nu}_t, \mathbf{U}) - D(\tilde{\nu}_t, \mathbf{U}) + T(\tilde{\nu}_t, \mathbf{U}) \quad [\text{Duraiamy et al.}]$$

- ❖ +++ Bayesian: Can use integral data (e.g., surface pressure) or sparse data to infer the multiplicative correction term  $\beta(x)$ . Then, use posterior of  $\beta(x)$  to obtain QoI (e.g., velocity).
- ❖ +++ Full field inversion! Better than parametric approaches.
- ❖ +? Model specific: different inference formulation for each model (e.g., SA, k- $\omega$ ). Can be + or -. Why plus? **Intimate connection with model: increases inference effectiveness!**
- ❖ +? Universality of  $\beta(x)$  and extrapolation to similar flows suggested but yet to be demonstrated.
- ❖ +? Constrained by assumption of the baseline model (e.g., Boussinesq assumption) but the flexibility may be sufficient!

# Assessment: Limitations

$$\frac{D\tilde{\nu}_t}{Dt} = \beta(x)P(\tilde{\nu}_t, \mathbf{U}) - D(\tilde{\nu}_t, \mathbf{U}) + T(\tilde{\nu}_t, \mathbf{U}) \quad \text{Duraiamy et al.}$$

- ❖ \* No physical basis to validate or invalidate the inferred  $\beta(\mathbf{x})$ .
- ❖ \* Different data (particularly for partial/sparse data) may give different  $\beta(\mathbf{x})$ .
- ❖ \* **Physical identifiability difficulty:** when data suggest underestimated production ( $\beta > 1$ ), it could well be overestimated dissipation, or too much transport to the neighborhood.



- ❖ **++ But: Provides valuable guidance for turbulence model development.**

# Injecting Uncertainty in Reynolds Stresses

# RANS Equations: Composite Model Theory

- The theories are reliable (based on conservation of momentum) [Oliver, Moser, et al.]

$$\nabla \cdot (\boldsymbol{\tau}_{\text{rans}})$$

$$\underbrace{\frac{\partial U_i}{\partial t} + \frac{\partial (U_i U_j)}{\partial x_j}}_{\text{convection}} + \underbrace{\frac{1}{\rho} \frac{\partial p}{\partial x_i}}_{\text{pressure grad.}} - \underbrace{\nu \frac{\partial^2 U_i}{\partial x_j \partial x_j}}_{\text{diffusion}} = \underbrace{- \frac{\partial \overline{u_i u_j}}{\partial x_j}}_{\text{div. of Reynolds stress}}$$

Mathematically rigorous/correct

Reynolds stresses  
need closure model

- Uncertainties are mostly caused by the closure model for the Reynolds stress.

$$\mathcal{N}(U) = \nabla \cdot (\boldsymbol{\tau}_{\text{rans}})$$

with

$$\boldsymbol{\tau}_{\text{rans}} = \frac{\nu_t}{2} (\nabla U + \nabla^t U)$$

# Injecting Uncertainty in Reynolds Stresses

[Oliver, Moser et al.]

- ❖ **+++ Introduce Reynolds stress discrepancy tensor to RANS equation and model with stochastic differential equation.**
- ❖ **The SDE is similar but simpler than RSTM equations. Driven by Wiener process (white noise).**

$$\frac{d\epsilon}{d\eta} = \sigma \left( \frac{1}{Re_\tau} + \nu_t(\bar{u}^+) \right)^{3/4} \left( \frac{d\bar{u}^+}{d\eta} \right)^{5/4} \frac{dW}{d\eta}$$

**channel flow**

- ❖ **Proof of concept in Burger's eqn. and channel flow.**
- ❖ **\* Yet to be applied to more realistic flows.**

# Injecting Uncertainty in Reynolds Stresses

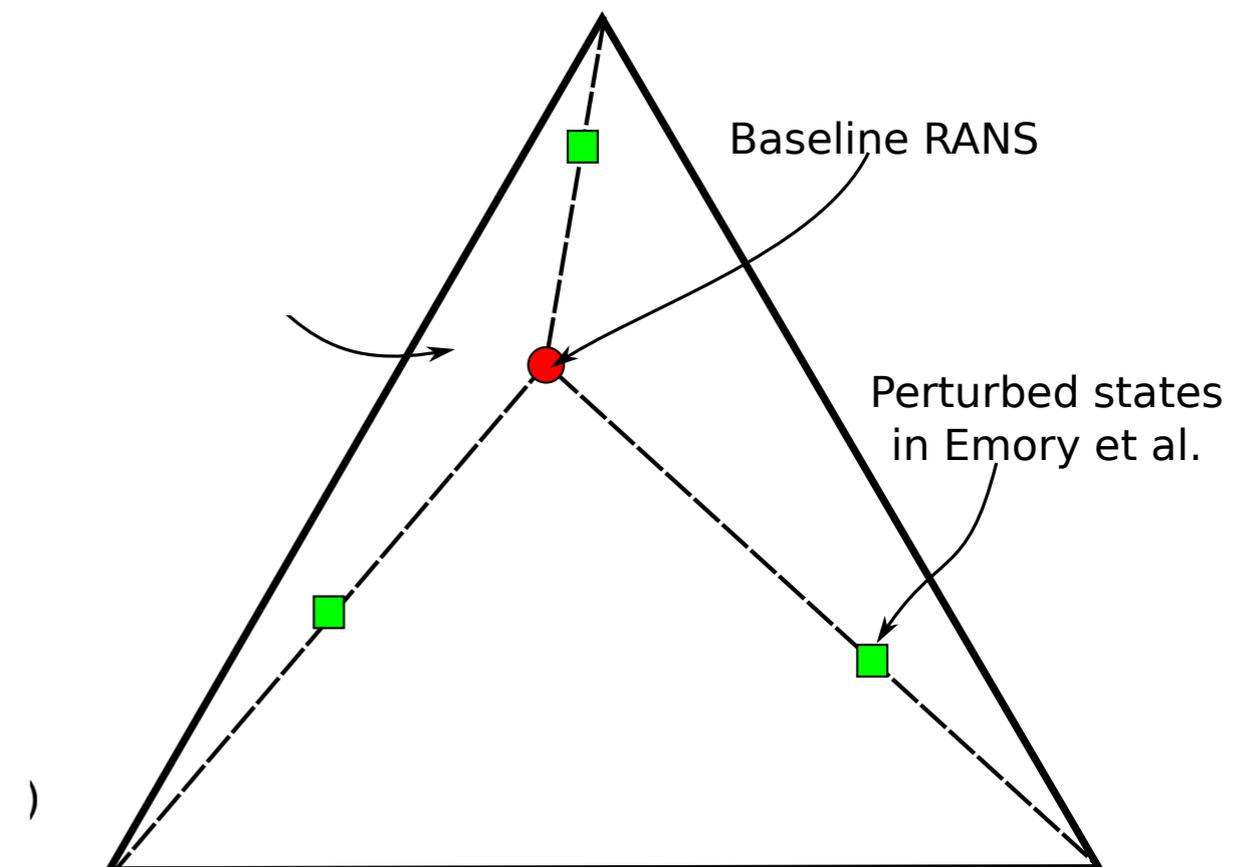
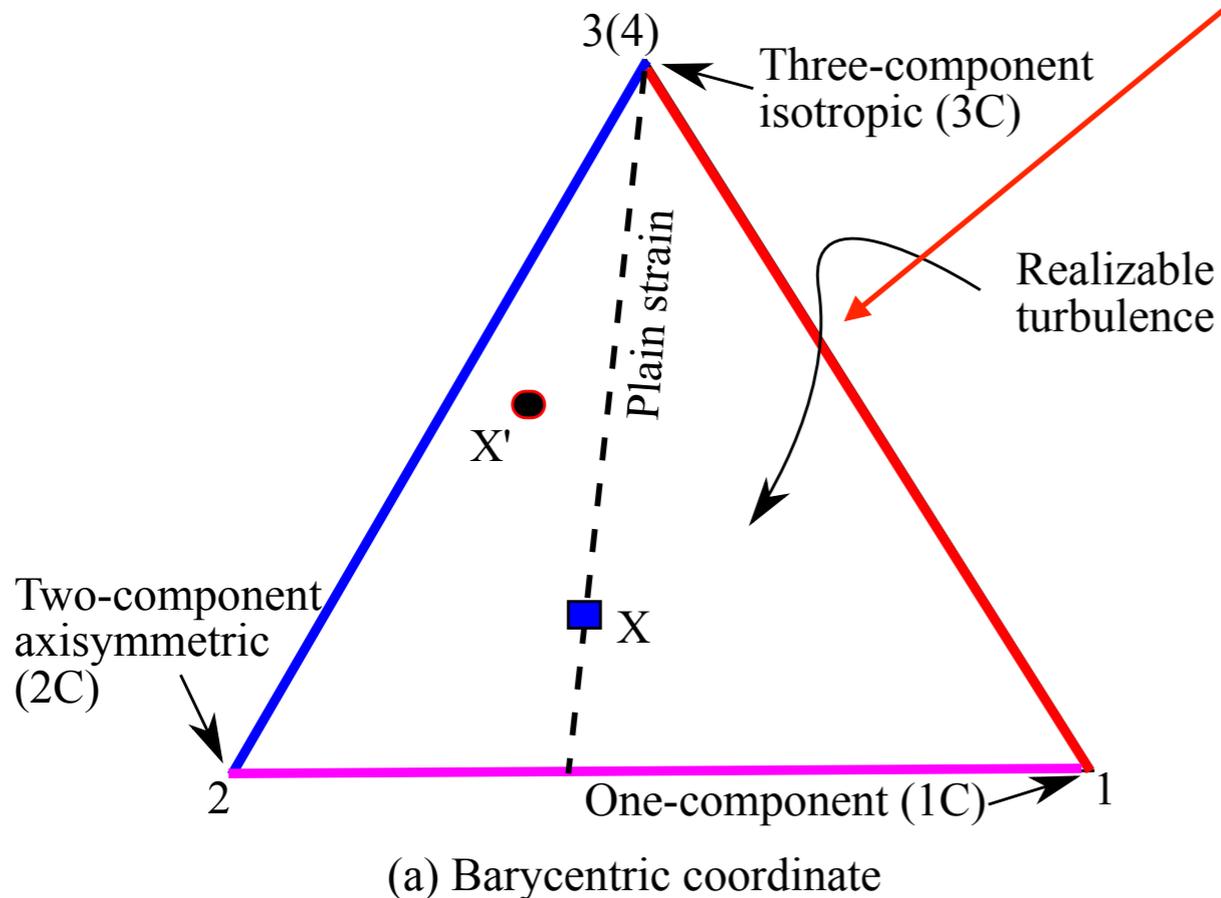
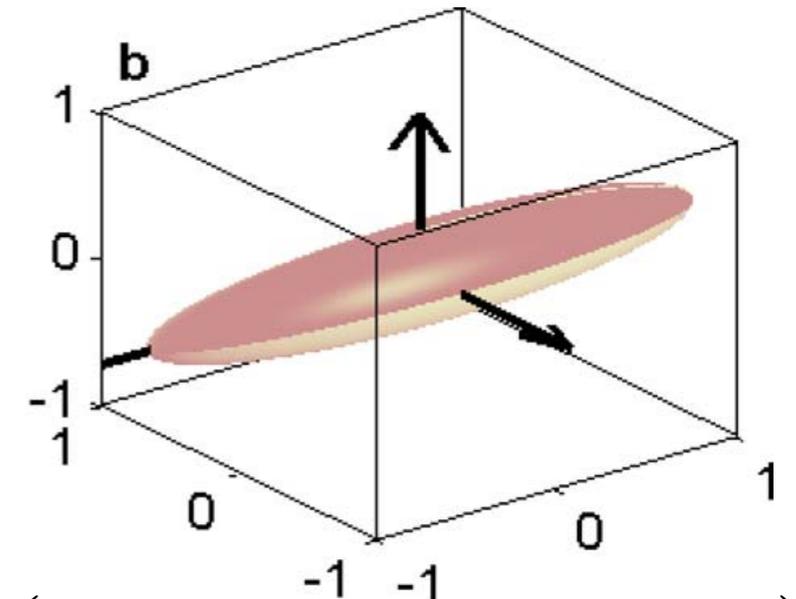
Emory, Gorle, Iaccarino, et al.

Fig. from Simonsen & Krogstad, POF 2005

- ❖ Perturb towards three limiting states in Barycentric triangle (realizability map)

$$\boldsymbol{\tau} = 2k \left( \frac{1}{3} \mathbf{I} + \mathbf{a} \right) = 2k \left( \frac{1}{3} \mathbf{I} + \mathbf{V} \boldsymbol{\Lambda} \mathbf{V}^T \right)$$

$$\boldsymbol{\tau} \longrightarrow (k, \xi, \eta, \varphi_1, \varphi_2, \varphi_3)$$



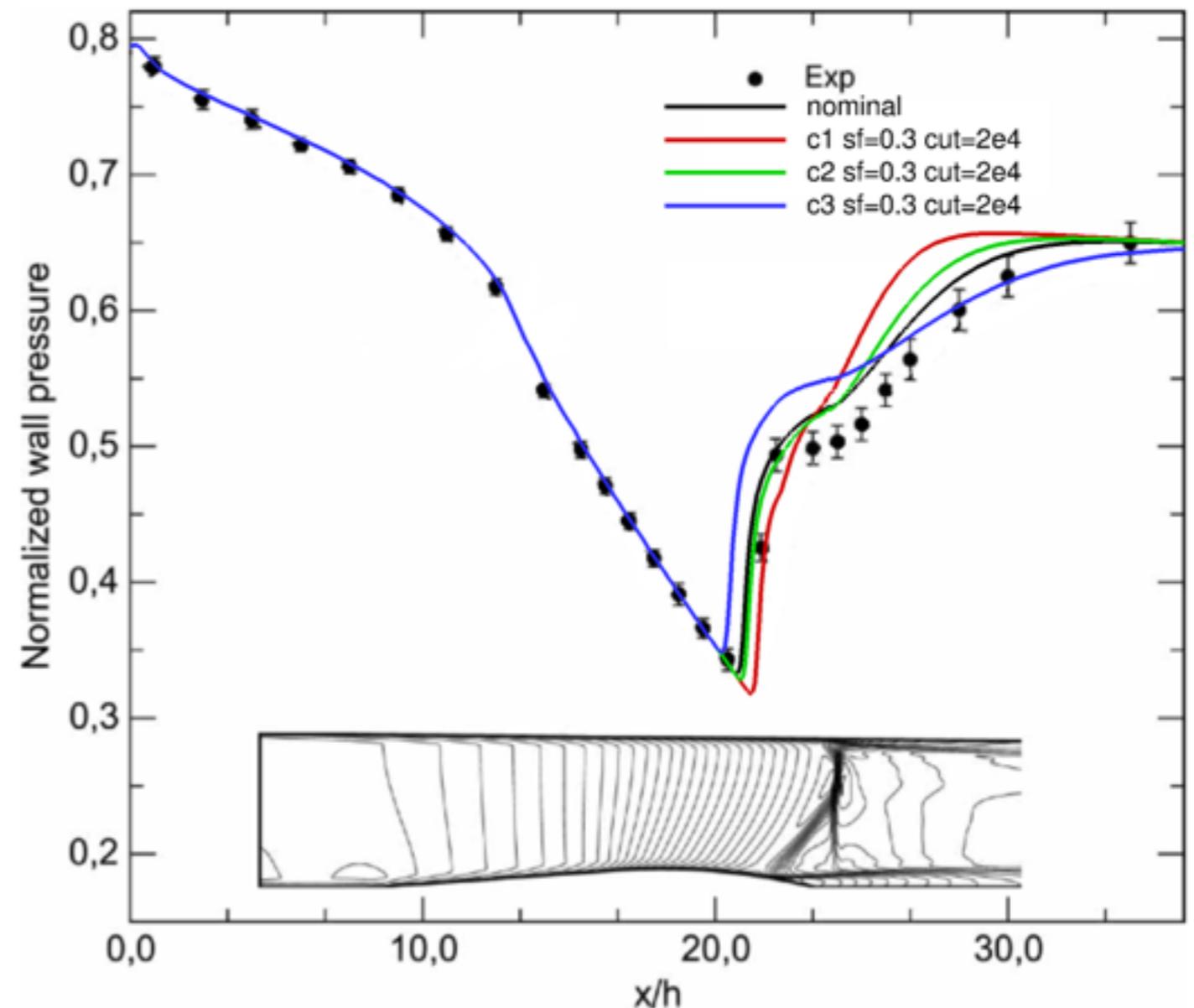
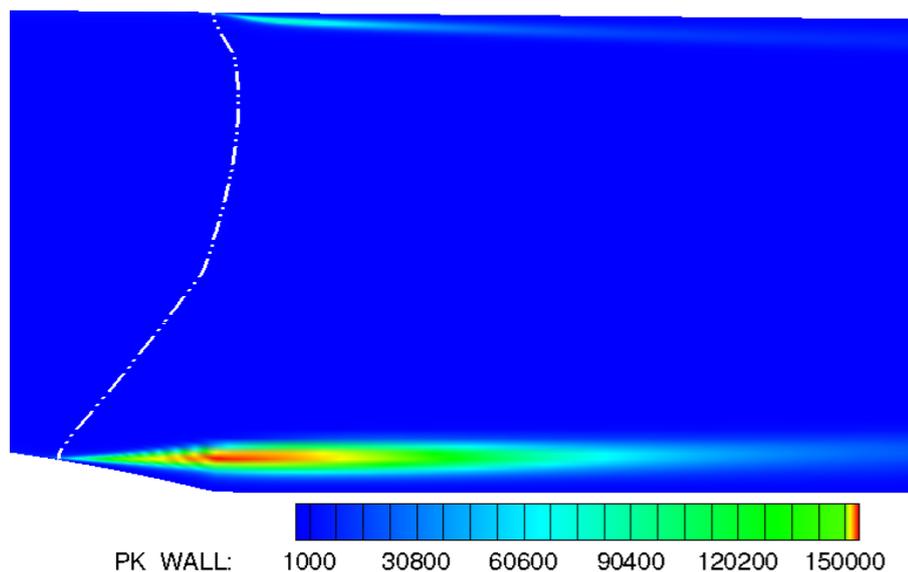
# Injecting Uncertainty in Reynolds Stresses

Emory, Iaccarino, et al.

- ❖ Use empirical marker function to specify the extent of perturbation towards realizable limit (vertices).
- ❖ Propagate to velocities and QoIs



Marker function



# Assessment: Major Novelty

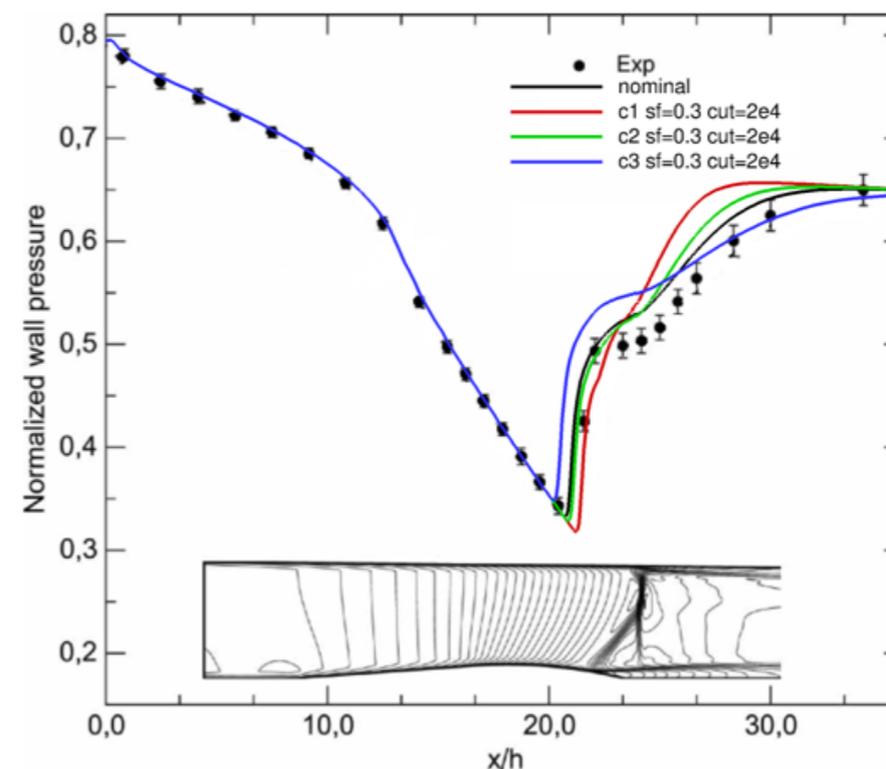
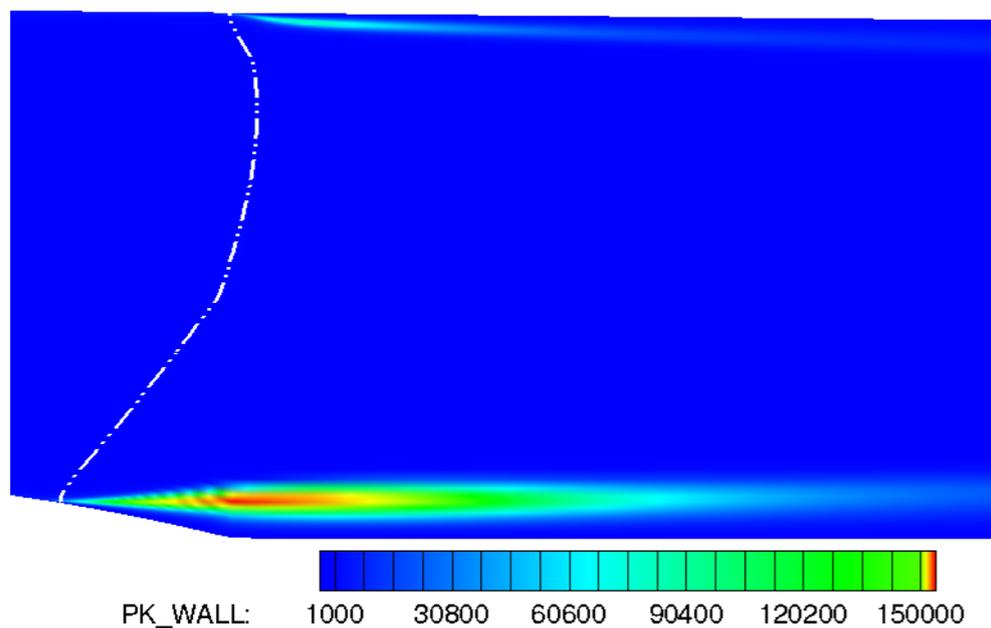
Emory, Gorle, Iaccarino, et al.

- ❖ +++ First to use realizability constraints to quantify RANS model form uncertainty (pioneering work!)
- ❖ \* But: realizability only provides bound for anisotropy perturbations. Only weak constraints on TKE and orientation.
- ❖ +++ Not constrained by the Boussinesq assumption.
- ❖ +++ Directly perturb Reynolds stress: same procedure for different models.
- ❖ \* Three evaluations: not a comprehensive exploration of the high dimensional uncertainty space.

# Assessment: Other Minor Pros and Cons

Emory, Gorle, Iaccarino, et al.

- ❖ + Low computational overhead. Only three simulations needed: three perturbations; one marker function.
- ❖ – Empirical function needed for spatial distribution of the perturbations.



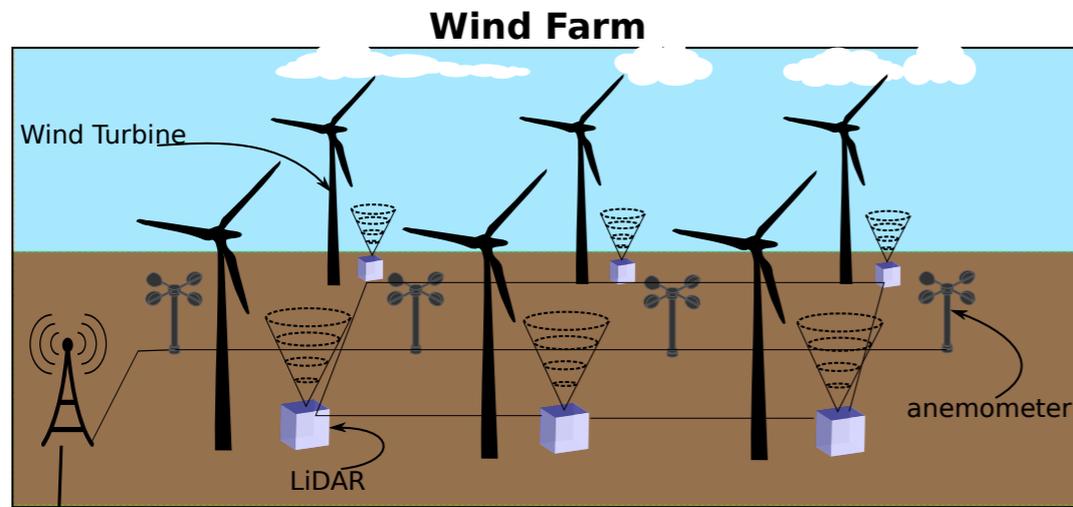
# Our Approach

A Data-Driven, Physics-Informed  
Approach  
Based on Bayesian Inference

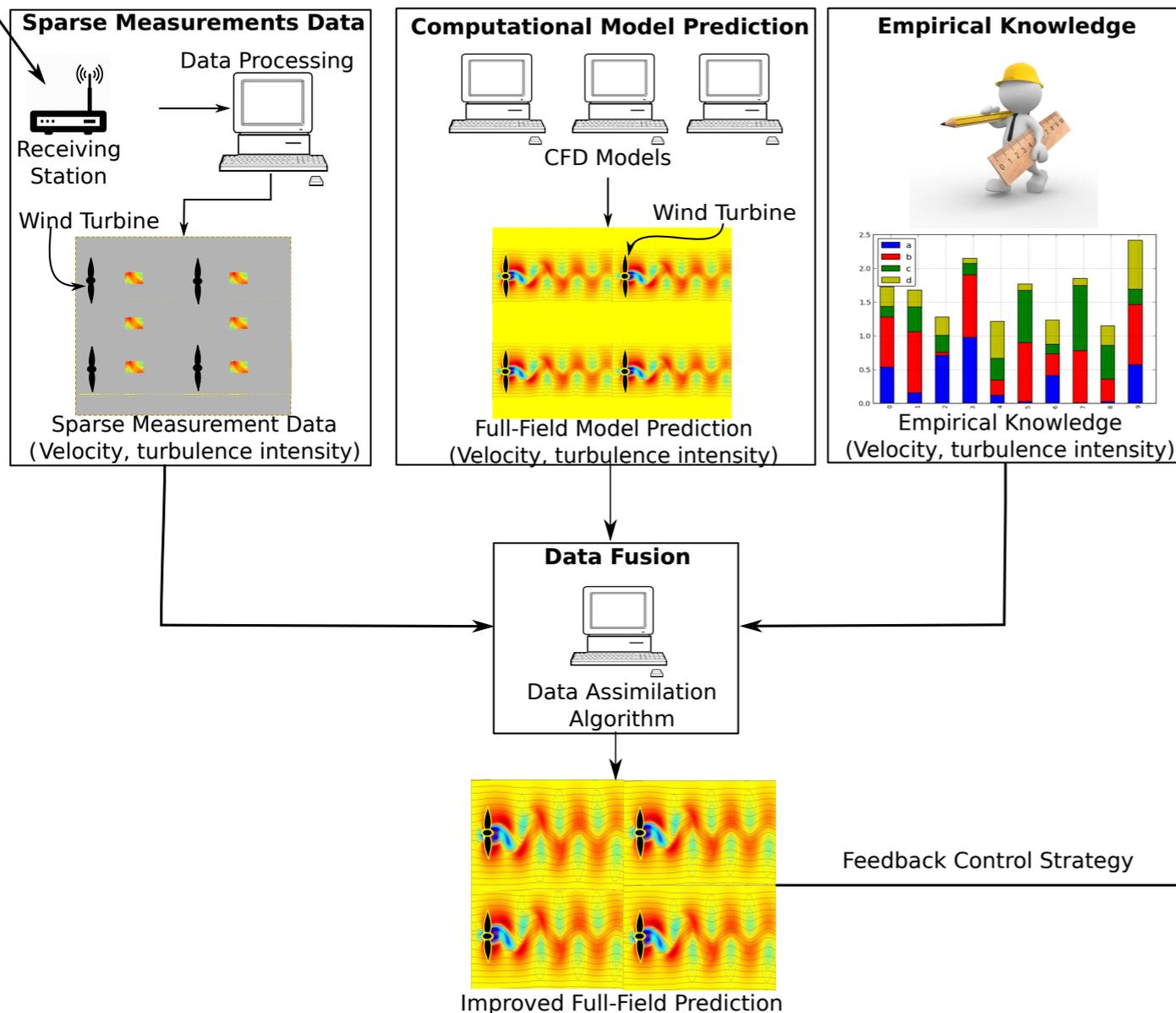
# Two Scenarios of Industrial CFD Simulations

- ❖ **Monitoring / Forecasting**
- ❖ **Support Design/Optimization**

# CFD to Support System Monitoring



Wireless Transmission



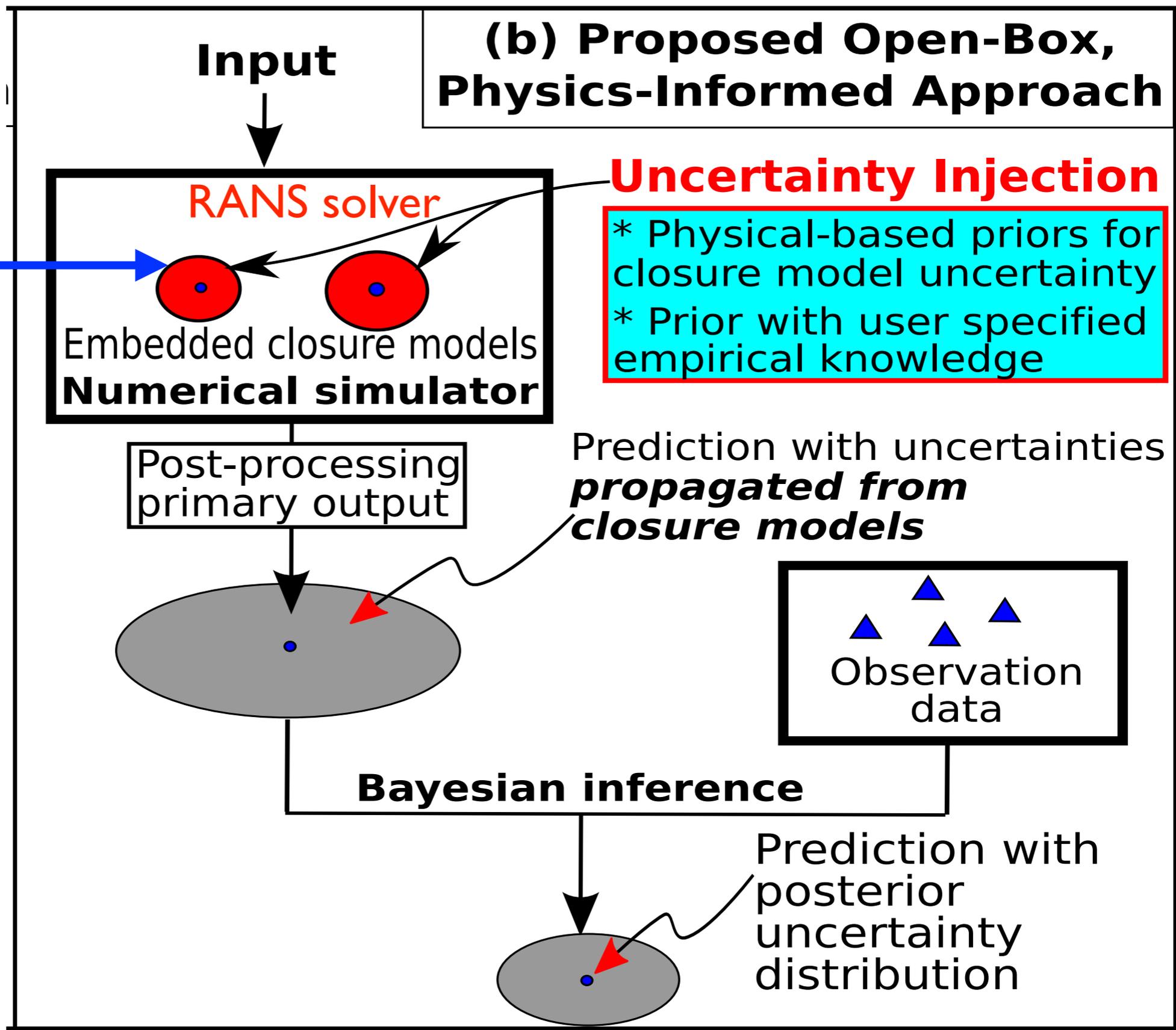
Real-time  
streamed sensor  
data are available  
but are sparse

$$\mathcal{N}(U)$$

=

$$\nabla \cdot (\tau_{\text{rans}} + \delta\tau)$$

Model the discrepancy as zero mean random field.

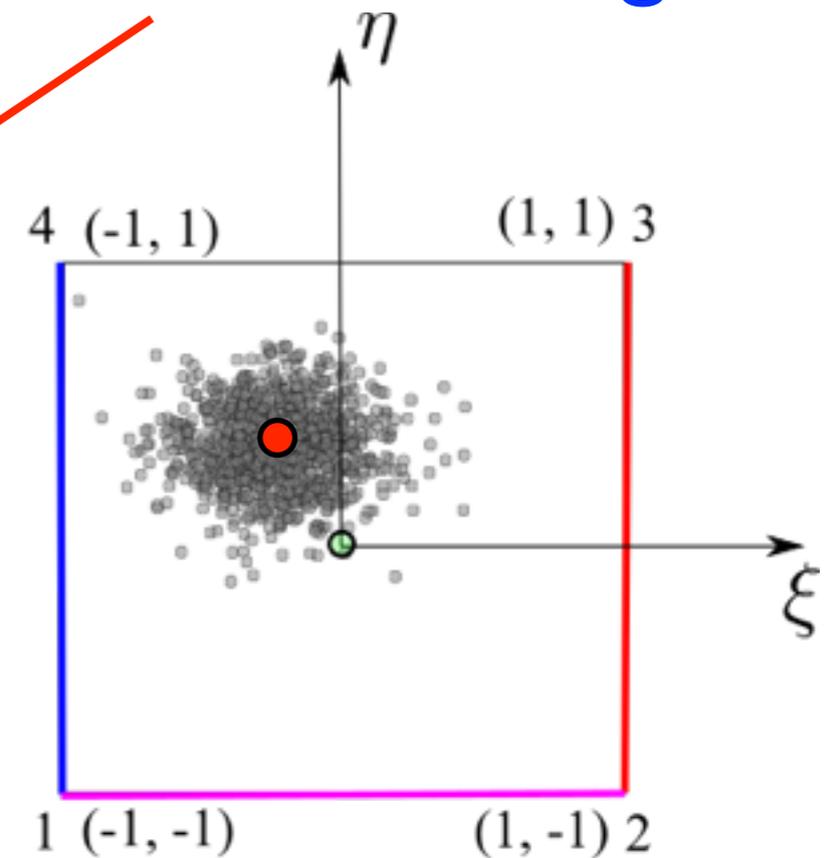
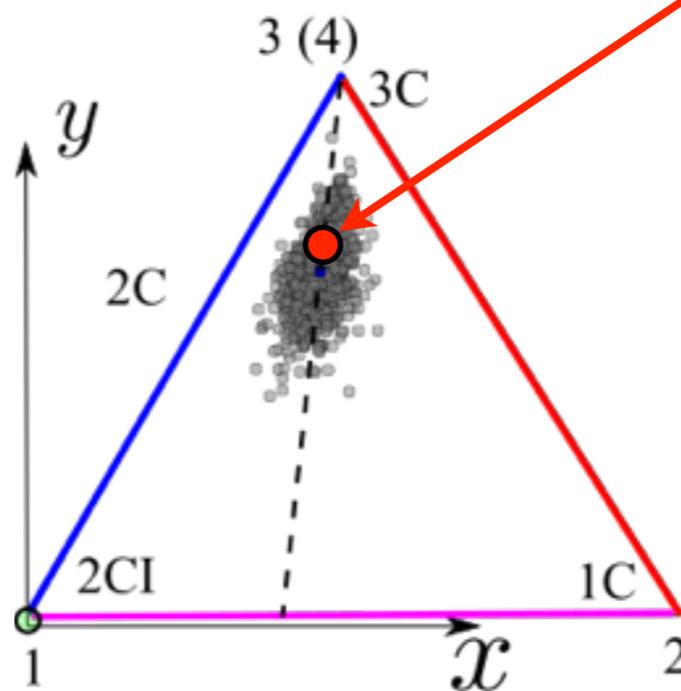
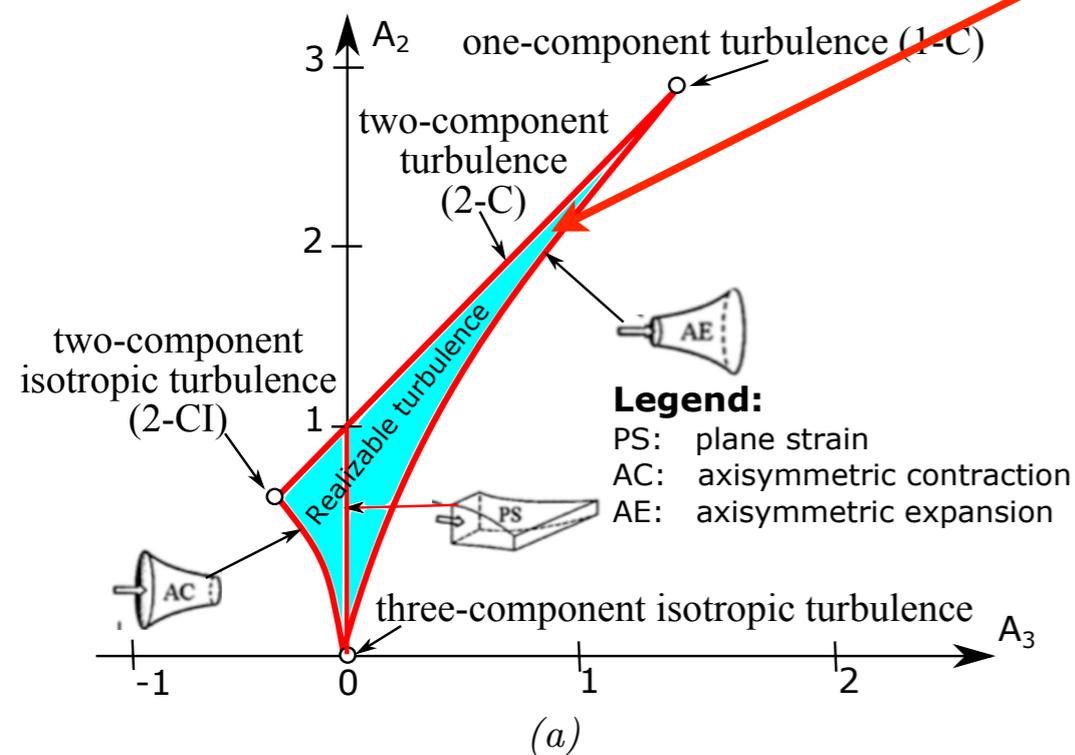


# What do we know about Reynolds stresses?

- Symmetric tensor field with physical realizability constraints:

Inject uncertainty only in the realizable range

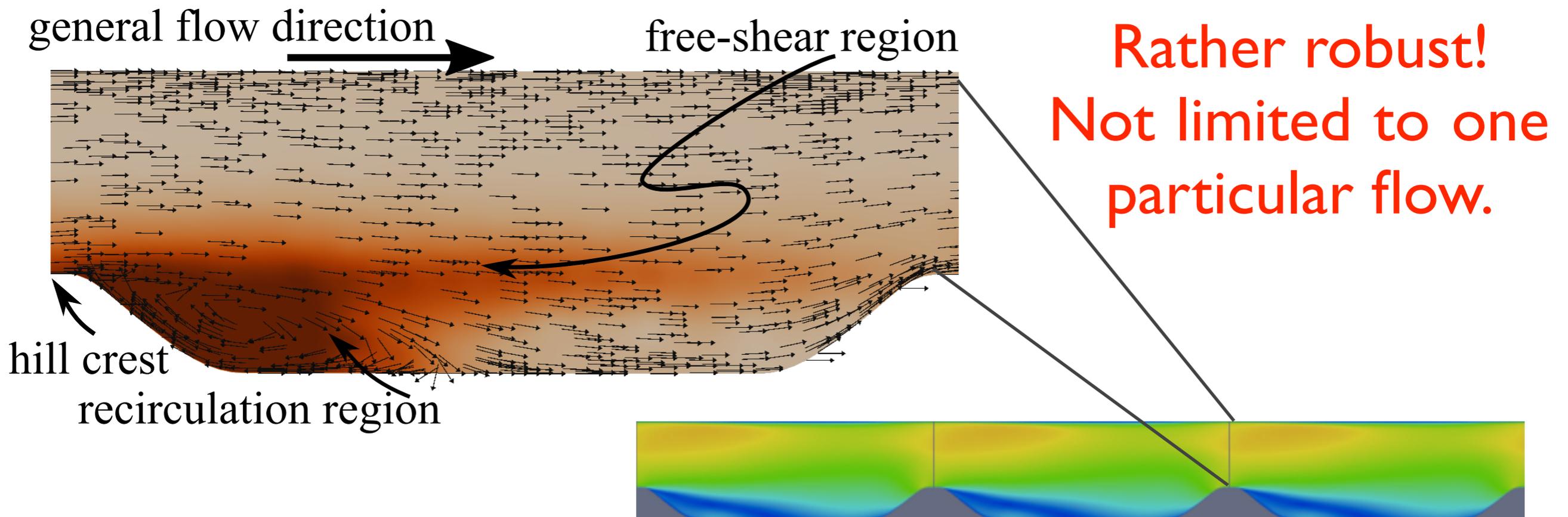
$$\boldsymbol{\tau} = 2k \left( \frac{1}{3} \mathbf{I} + \mathbf{a} \right) = 2k \left( \frac{1}{3} \mathbf{I} + \mathbf{V} \boldsymbol{\Lambda} \mathbf{V}^T \right)$$



References: M. Emory, R. Pecnik, G. Iaccarino, AIAA 2011; C. Gorle, G. Iaccarino, POF 2013; M. Emory, J. Larsson, G. Iaccarino, POF 2013;

# What do we know about Reynolds stresses?

- ❖ Reynolds stress field (and its discrepancies) are smooth, with length scales comparable to the length scale of the mean flow features.
- ❖ Certain regions are more problematic for RANS models: separation, mean flow curvature, adverse pressure gradient etc.



# Physics Based Prior: Summary

Perform RANS baseline simulation:

$$\tau \rightarrow (k, \lambda_1, \lambda_2) \rightarrow (k, C_1, C_2) \rightarrow (k, \xi, \eta)$$

truth

$$k(x) = \tilde{k}^{rans}(x) \exp[\delta^k(x)]$$

$$\xi(x) = \tilde{\xi}^{rans}(x) + \delta^\xi(x)$$

$$\eta(x) = \tilde{\eta}^{rans}(x) + \delta^\eta(x)$$

RANS prediction

discrepancy

$$\delta^k(x, \theta^k) = \sum_{i=1}^{\infty} \omega_i^k |_{\theta^k} \phi_i(x)$$

$$\delta^\xi(x, \theta^\xi) = \sum_{i=1}^{\infty} \omega_i^\xi |_{\theta^\xi} \phi_i(x)$$

$$\delta^\eta(x, \theta^\eta) = \sum_{i=1}^{\infty} \omega_i^\eta |_{\theta^\eta} \phi_i(x)$$

basis functions

Reynolds stress field is parameterized with a small number of coefficients:

$$\omega \equiv [\omega_1^k, \omega_1^\xi, \omega_1^\eta, \omega_2^k, \omega_2^\xi, \omega_2^\eta, \dots, \omega_m^k, \omega_m^\xi, \omega_m^\eta]$$

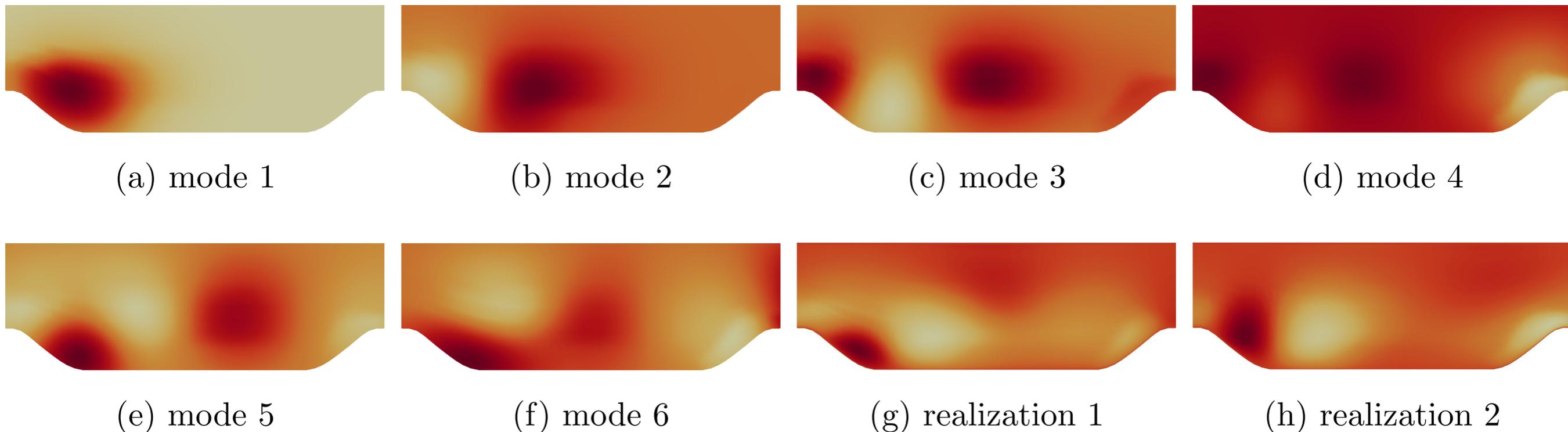
**Physics Based Dimension Reduction!**

# Modes and Realizations of Discrepancy

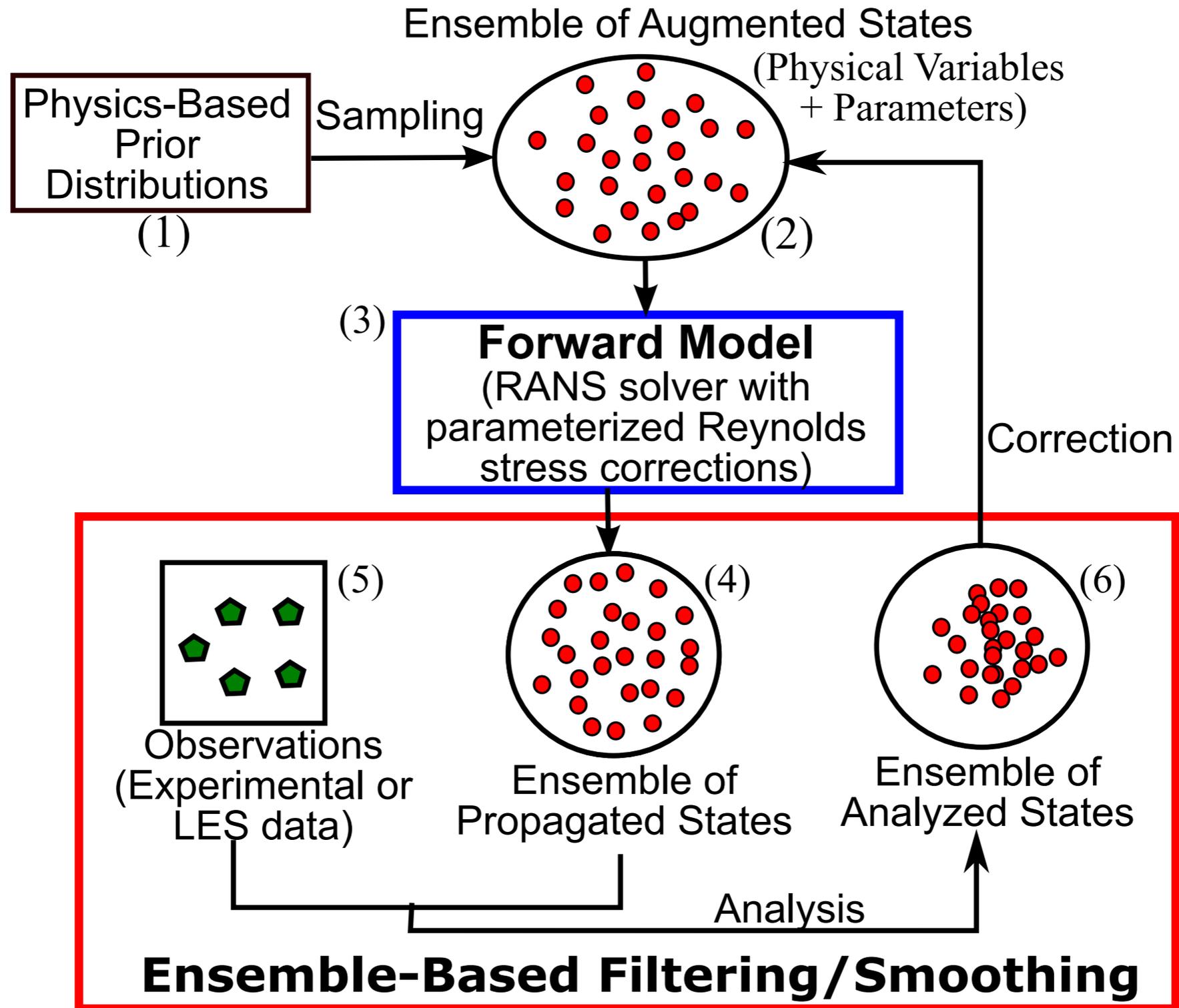
- The prior is modeled as a Gaussian process:

$$K(x, x') = \sigma(x)\sigma(x') \exp\left(-\frac{|x - x'|^2}{l^2}\right)$$

- Basis functions are obtained with Karhunen-Loeve expansion. **The prior knowledge is encoded in the basis functions.**



# Summary of the UQ Algorithm

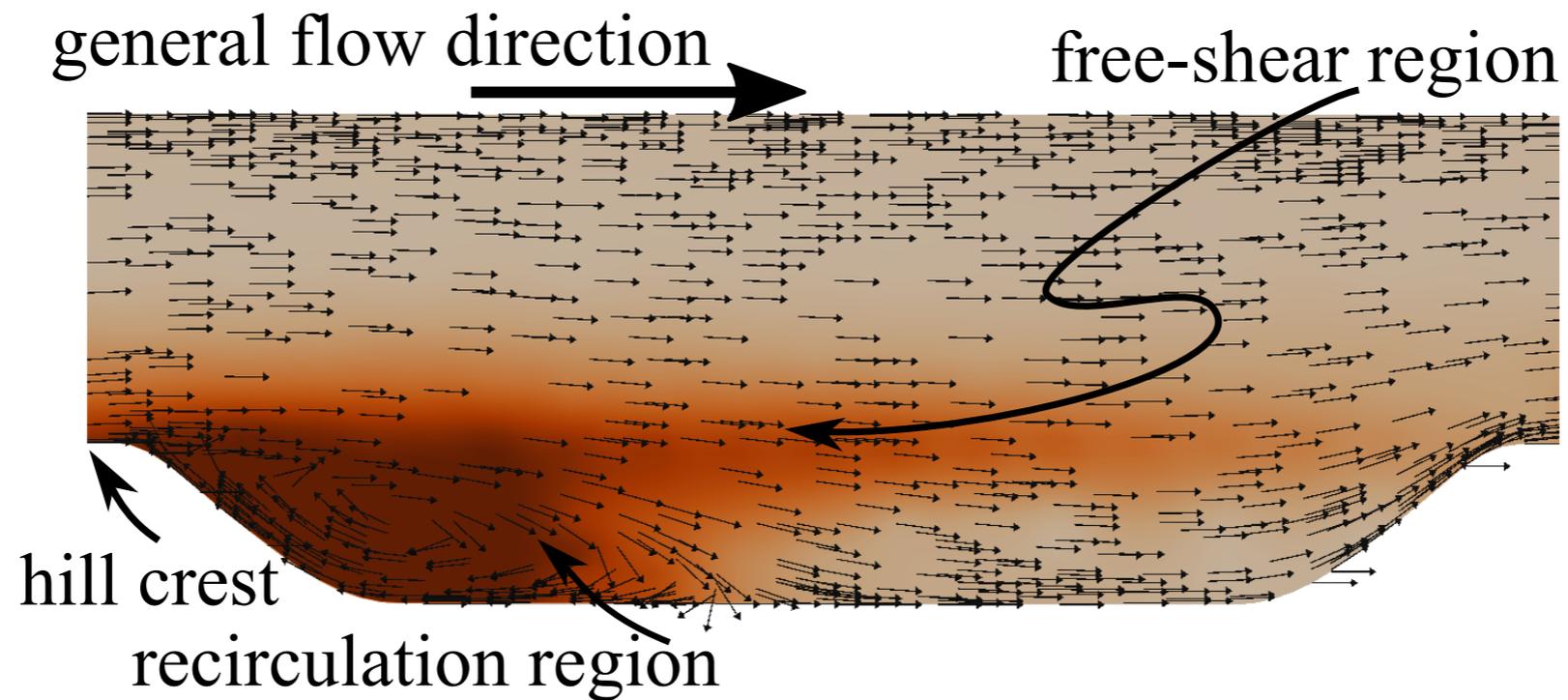


M. A. Iglesias, K. J. Law, A. M. Stuart, Ensemble Kalman methods for inverse problems, Inverse Problems 29 (4) (2013) 045001.

Simple Model (standard RANS models)  
+  
Sparse Data (velocity observations)  
+  
Physics-Based Prior Knowledge  
=  
Predictions  
(better than advanced models)  
with quantified uncertainties

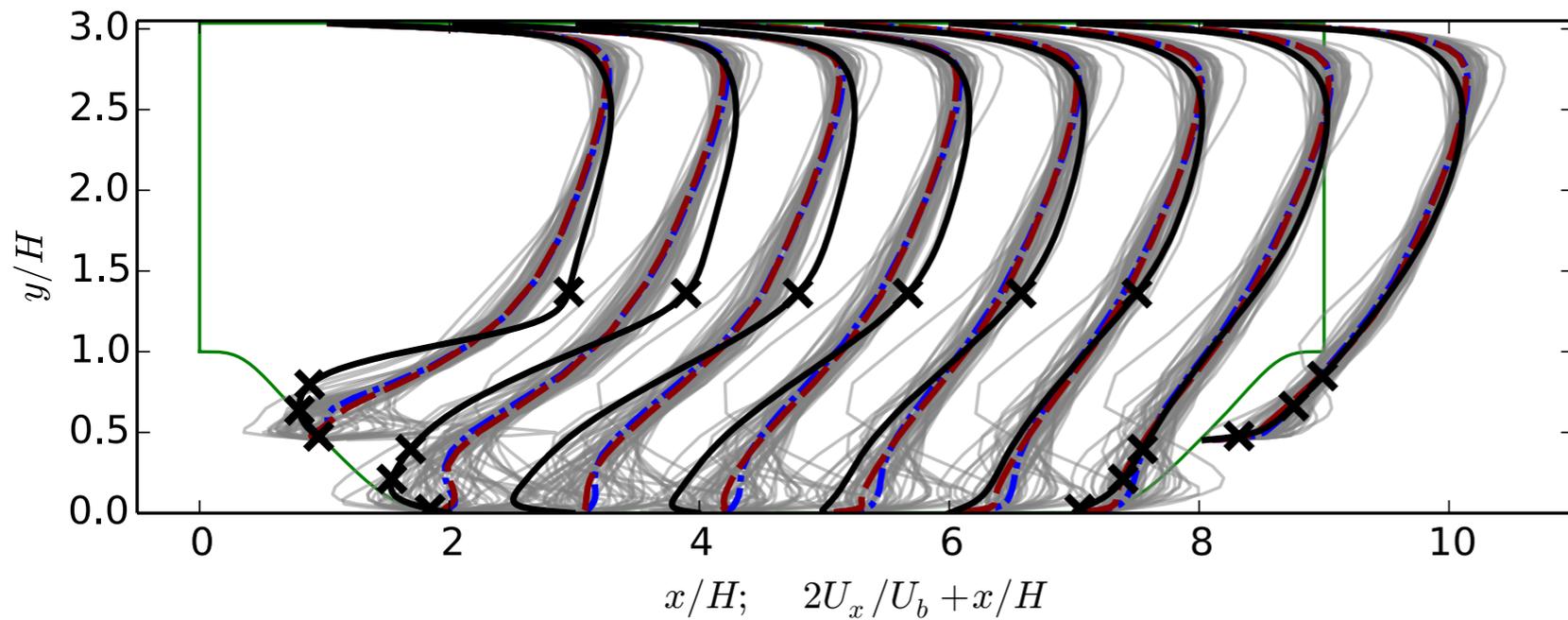
- [1]. H. Xiao, J.-L. Wu, J.-X. Wang, R. Sun, and C. J. Roy. Quantifying and reducing model-form uncertainties in Reynolds averaged Navier-Stokes equations: An open-box, physics-based, Bayesian approach. Submitted to JCP, 2015.

# Test Case I: Flow Over Periodic Hills



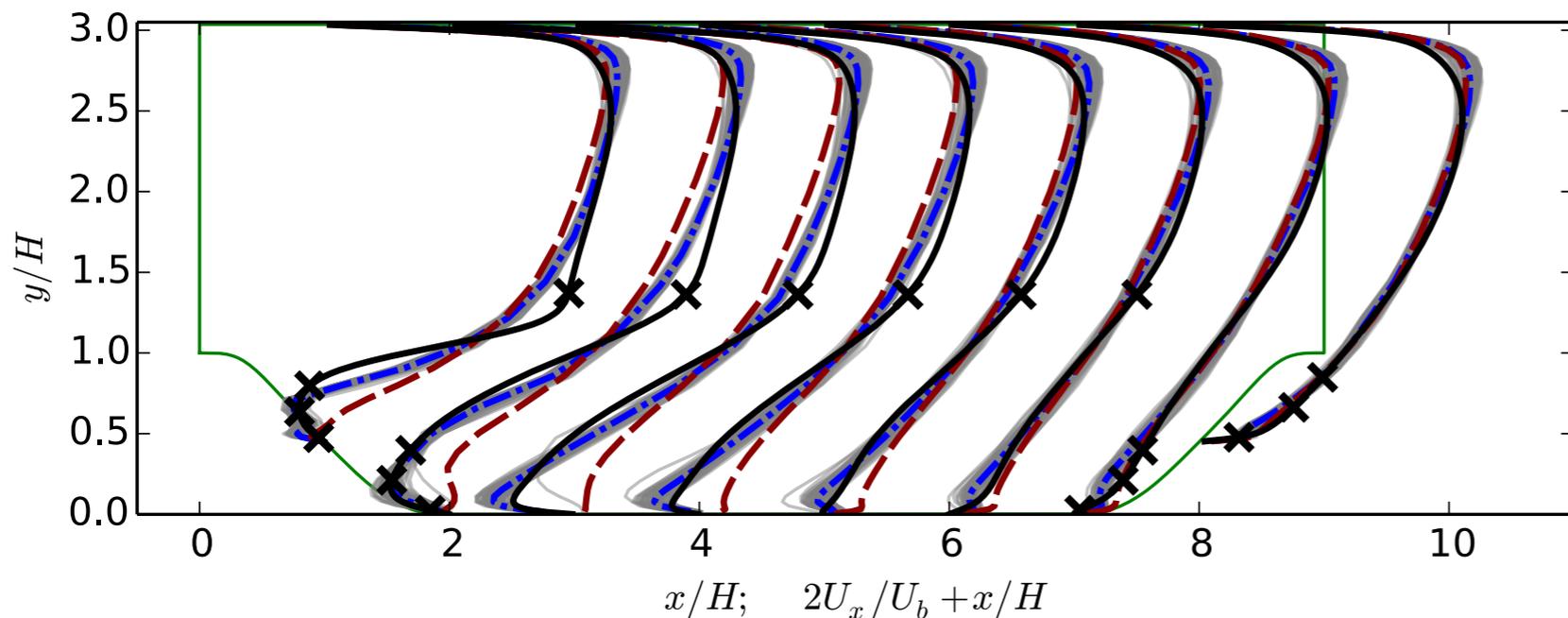
Shown previously.

# Prior and Posterior Velocities



(a) Prior velocities ensemble

Prior



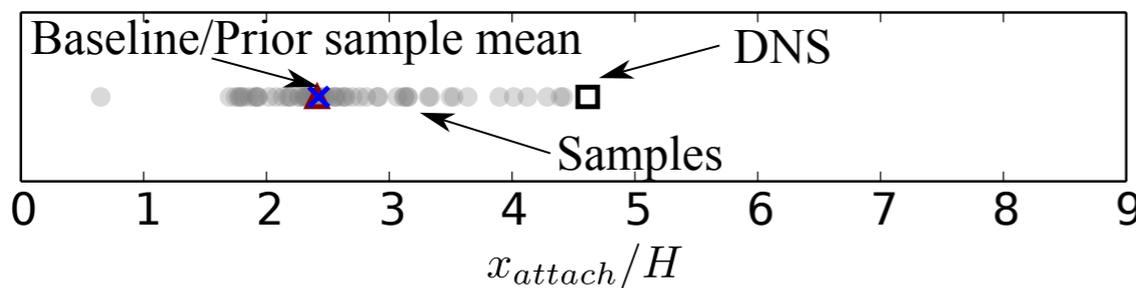
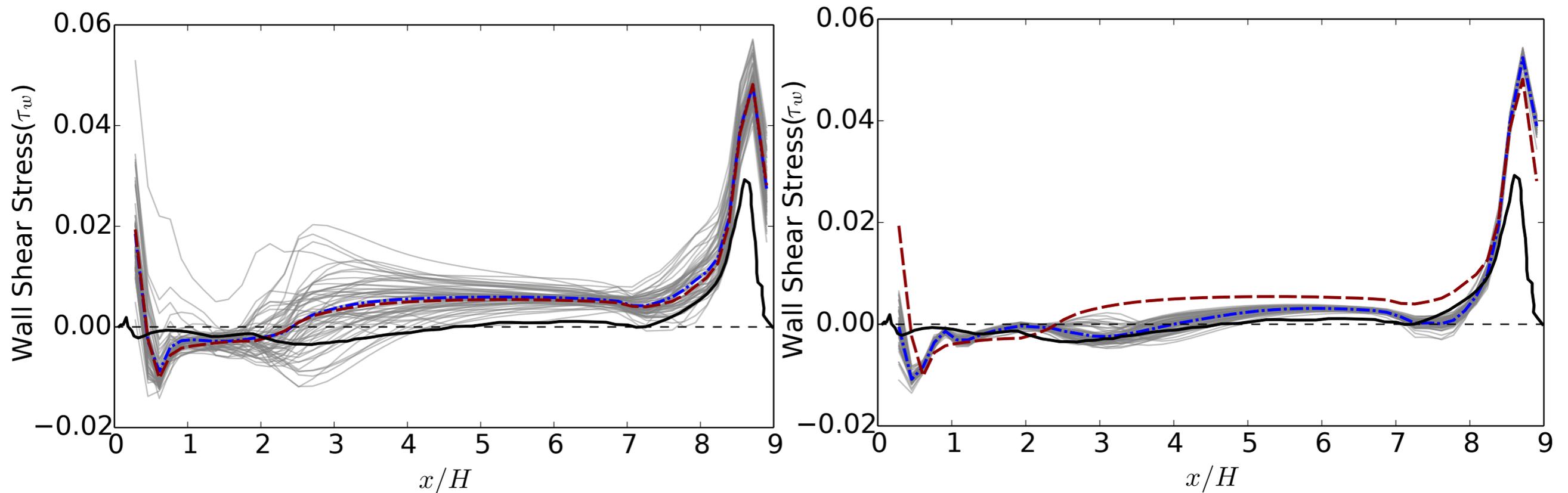
(b) Posterior velocities ensemble

Posterior

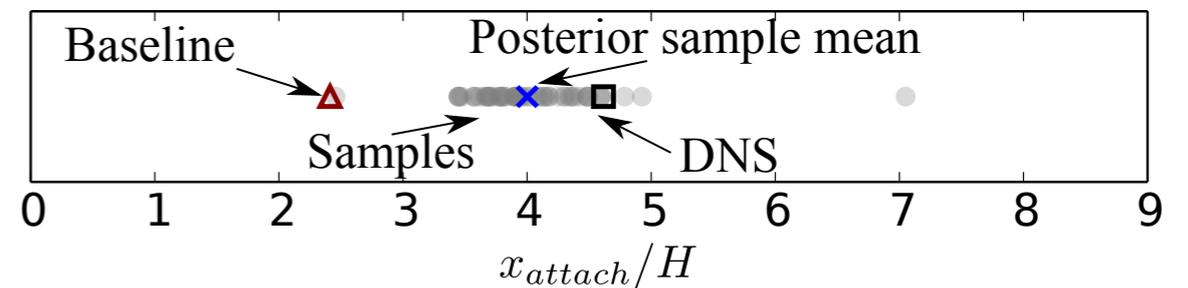


# Prior and Posterior of Other Qols

Qols: Shear stress on bottom wall; reattachment point (obtained by post-processing of velocity field)



(a) Prior ensemble

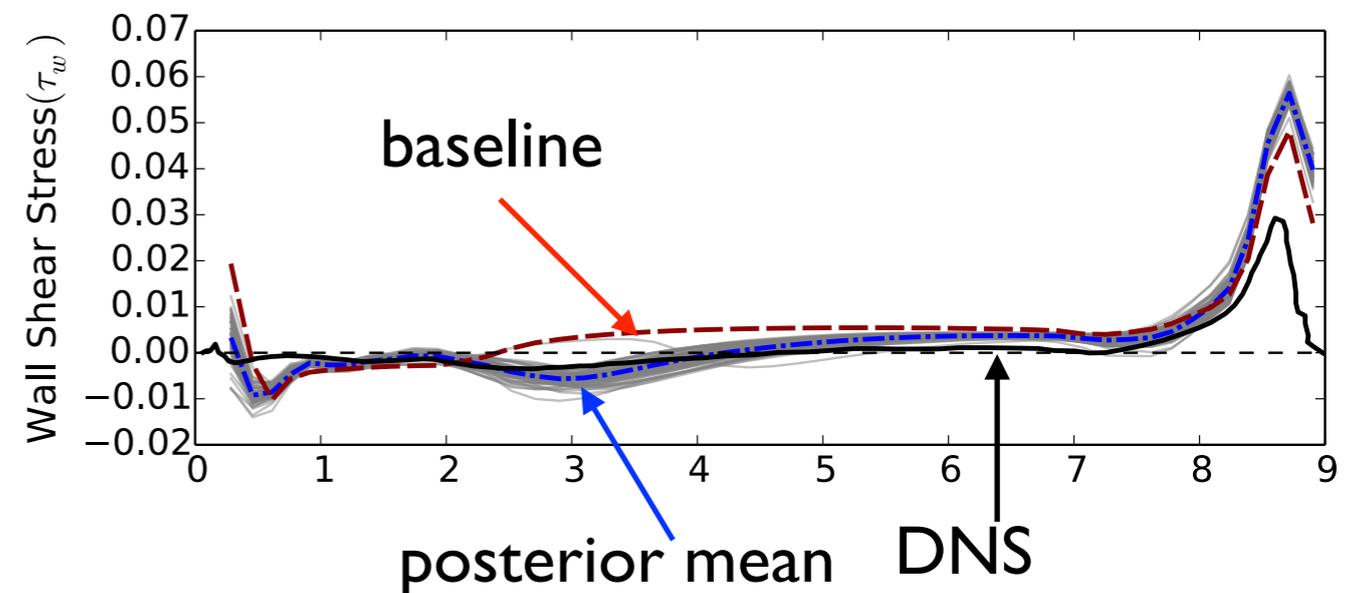
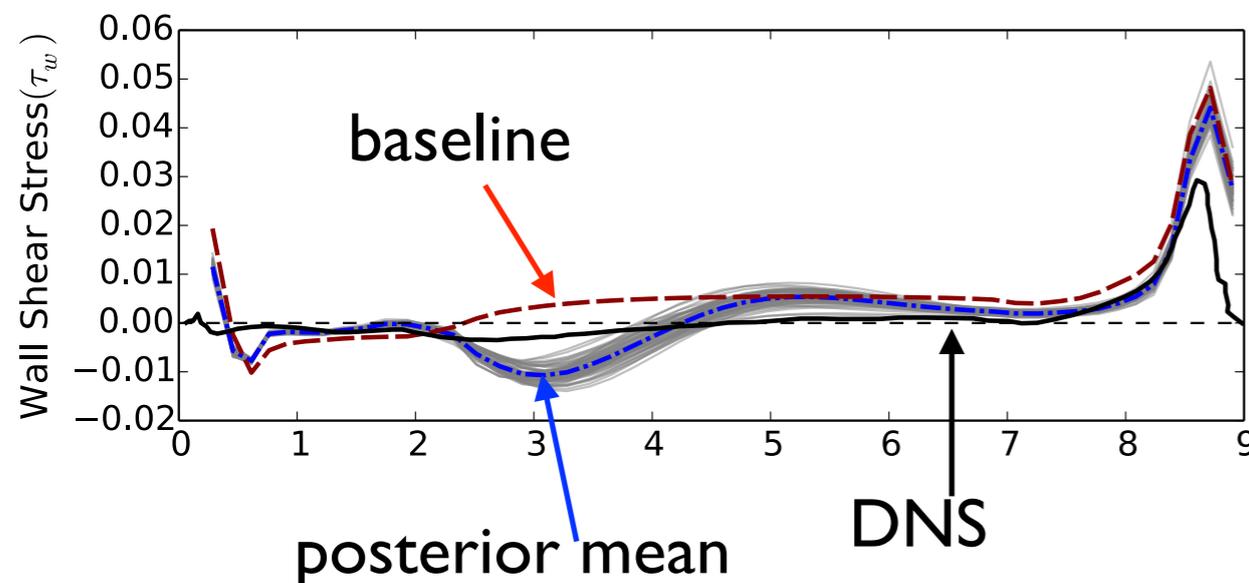
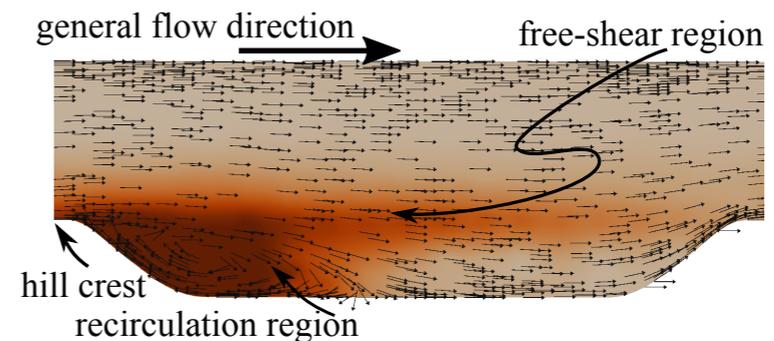


(b) Posterior ensemble

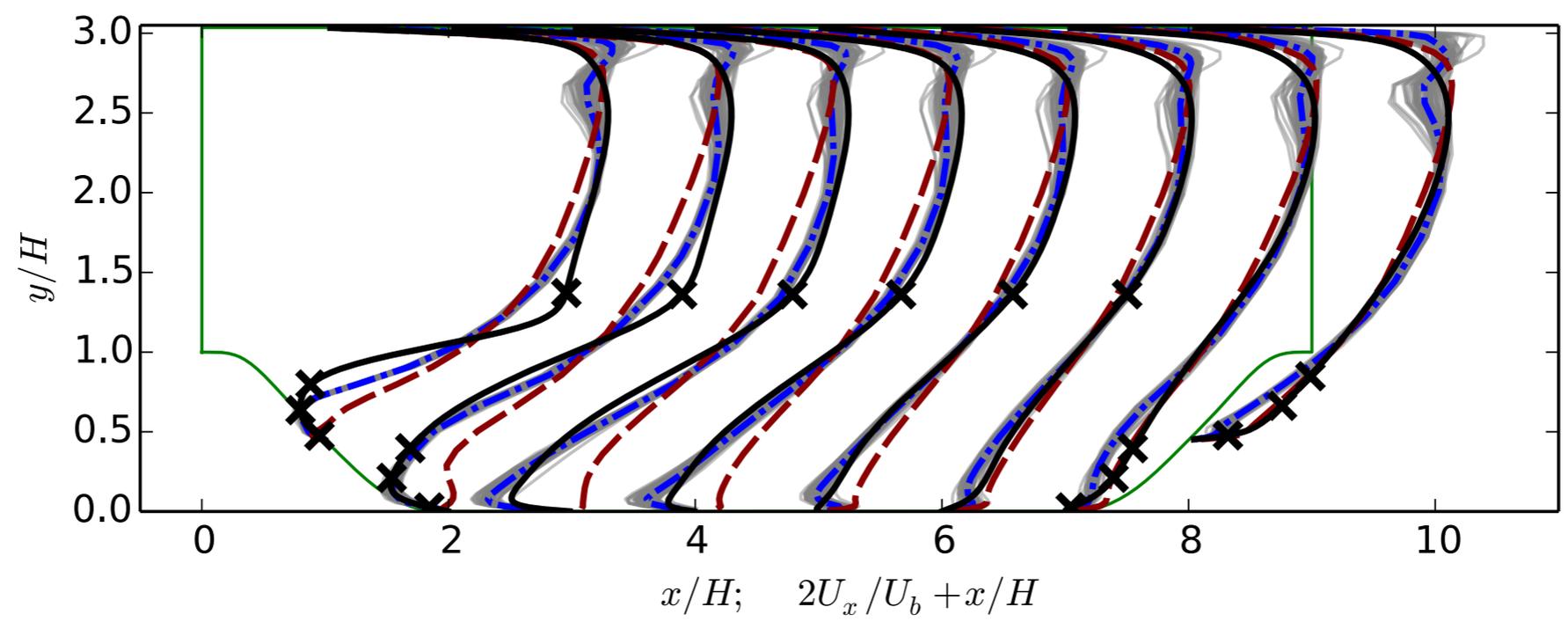
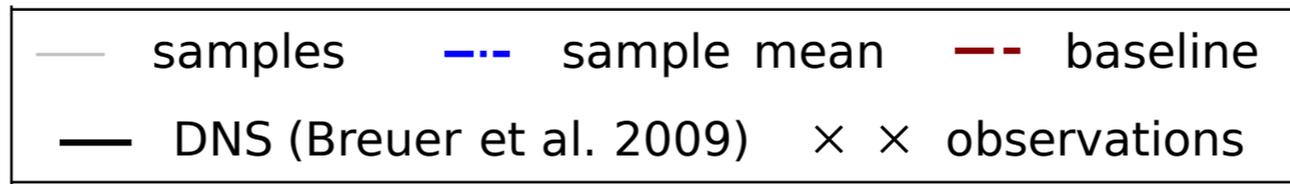
# Effects of Physical Prior Knowledge

- ❖ Prior knowledge helps improving results. (Wang et al. 2015)
- ❖ It is easy to incorporate prior knowledge in the current framework, even for those empirical, imprecise experiences in engineering.

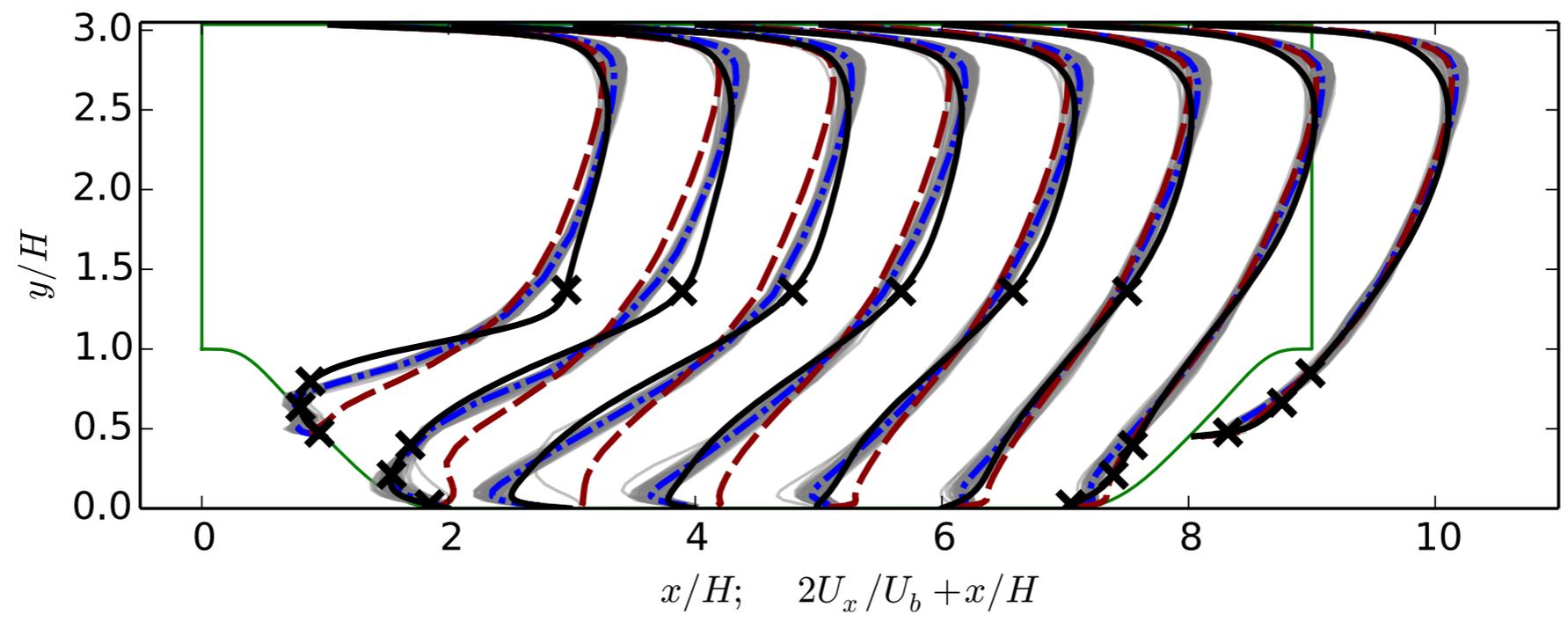
Constant variance  
(no prior knowledge)



[2] J.-X. Wang, J.-L. Wu, and H. Xiao. Incorporating prior knowledge for quantifying and reducing model-form uncertainty in RANS simulations. Submitted to IJUQ, November, 2015.

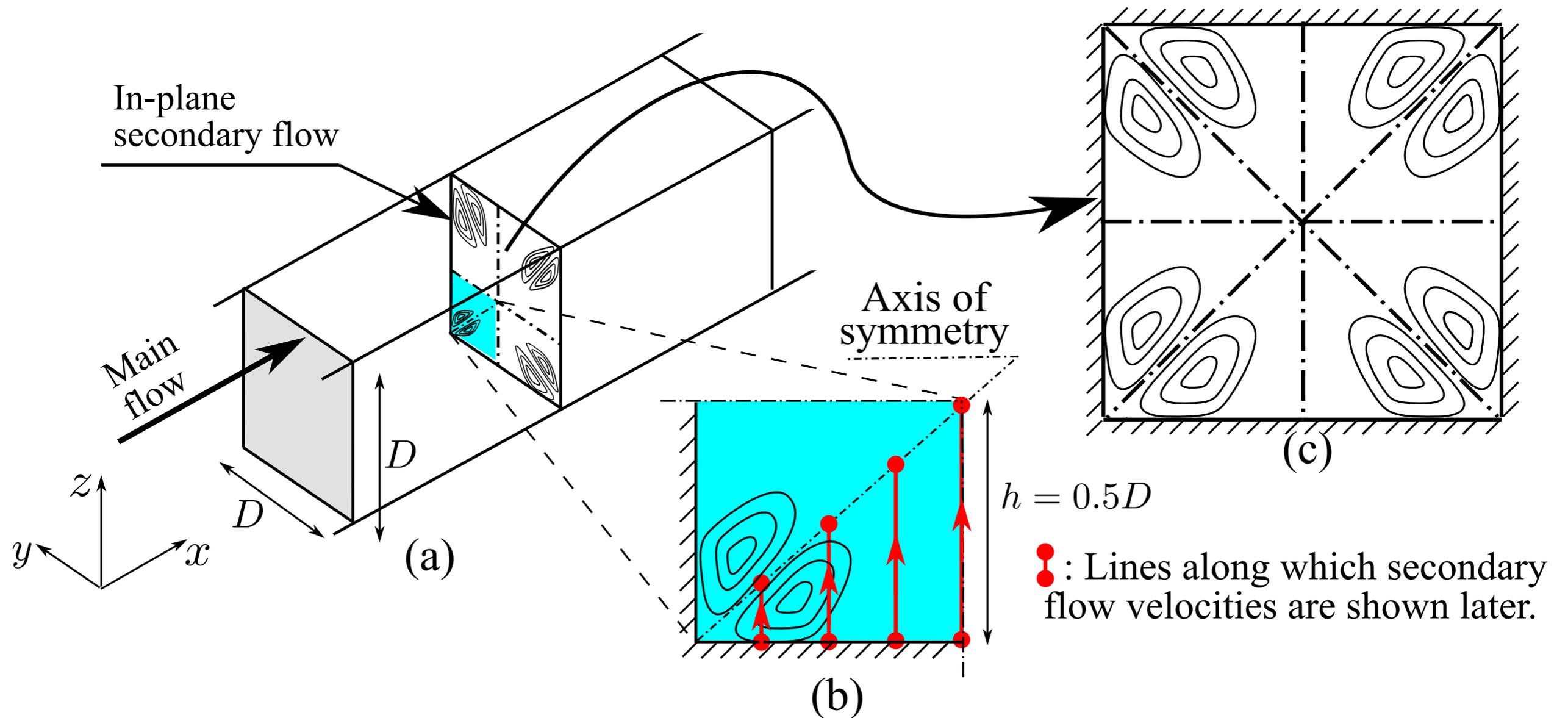


(a)  $U_x$  with non-informative  $\sigma(x)$



(b)  $U_x$  with informative  $\sigma(x)$

# Test Case II: Flow in a Square Duct



The flow features in-plane secondary flow vortices, which cannot be predicted by standard RANS models.

# Prior In-plane velocity:

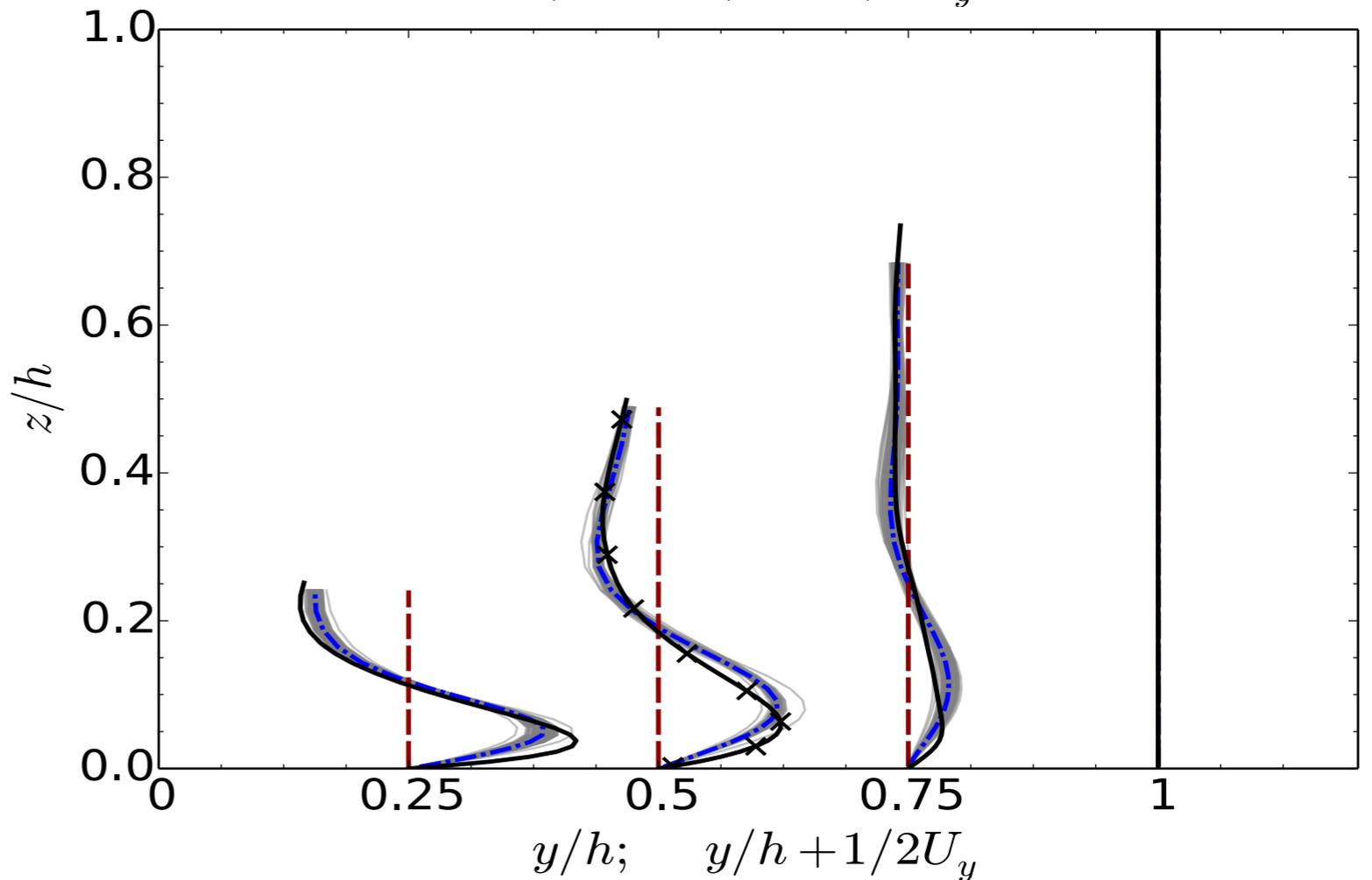
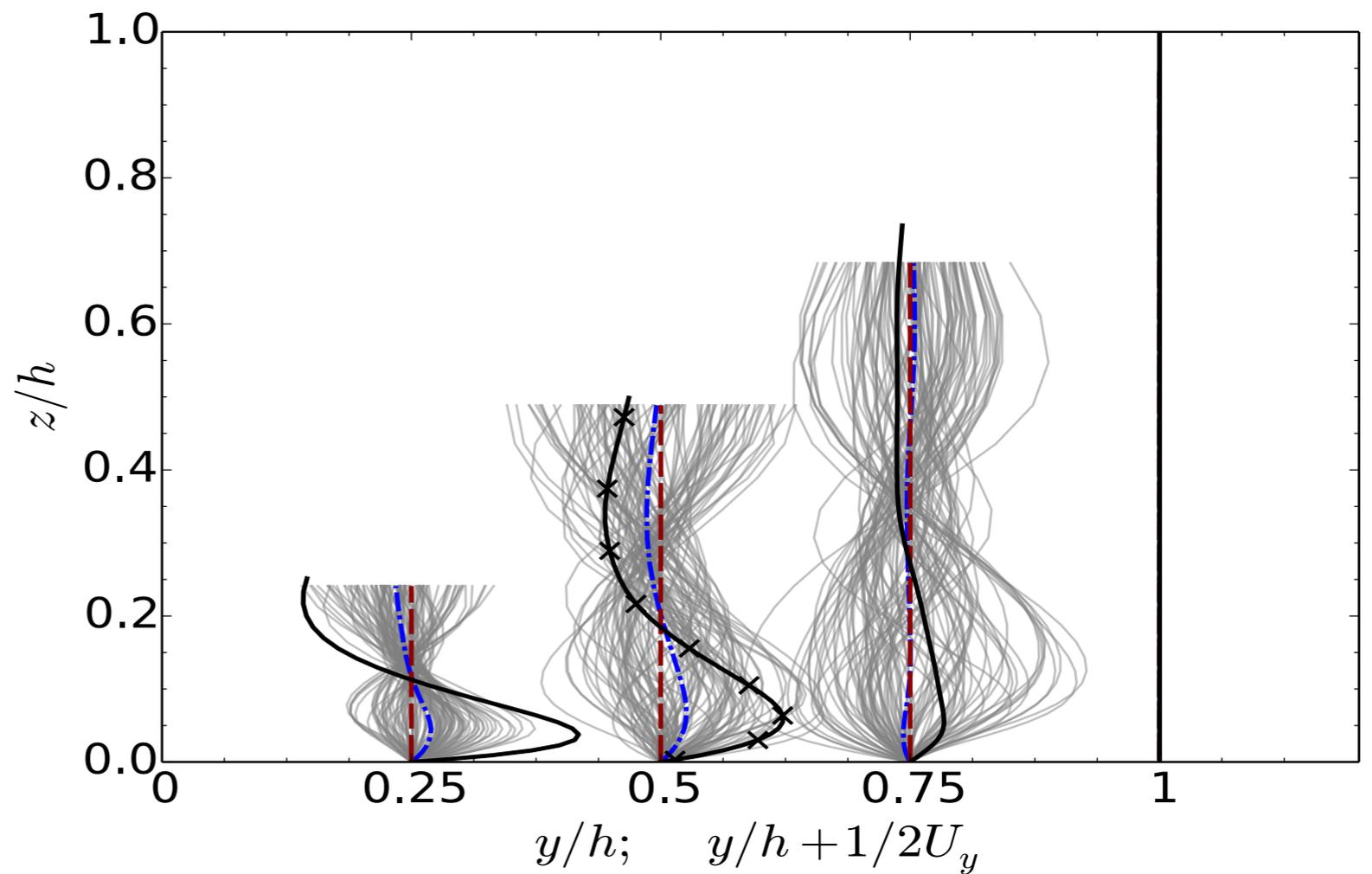
Black: DNS

Red: Baseline RAN

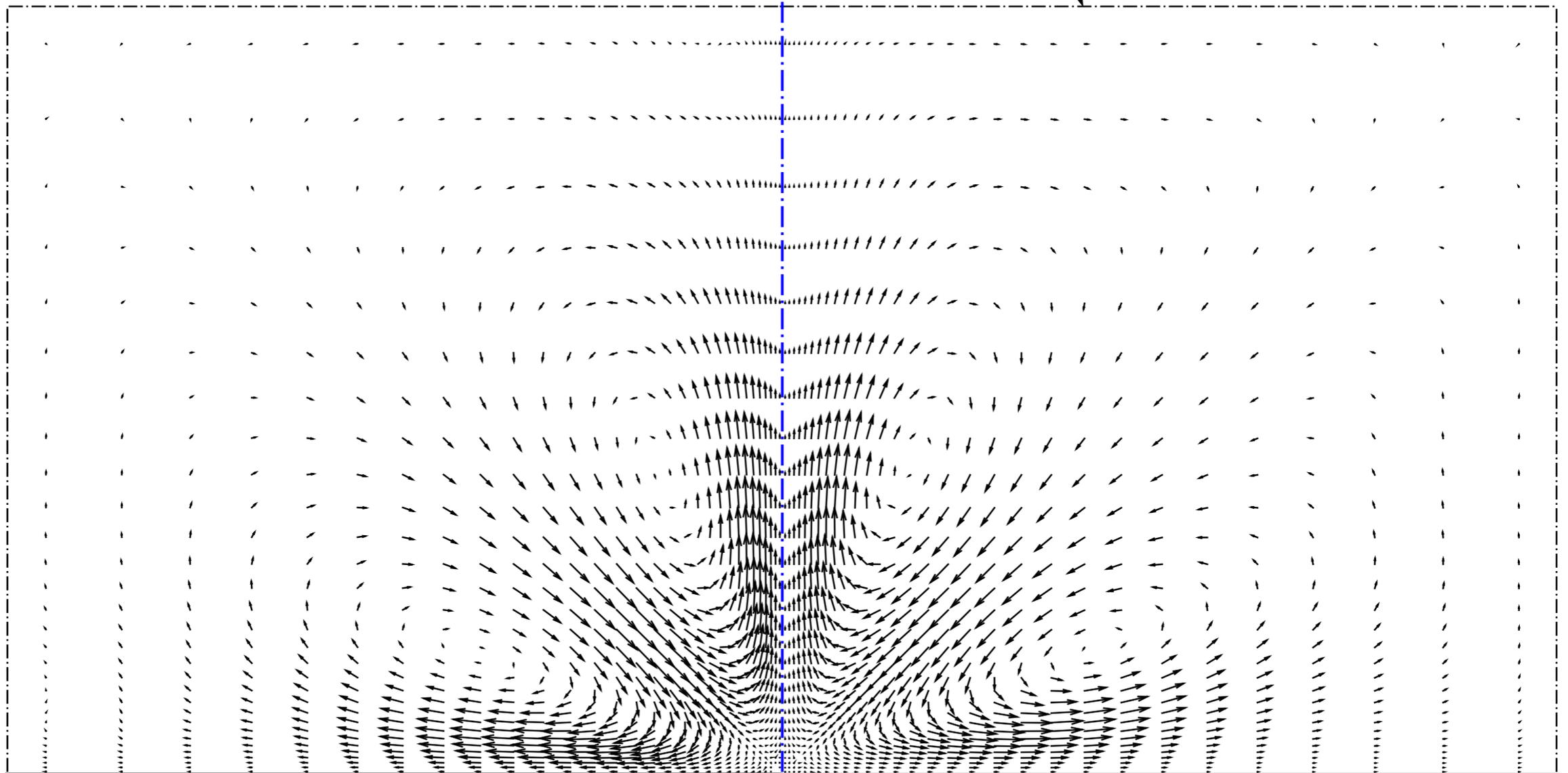
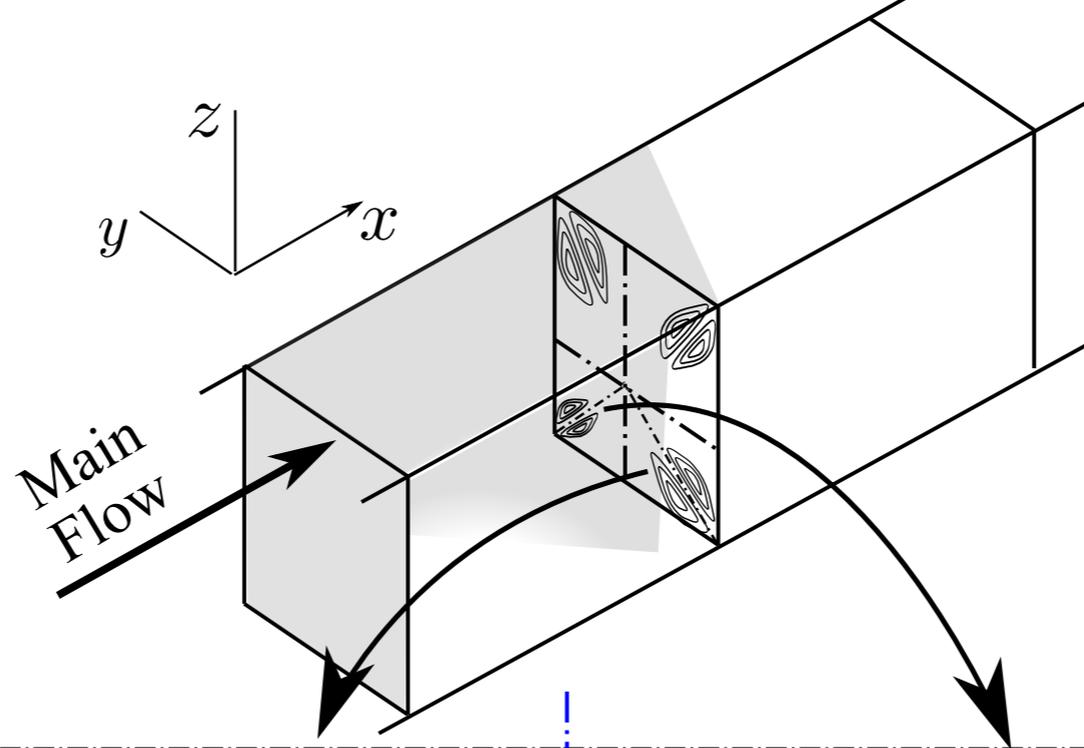
Blue: sample mean

# Posterior In-plane velocity:

Prior scaled by a factor of 0.3 clarity



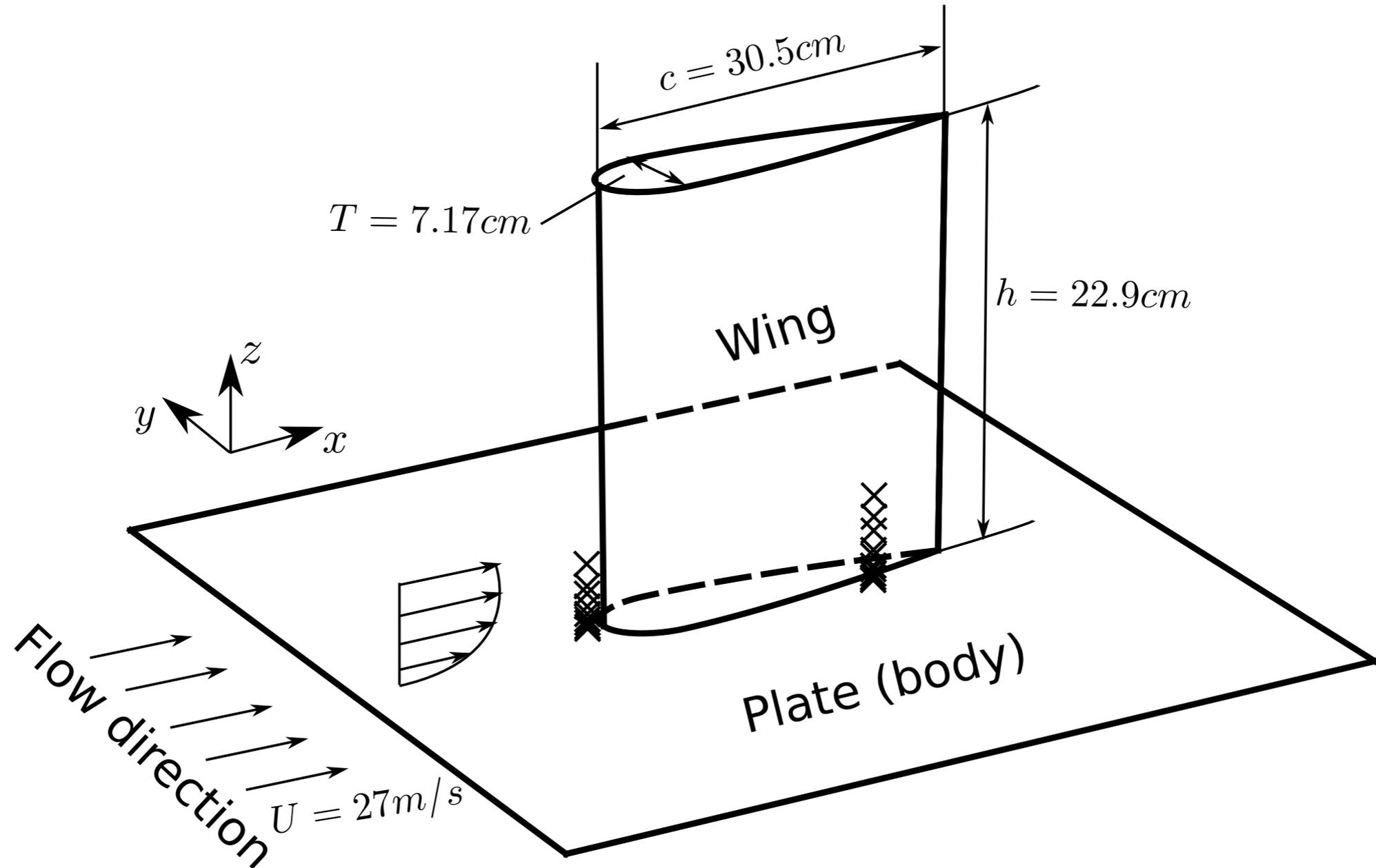
# QoI: In-plane Velocity



DNS

Posterior mean

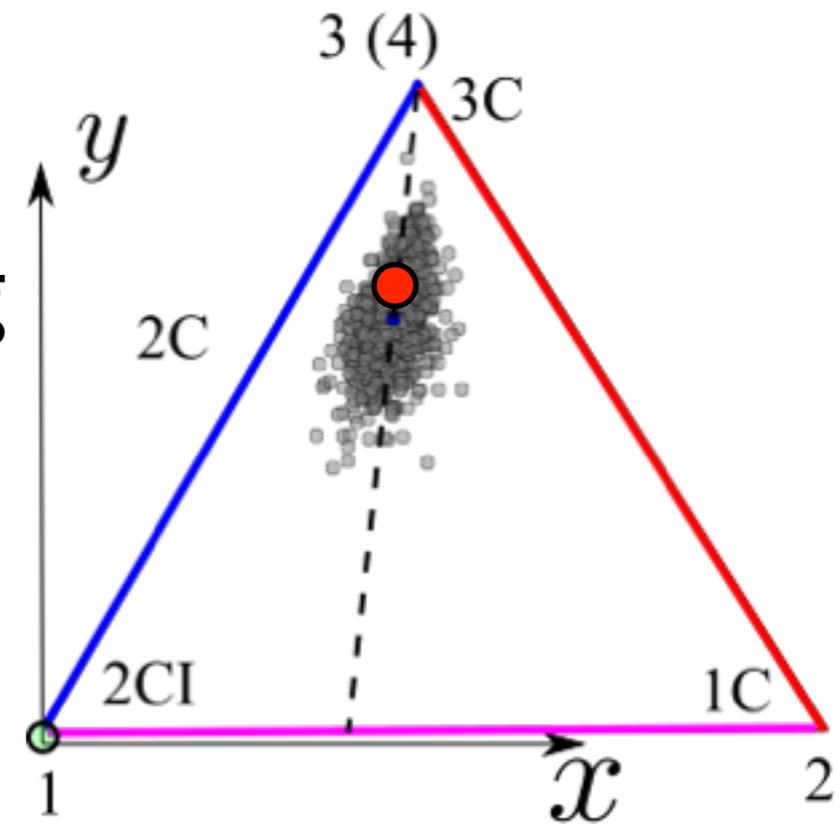
# Test Case III: Wing-Body Junction Flow



[6] Wu, Wang, Xiao. Quantifying Model Form Uncertainty in RANS Simulation of Wing-Body Junction Flow. Submitted to FTC.

# Computational Costs

- ❖ A baseline RANS simulation costs  $T$ . Each solve with perturbed Reynolds stress costs  $0.1T$  (since we are starting at converged velocities in the baseline).
- ❖ 60 samples x 10 Kalman iterations = 600 forward evaluations
- ❖ Total computation CPU hours is  $600 \times 0.1T = 60T$
- ❖ Samples evaluations are embarrassingly parallel: can run simultaneously on 60 processors. The wall time is still  $T$ !



# Two Scenarios of Industrial CFD Simulations

- ❖ Monitoring / Forecasting
- ❖ **Support Design/Optimization**

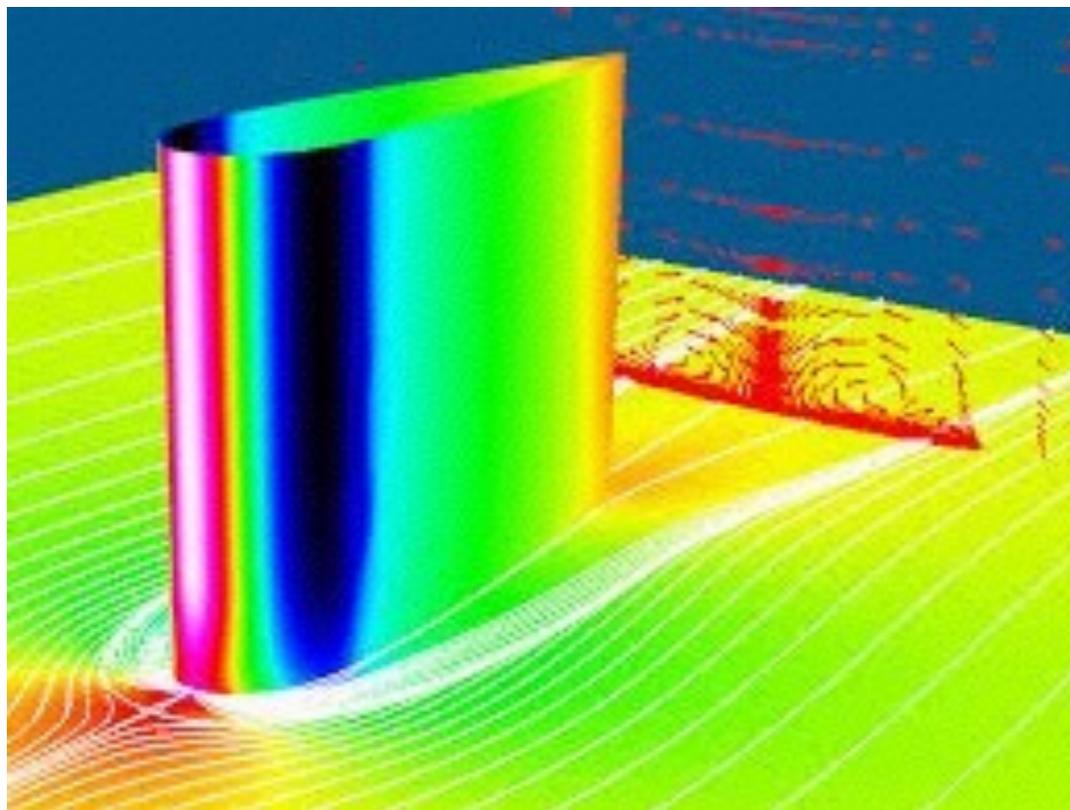
# What If There Are No Data Available?

- ❖ Typical design cycle in civil aviation
- ❖ During engineering design (airplane etc.), the system has not been built yet: no data available!
- ❖ However, data may be available at a down-scaled model at a lower Reynolds number, or from a previous models of the same product line.

# Vision for CFD in Support of Engineering Design and Optimization

## Calibration Cases (w/ data)

A few configuration with data (DNS or measurements)

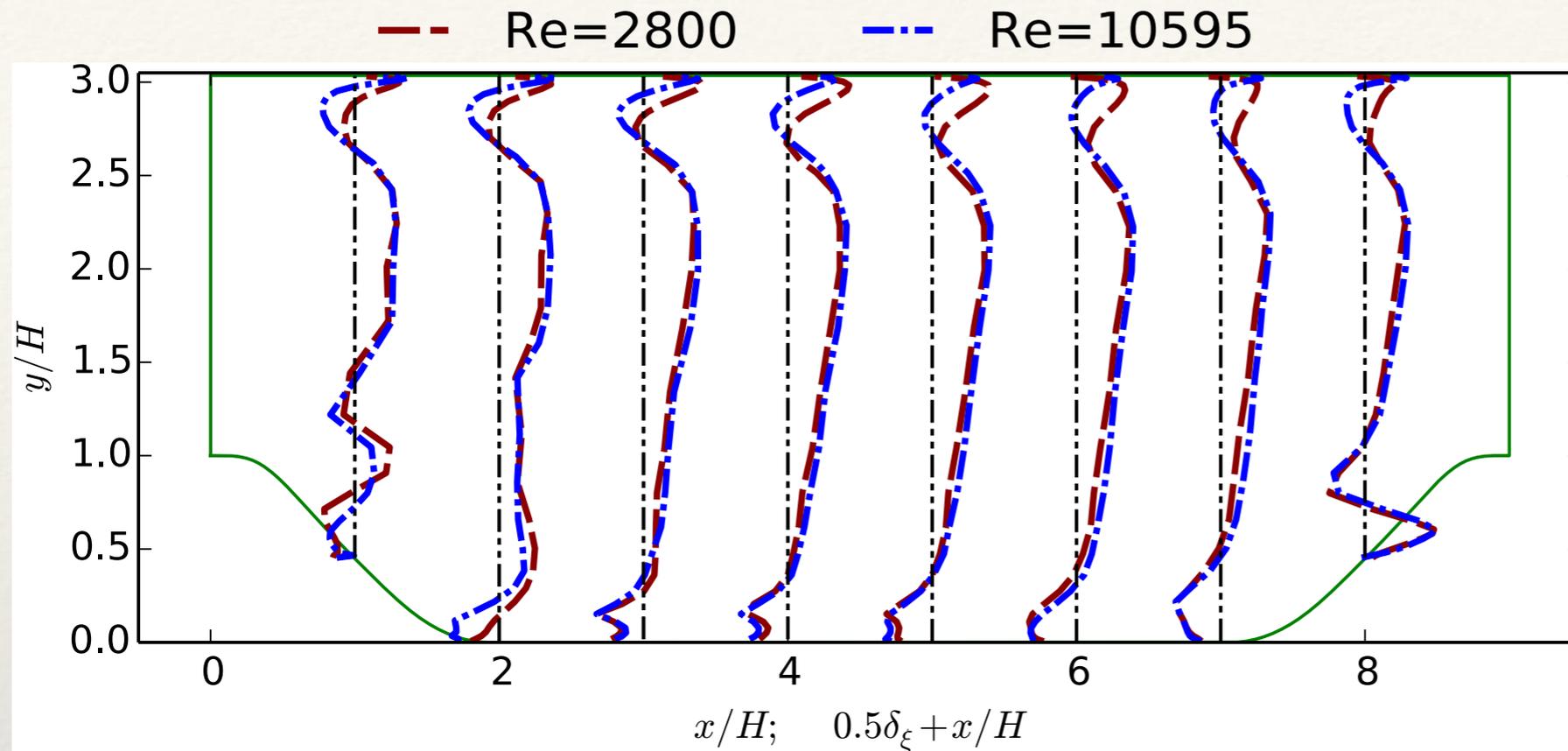


## Prediction Cases (w/o data)

Similar configuration with different:

- Twist
- Sweep angles
- Airfoil shape

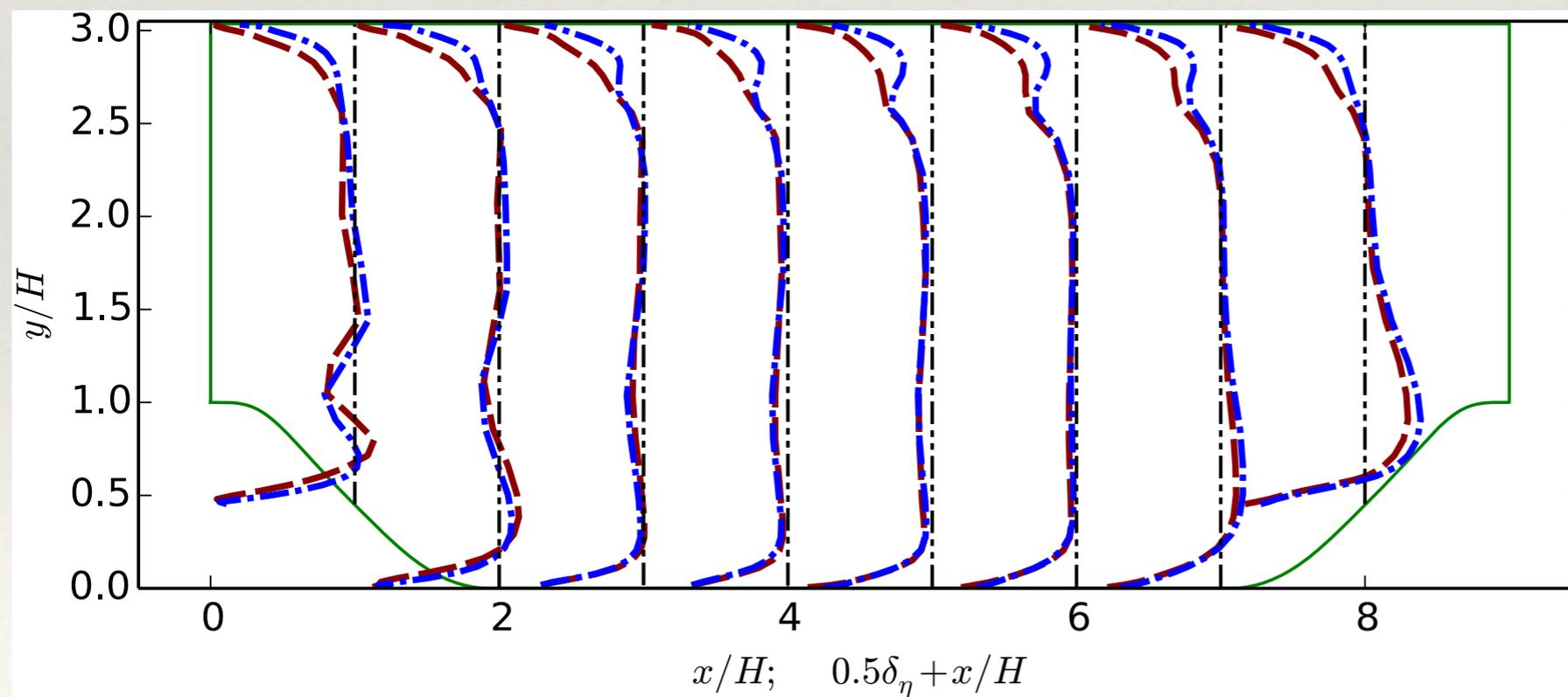
# Is The Discrepancy of Anisotropy Universal?



Probably!

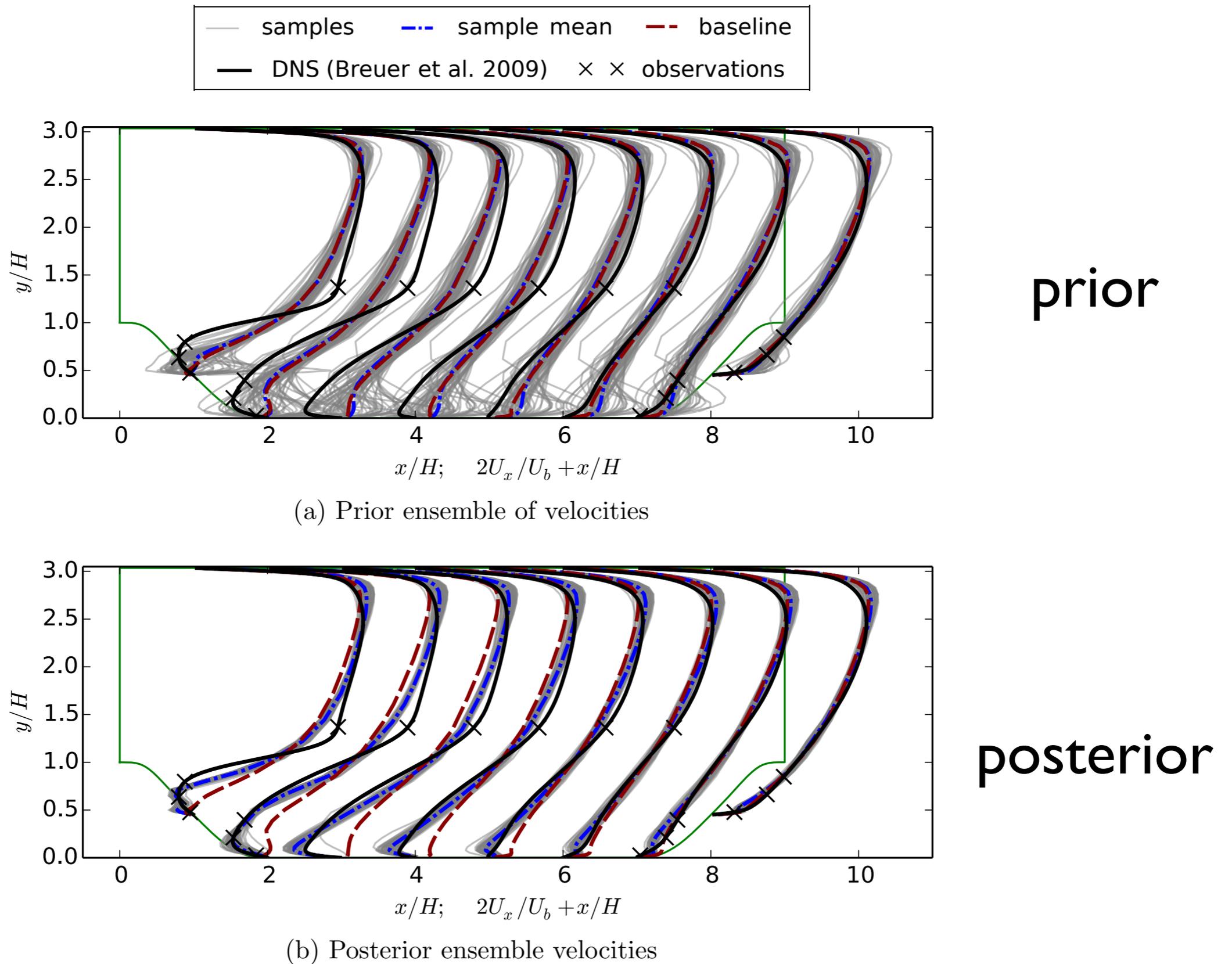
$\delta_\xi$

$\delta_\eta$



[3] J.-L. Wu, J.-X. Wang, and H. Xiao. A Bayesian calibration-prediction method for reducing model-form uncertainties with application in RANS simulations. *Flow, Turbulence and Combustion*, 2016.

# Calibration at $Re = 2800$ (with Data)



# Prediction at $Re=10595$ (No Data)

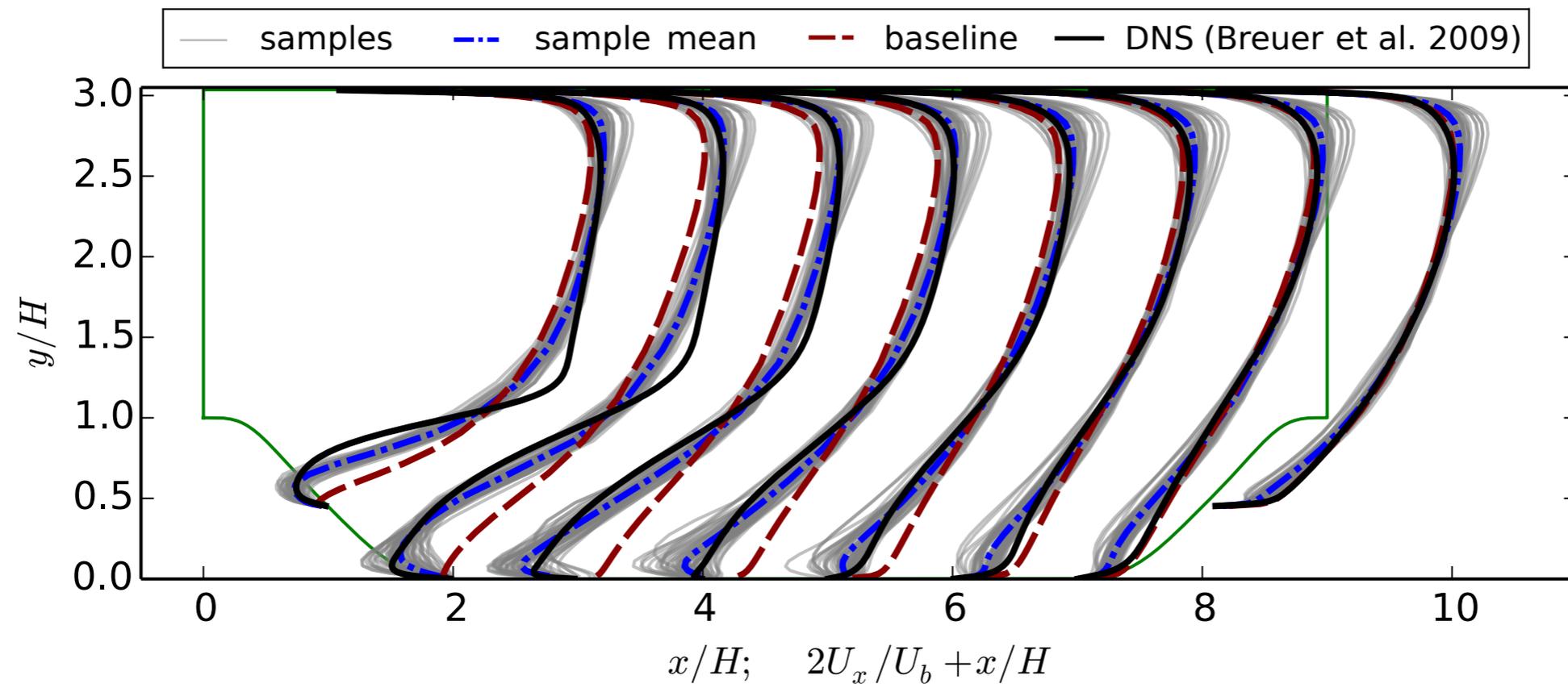
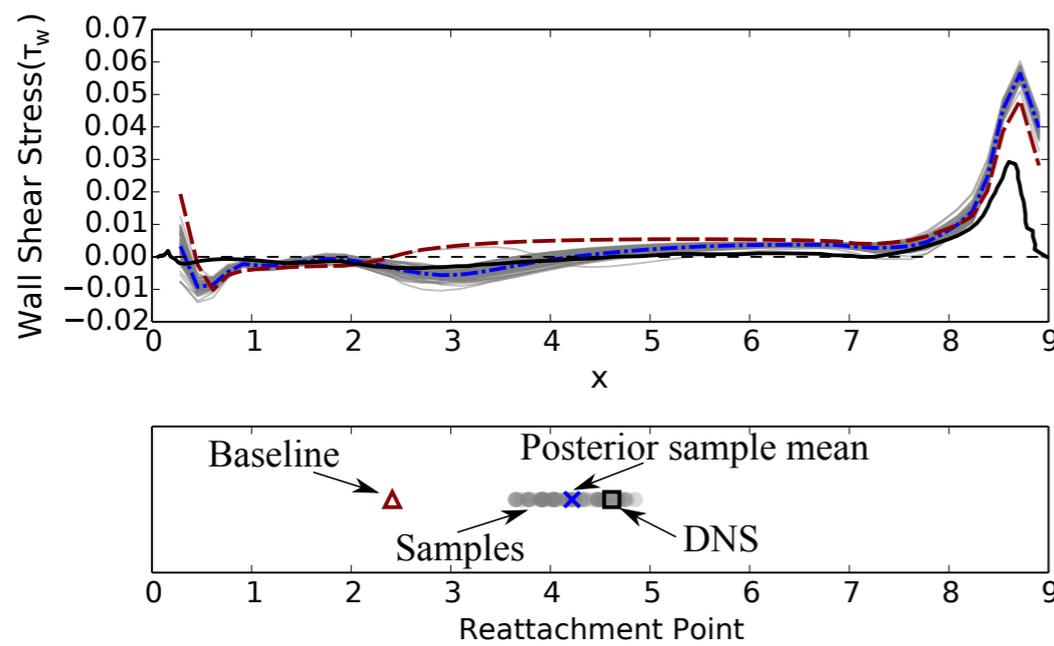
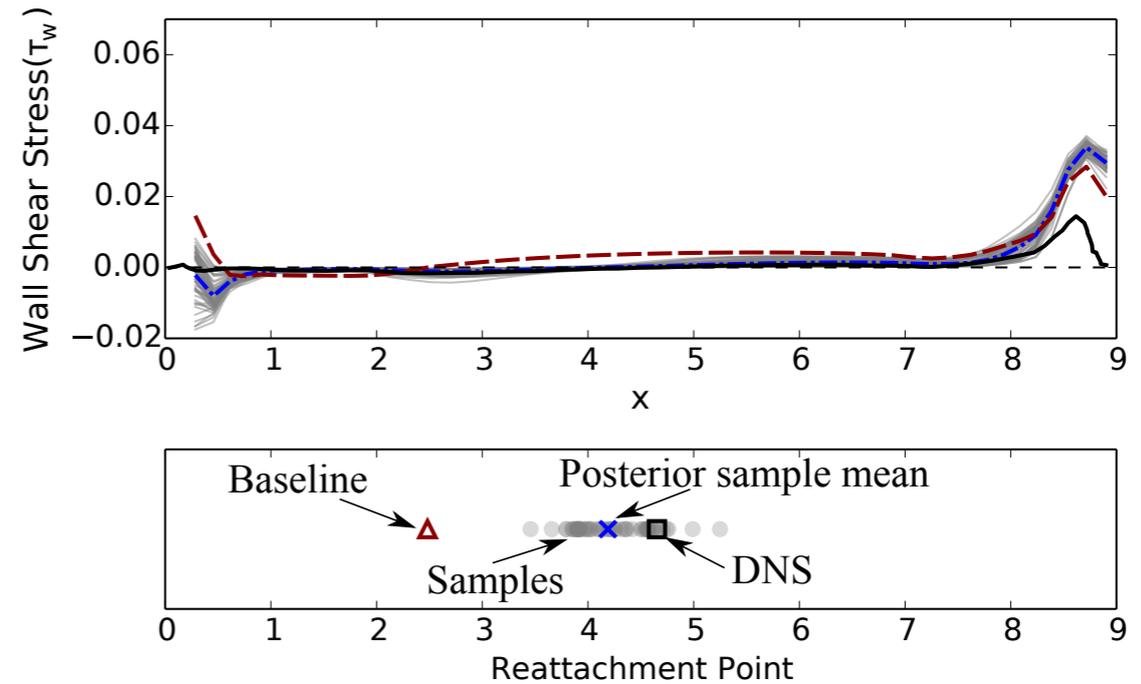


Figure 7: Ensemble of predicted velocity profiles of the flow over periodic hills of  $Re = 10595$  at eight streamwise cross-sections  $x/H = 1, 2, \dots, 8$  compared with benchmark data and baseline results.

- ❖ Predictions still good even without data.



(a) Calibration of  $Re = 2800$



(b) Prediction of  $Re = 10595$

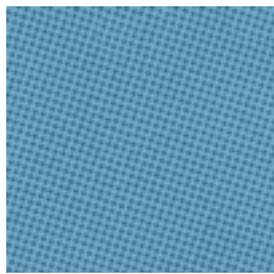
— samples    - - - sample mean    - - - baseline    — DNS

Figure 5: The wall shear stress  $\tau_w$  and reattachment point  $x_{attach}$  of flow over periodic hills of  $Re=10595$ . The extent of negative wall shear stress indicates the length of recirculation zone. The reattachment point is determined by the change of wall shear stress from negative to positive, which also indicates the end of recirculation zone. The greater opacity of markers indicates that there are more samples.

## ❖ Improvements for the predicted case.

# Another Illustrative Example

- ❖ Example for illustration: Calibrate Reynolds stress discrepancy in flow in square duct at  $Re = 10^4$ ; Predict: (1) a flow at higher Reynolds numbers and (2) a flow in a rectangular duct.



calibration:  
square duct flow  
@ low  $Re$



prediction:  
square duct flow  
high  $Re$

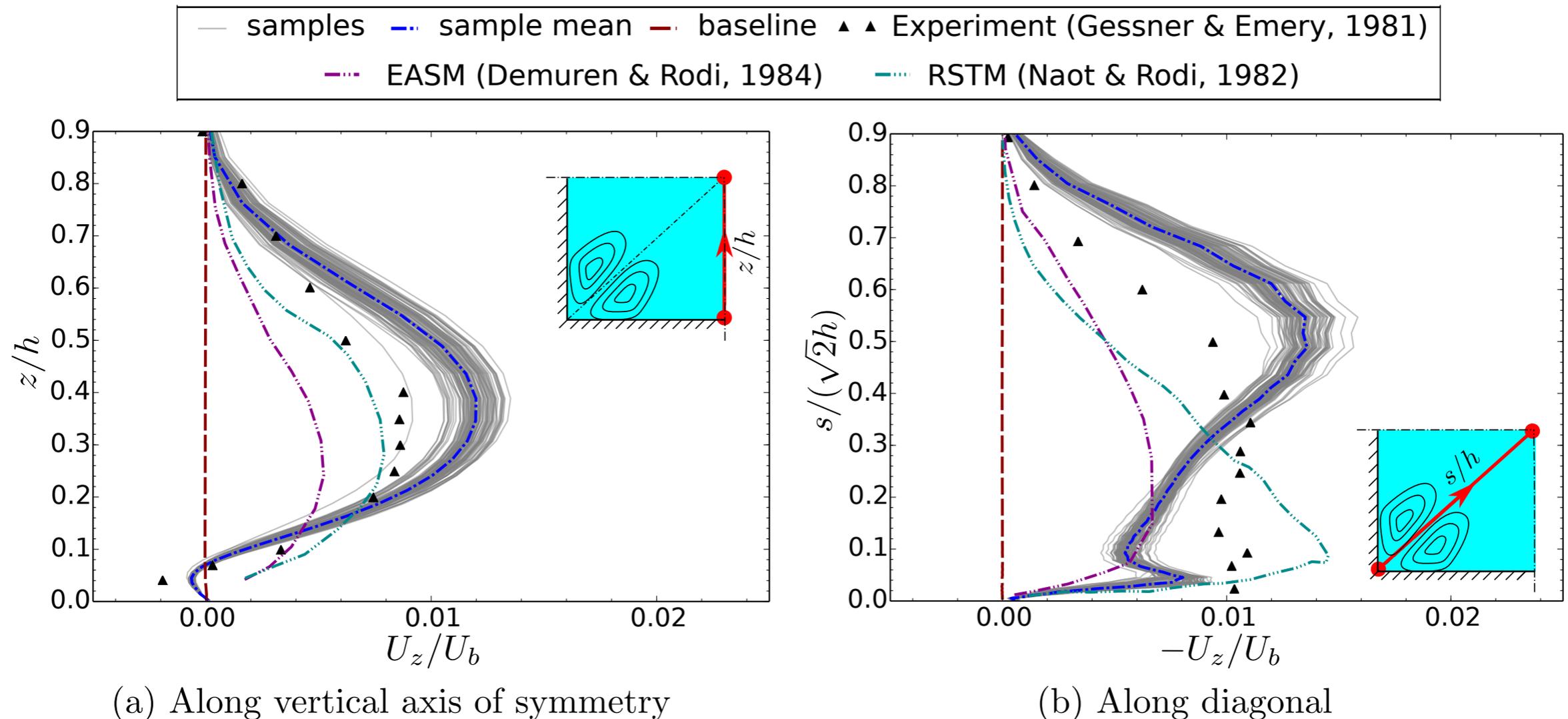


prediction:  
rectangular duct  
flow @ high  $Re$

J.-L. Wu, J.-X. Wang, and H. Xiao. A Bayesian calibration-prediction method for reducing model-form uncertainties with application in RANS simulations. *Flow, Turbulence and Combustion*, 2016.

# Prediction at High Reynolds Numbers

**Calibrate** Reynolds stress discrepancy at  $Re = 1 \times 10^4$ ;  
**Extrapolate** discrepancy to predict for  $Re = 2.5 \times 10^5$



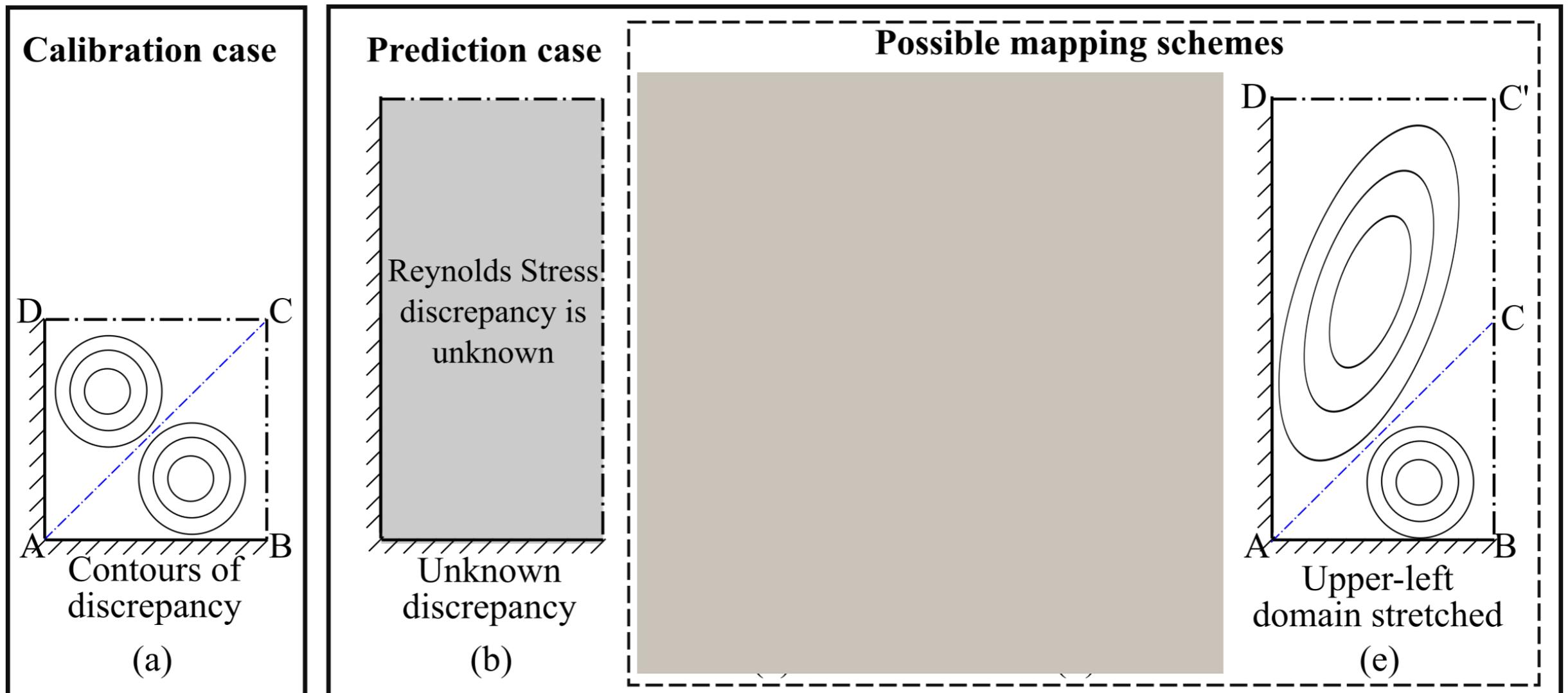
(a) Along vertical axis of symmetry

(b) Along diagonal

Figure 12: The comparison of predicted secondary velocity  $U_z$  at Reynolds number  $Re = 2.5 \times 10^5$  with experimental data (denoted as  $\blacktriangle$ ) and with predictions from advanced turbulence models including an explicit algebraic Reynolds stress model (EASM) and a Reynolds stress transport model (RSTM). Comparisons are shown (a) along the vertical axis of symmetry and (b) along the diagonal. Note that the prediction does not utilize observation data from the flow at  $Re = 2.5 \times 10^5$ .

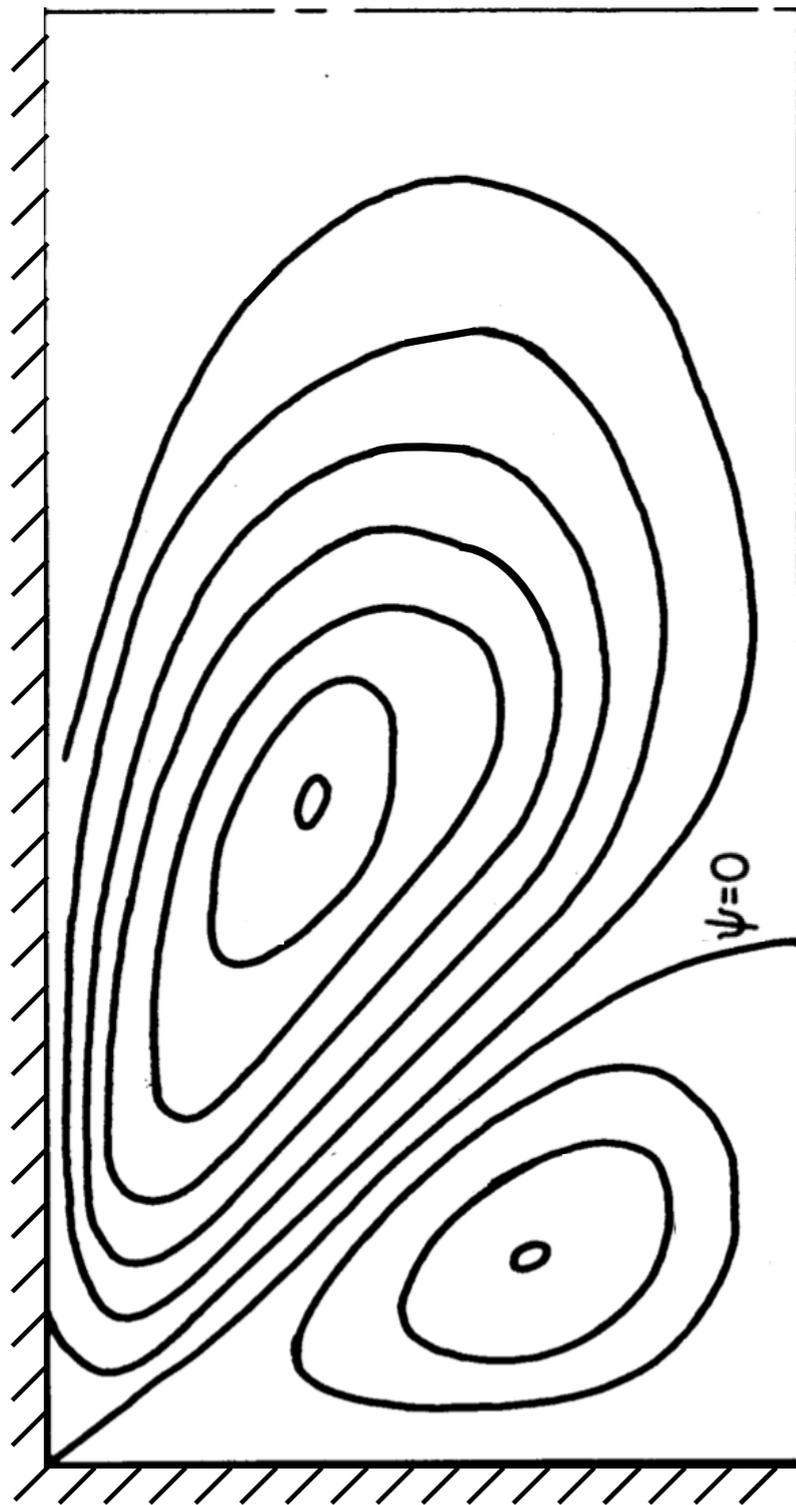
# Extrapolation to Flow in a Different Geometry

The flow to be predicted has a different Reynolds number and different geometry than the calibration case.

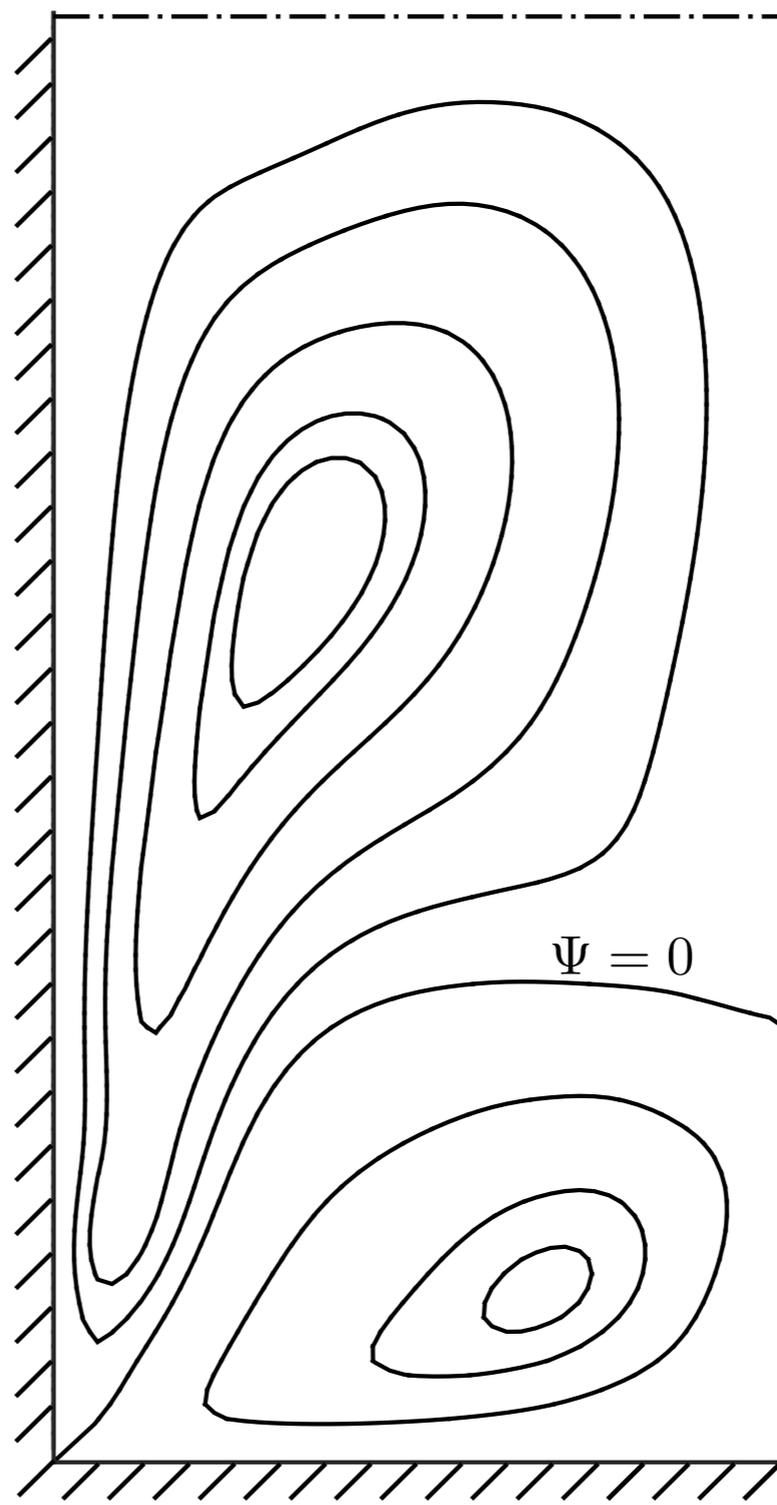


J.-L. Wu, J.-X. Wang, and H. Xiao. A Bayesian calibration-prediction method for reducing model-form uncertainties with application in RANS simulations. *Flow, Turbulence and Combustion*, 2016.

# Predicted Streamlines



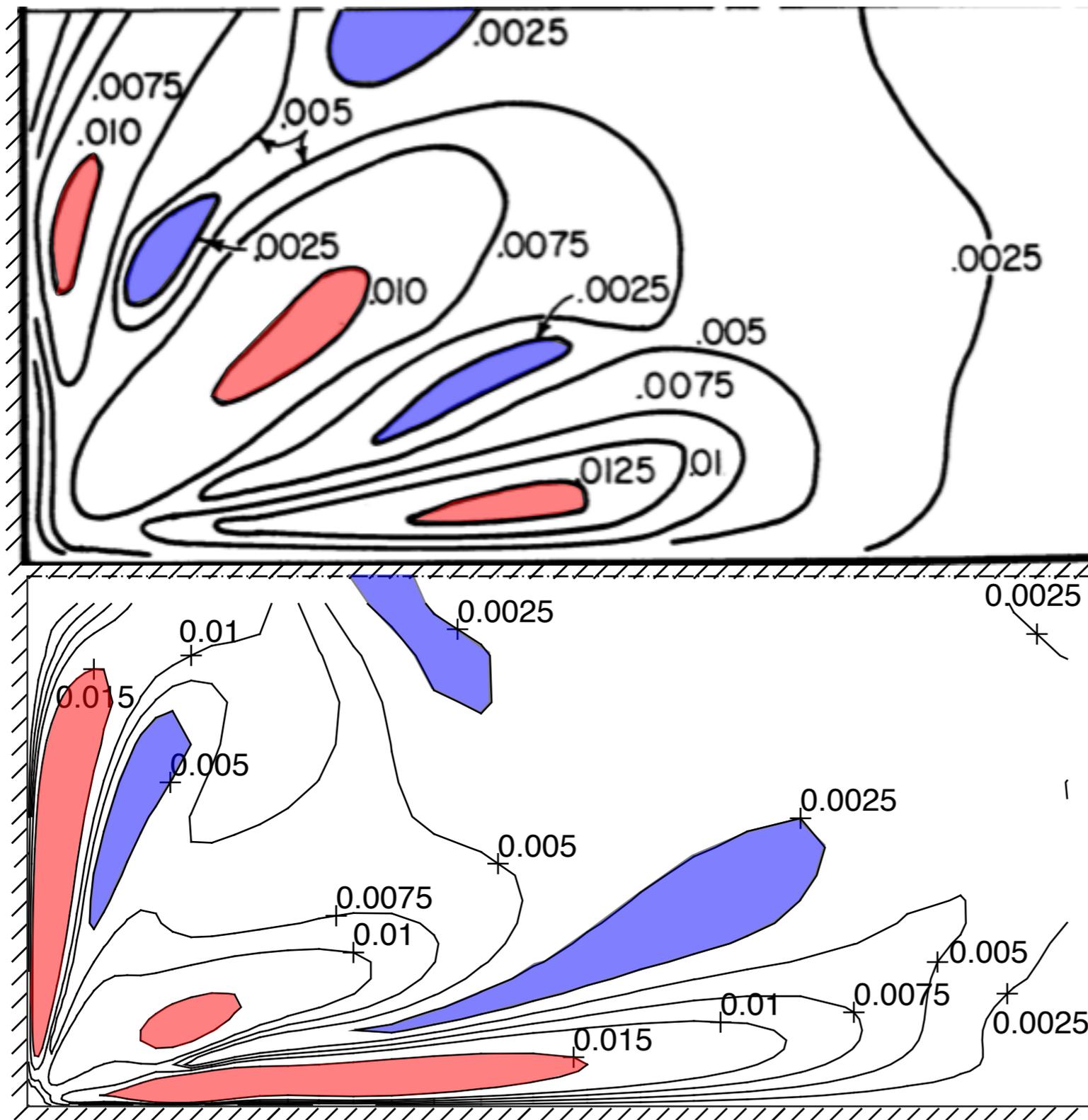
(a) Experiment [28]



(d) Scheme 3

(predicted  
posterior  
mean)

# Predicted Secondary Flow Velocity Magnitude



Red: Peaks

Blue: Troughs

# Assessment of Current Framework

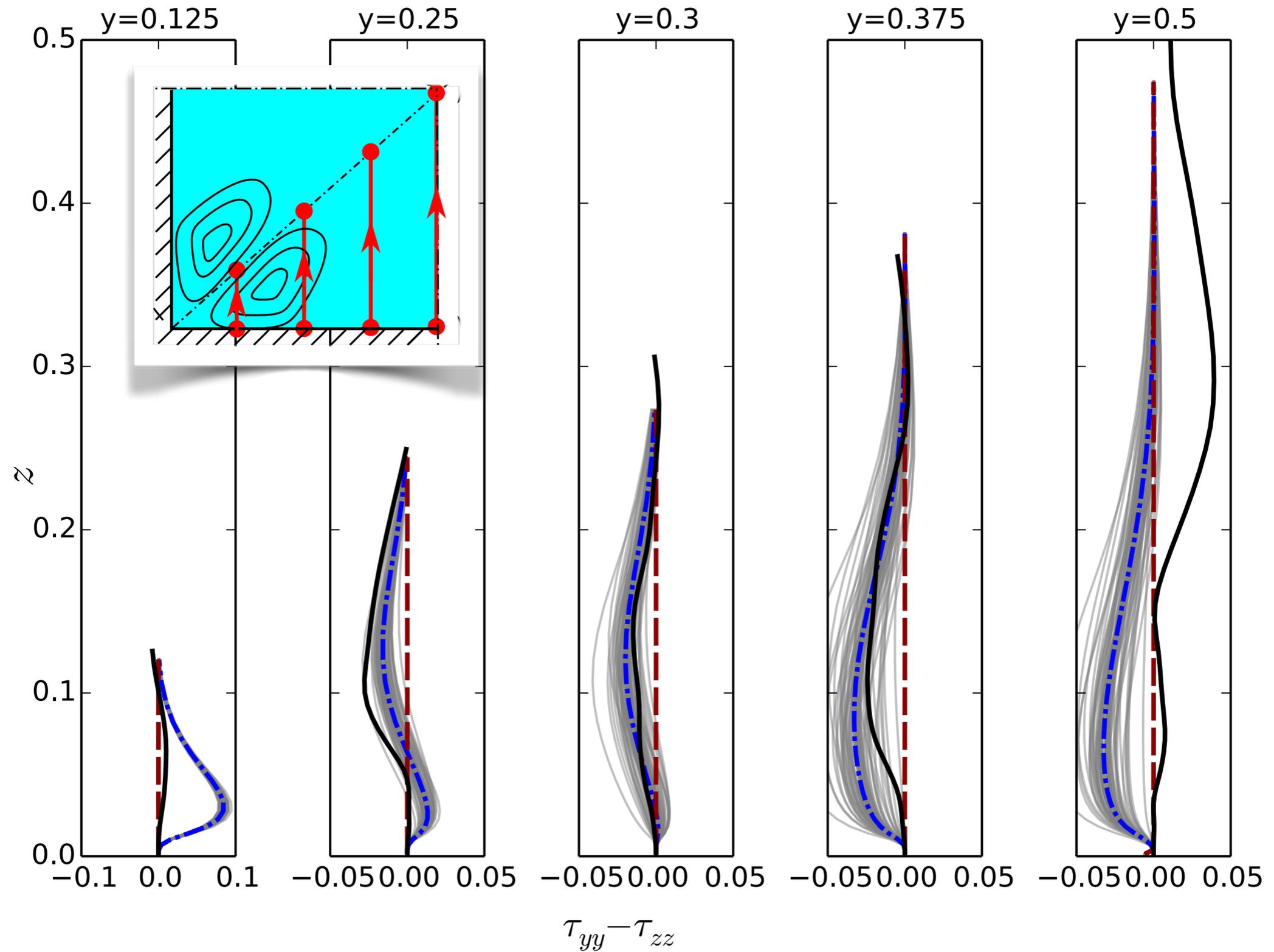
- + Bayesian inference utilizes disparate sources of information: physical constraints / empirical prior knowledge, observation data, and **numerical model**.
- + *Same formulation for different turbulence models: directly perturb Reynolds stresses.*
- + *Not constrained by the Boussinesq assumption.*
- + Inferred quantities (Reynolds stress) are physical and can be validated against benchmark. **We would know when we are wrong**, in contrast to inferring  $\beta(x)$ .

*Inherited from  
laccarino et al.*

# Assessment of Current Framework

- +/- Has the potential for extrapolation to different flows (preliminary success shown; more work ongoing).
- – In currently assumed scenario (very sparse velocity data), inferred Reynolds stress are not accurate. **But: a projection on a manifold is correct; possible to obtain accurate Reynolds stresses if given more data!**
- \* Adjoint model (as opposed to Ensemble Kalman filtering) may help retrieving better Reynolds stress.

# Reynolds Stress Imbalance



# Summary

- We developed a data-driven, physics-informed, Bayesian framework to quantify uncertainties in RANS models.
- The Bayesian framework incorporate all sources of information: **physical constraints + empirical prior knowledge, observation data, and numerical model.**
- Extended to cases without observation data (by extrapolating the inferred Reynolds stress discrepancy from a case with observation data).

Thank you for your attention!  
Questions!