

# **DNS of Roughness-Induced Transition in the Boundary Layer of a Hypersonic Spherical Forebody**

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Chair of Aerodynamics and Fluid Mechanics  
Technical University of Munich

# Motivation



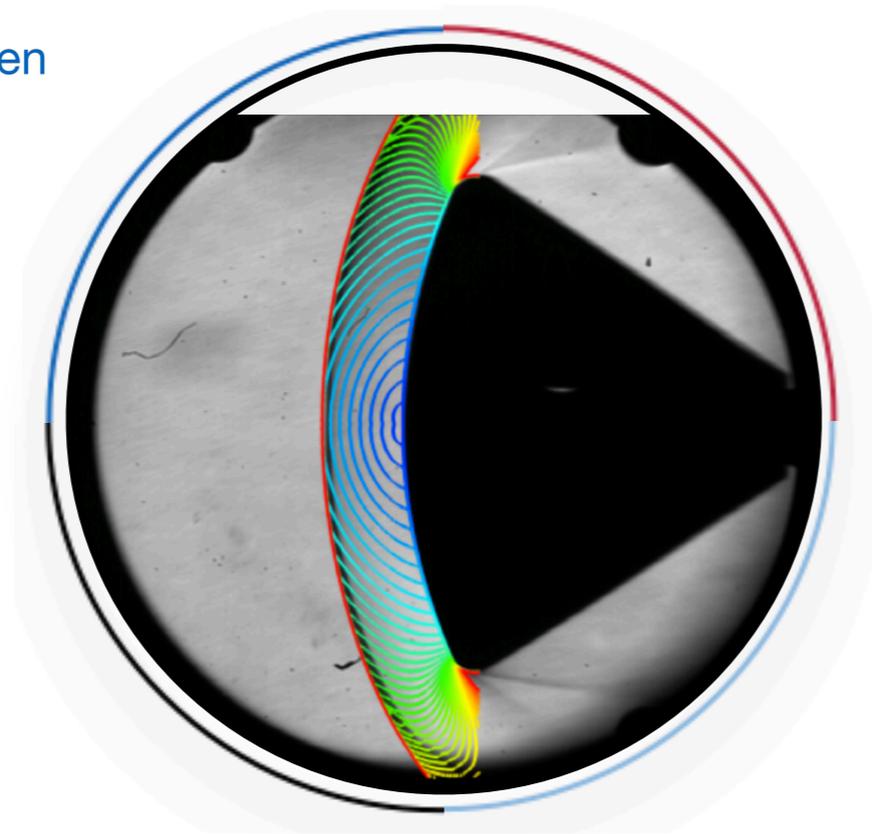
Apollo 12 Command Module,  
Virginia Air & Space Center



# Project: Transition on Capsule Configurations



Technische Universität München



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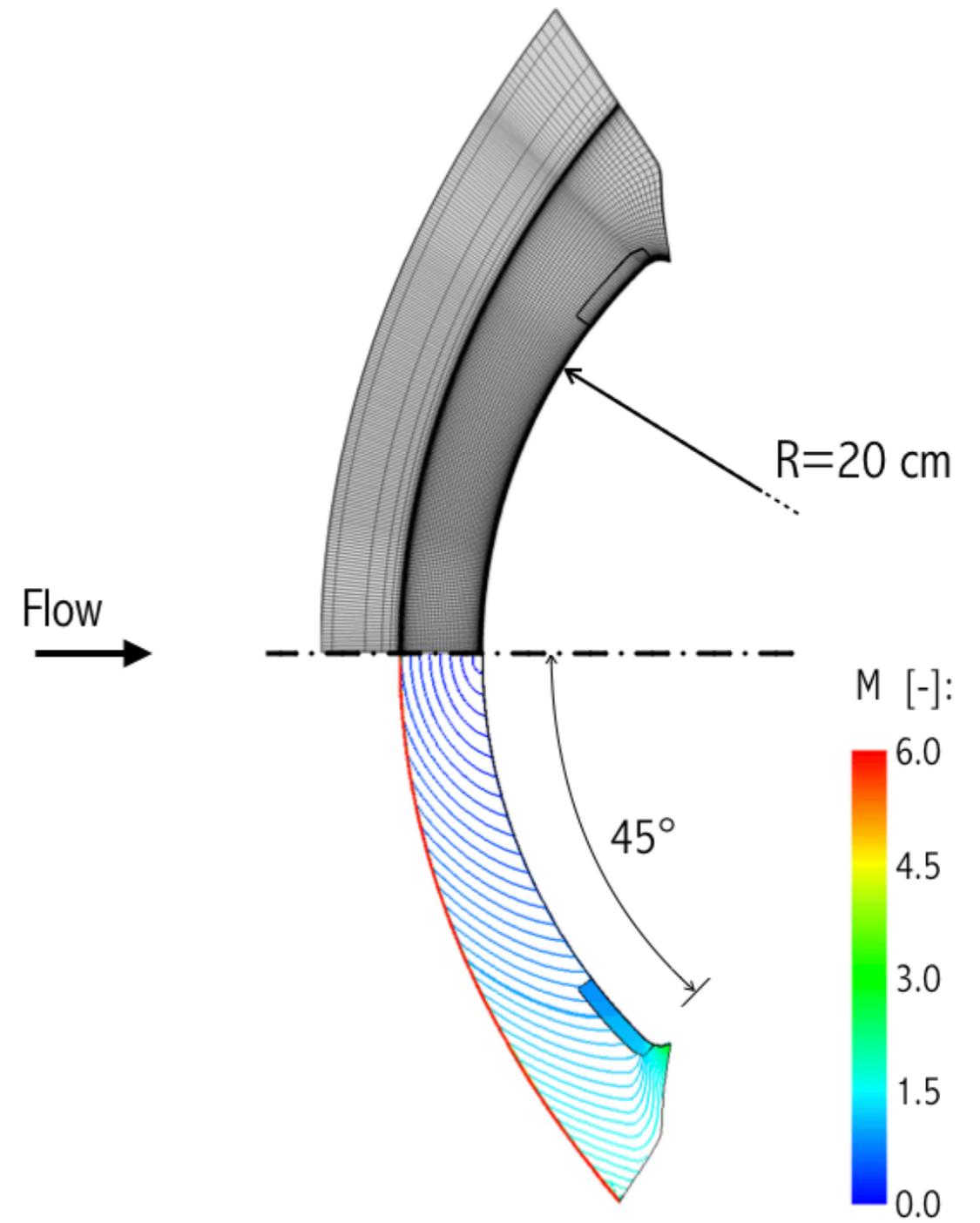


- DNS
- High-Temperature Gas Effects



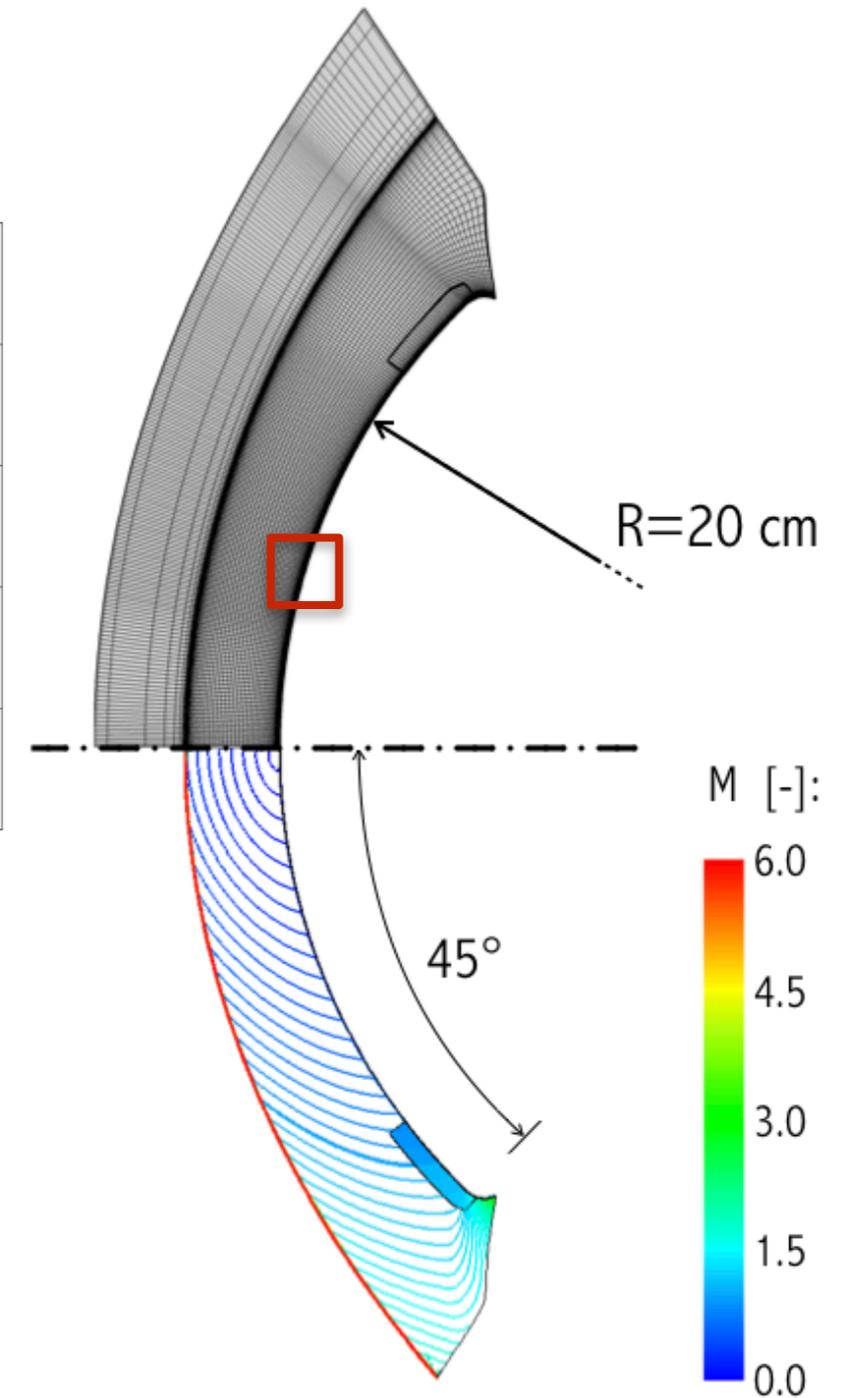
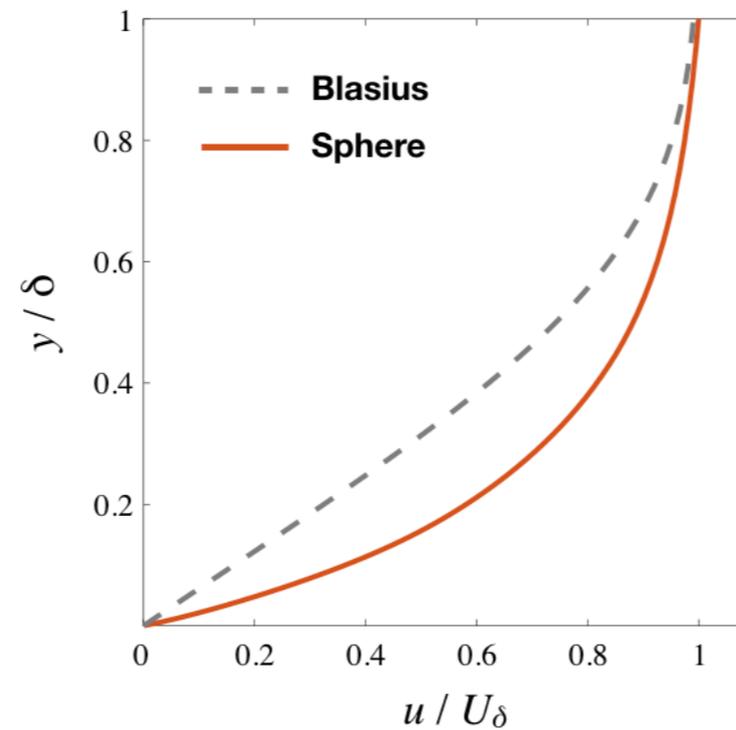
RWTHAACHEN  
UNIVERSITY

# Analysis of the Smooth Configuration



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1<sup>st</sup> Mode: extremely accelerated boundary layer  
—> STABLE



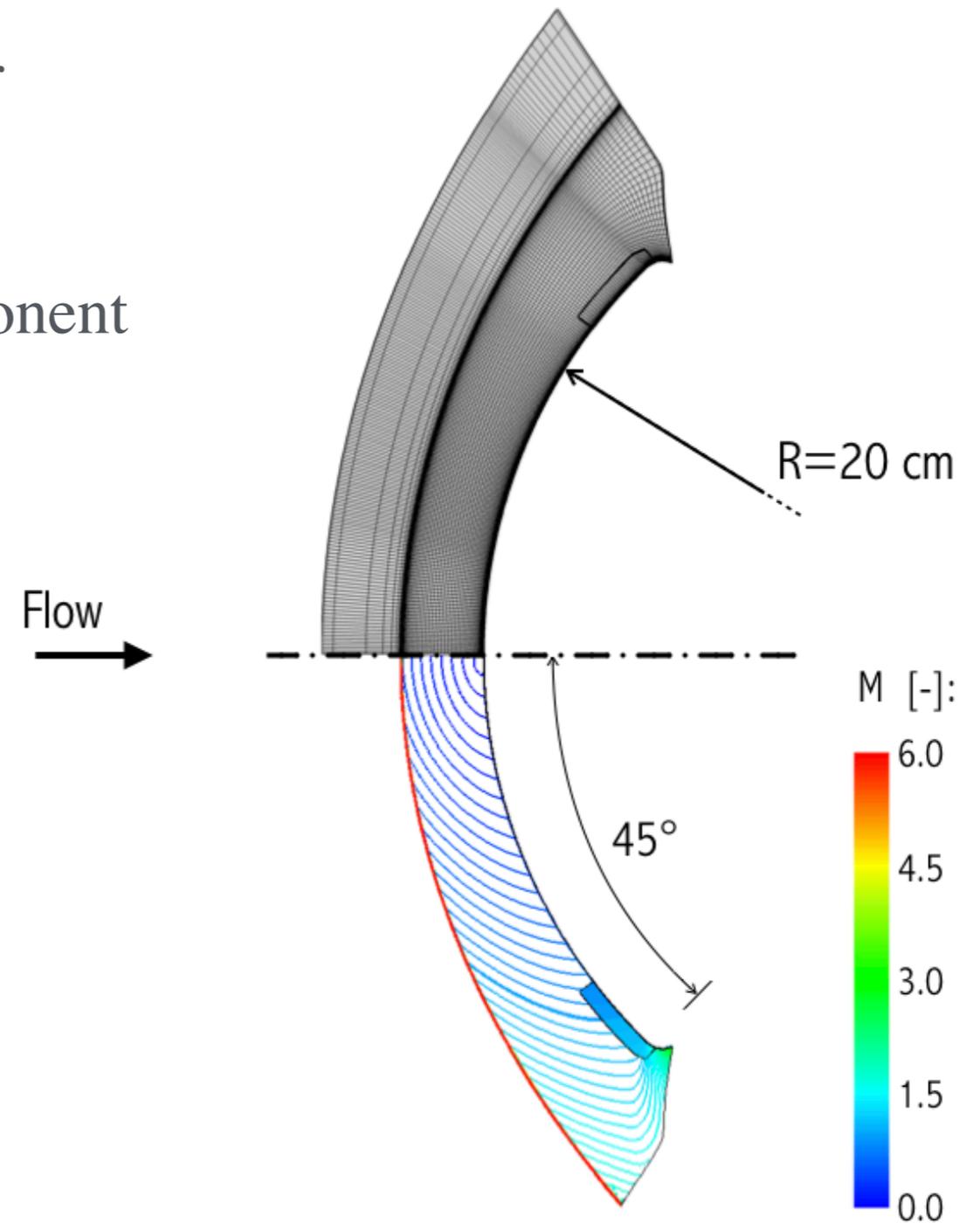
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Crossflow: absence of spanwise velocity component

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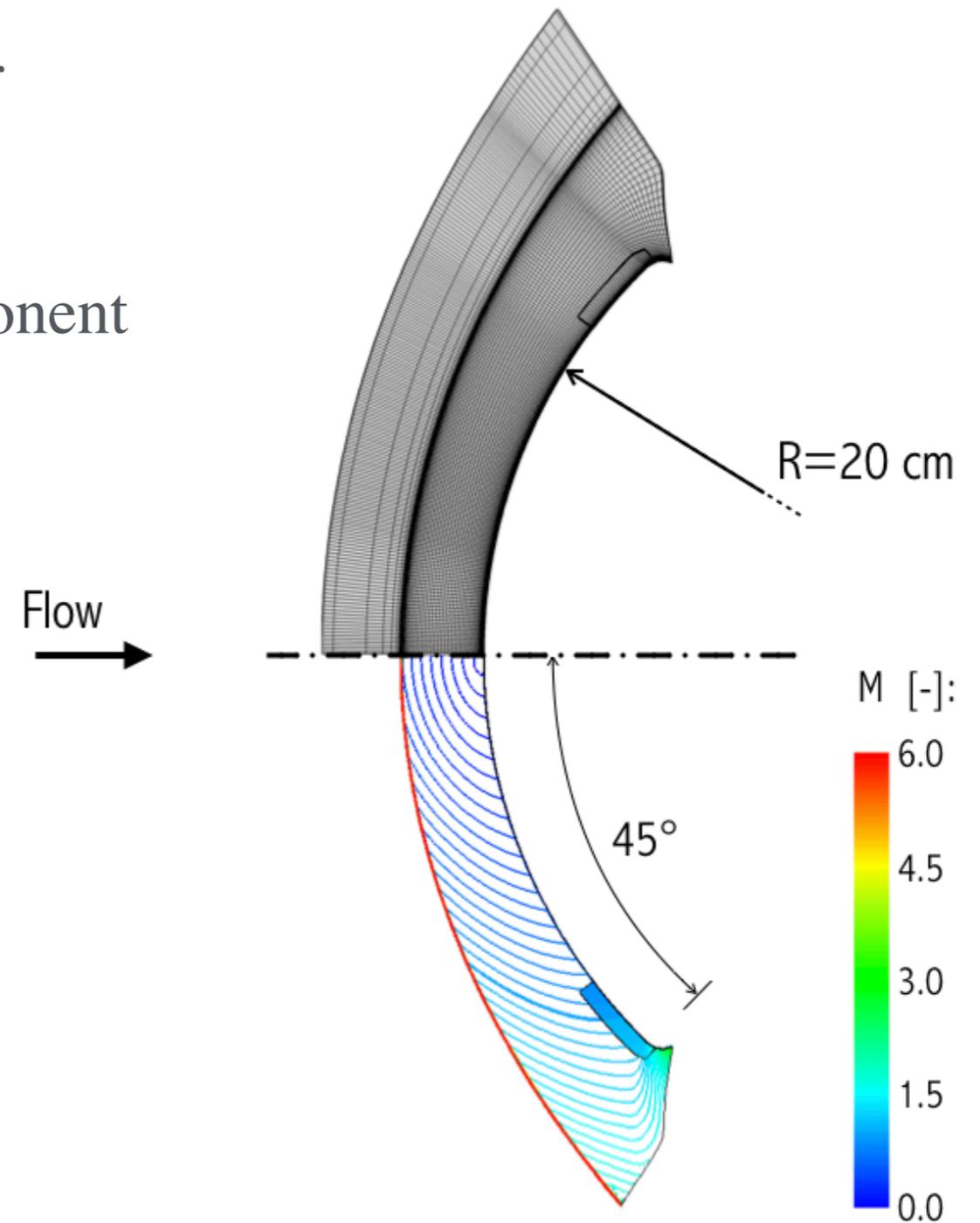
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Görtler: convex geometry

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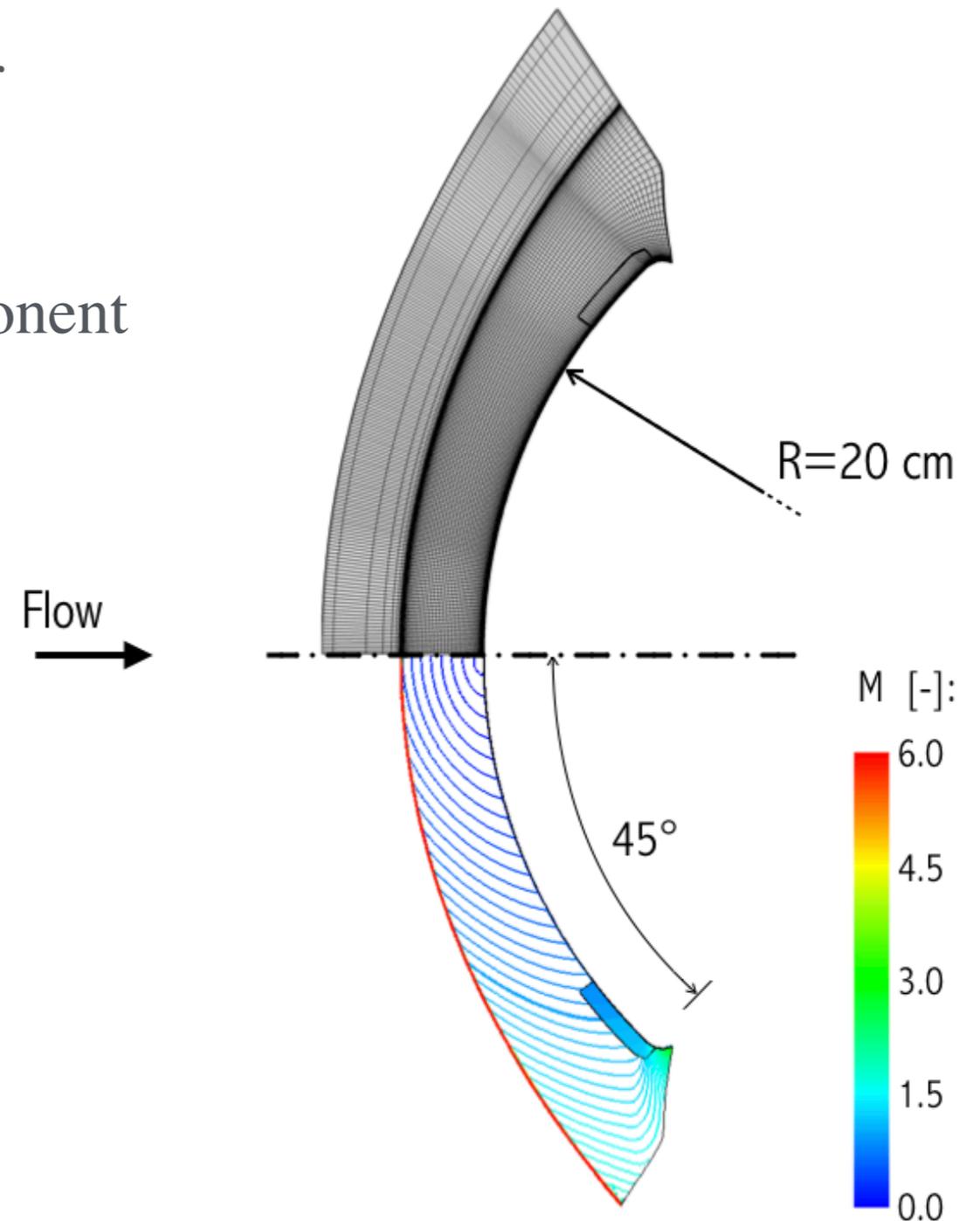
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Görtler: convex geometry

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Transient Growth:  $N$ -factors  $< 3^1$

—> NEGLIGIBLE



<sup>1</sup> Hein, Theiss, Di Giovanni, Stemmer, Schilden, Schröder, Paredes, Choudhari, Li, Reshotko, "Numerical Investigation of Roughness Effects on Transition on Spherical Capsules", *J. Spacecraft and Rockets*, 2018 (accepted)

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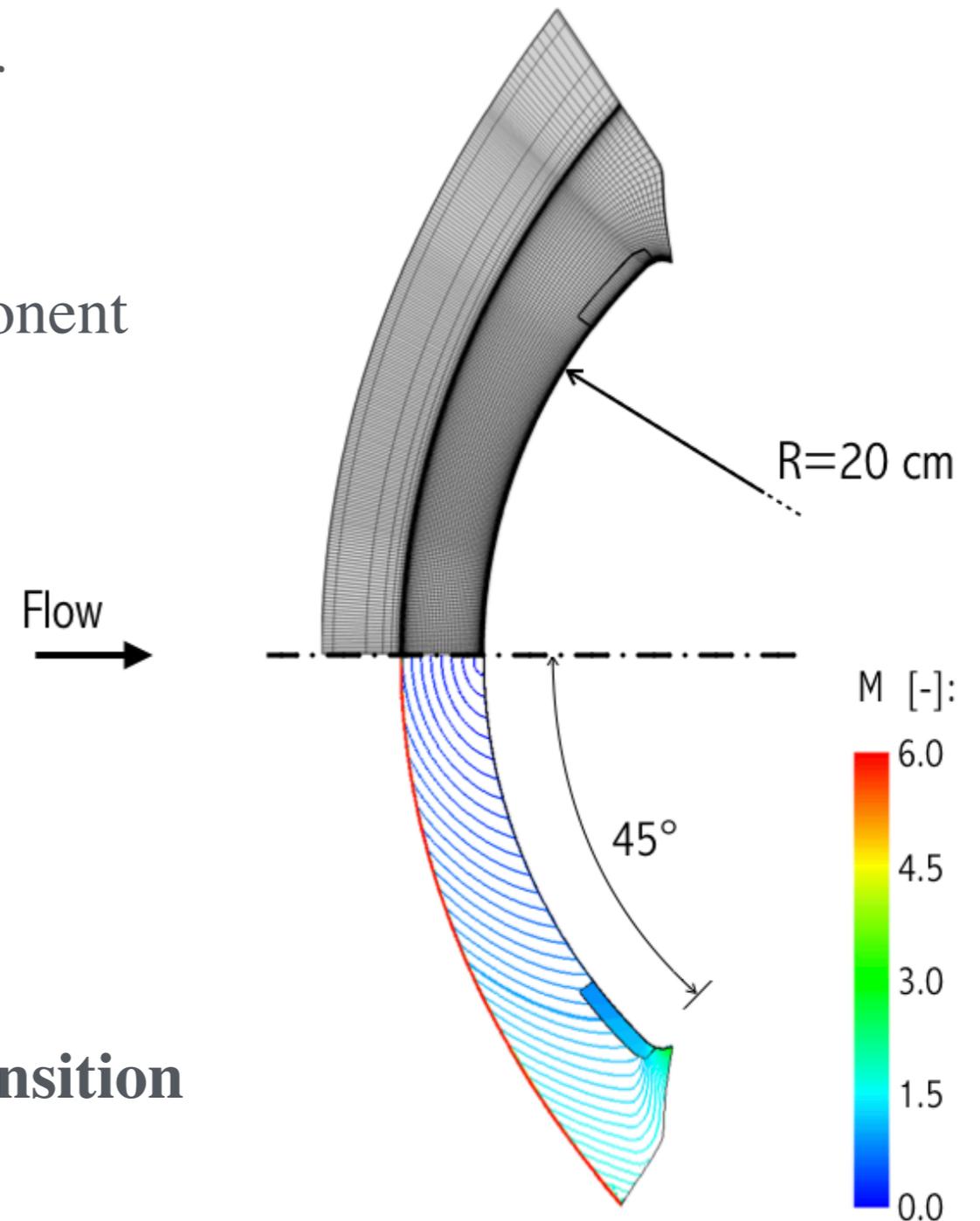
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—> STABLE

Transient Growth:  $N$ -factors  $< 3^1$

—> NEGLIGIBLE

—> **Roughness-induced transition**



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## I. Wind-tunnel conditions ( $M = 5.9$ )

Spanwise periodic roughness elements

Random distributed roughness

Base Flow

Stability Analysis

## II. Re-entry conditions ( $M = 20$ )

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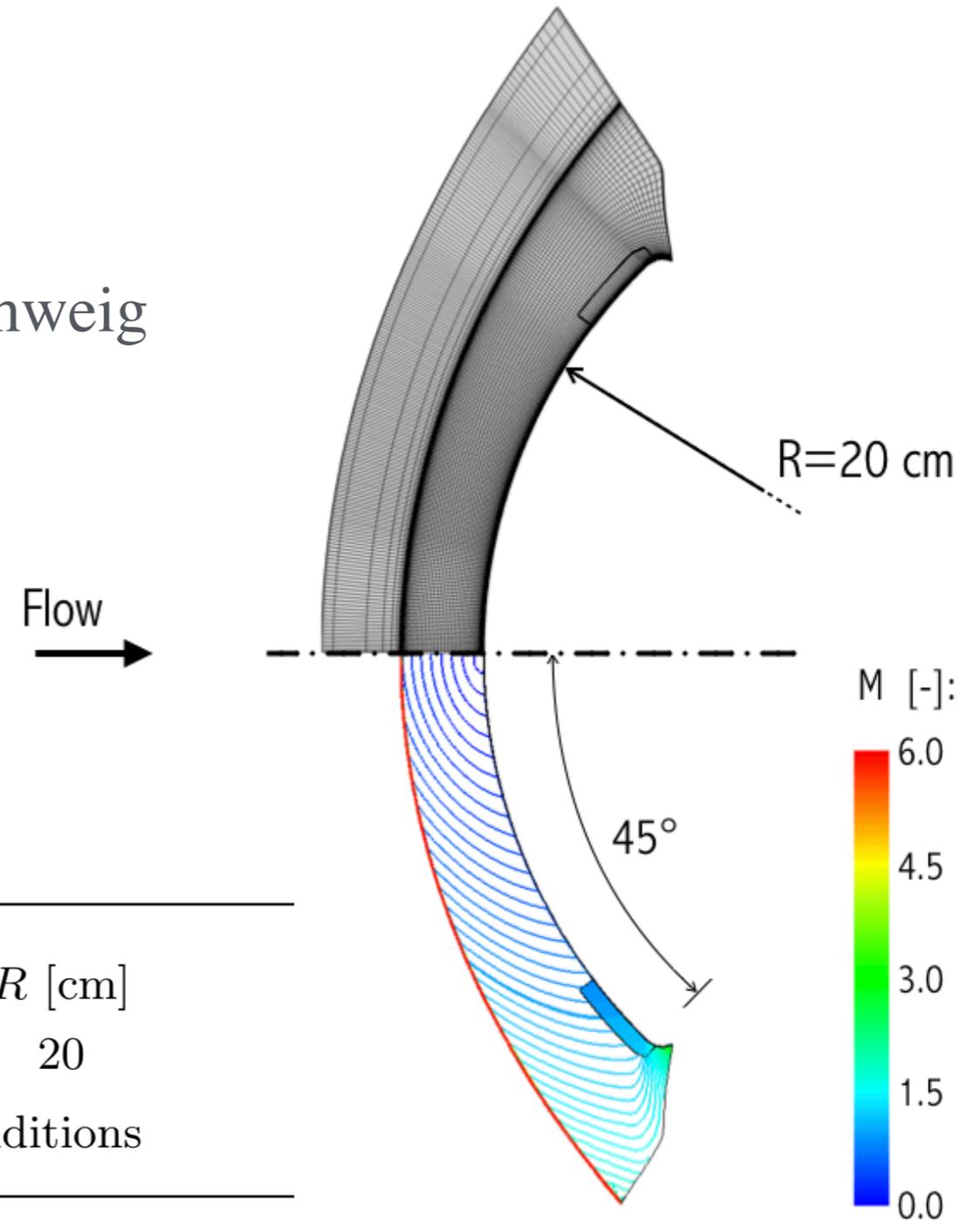
Stability Analysis

# Geometry and Freestream Conditions

Geometry: capsule-like hemisphere

Conditions: Hypersonic Ludwig tube Braunschweig (HLB)

Gas model: ideal gas



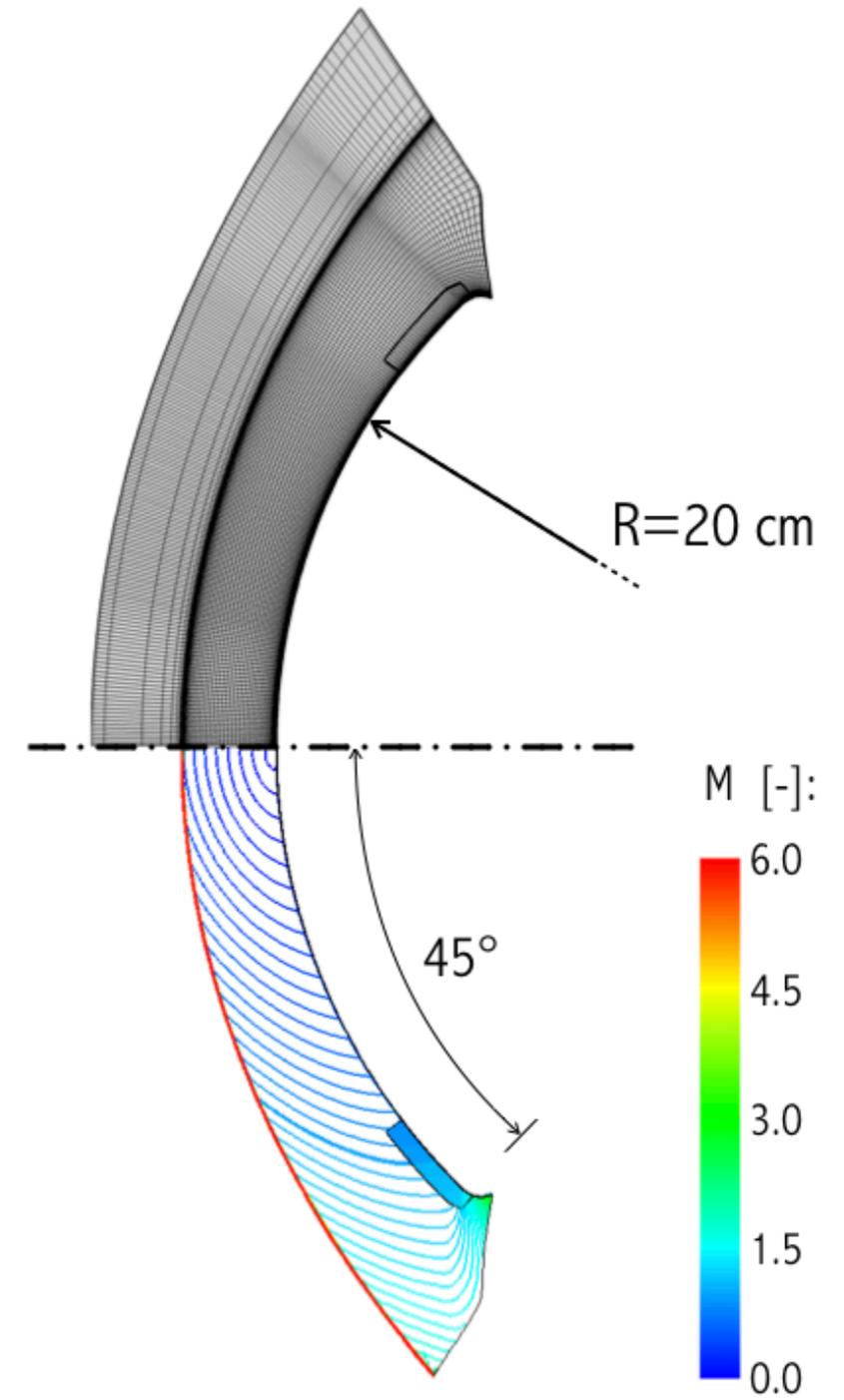
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Medium	$M$	$T_0$ [K]	$T_w$ [K]	$Re_\infty$ [1/m]	$R$ [cm]
Air	5.9	470	295	$18 \cdot 10^6$	20

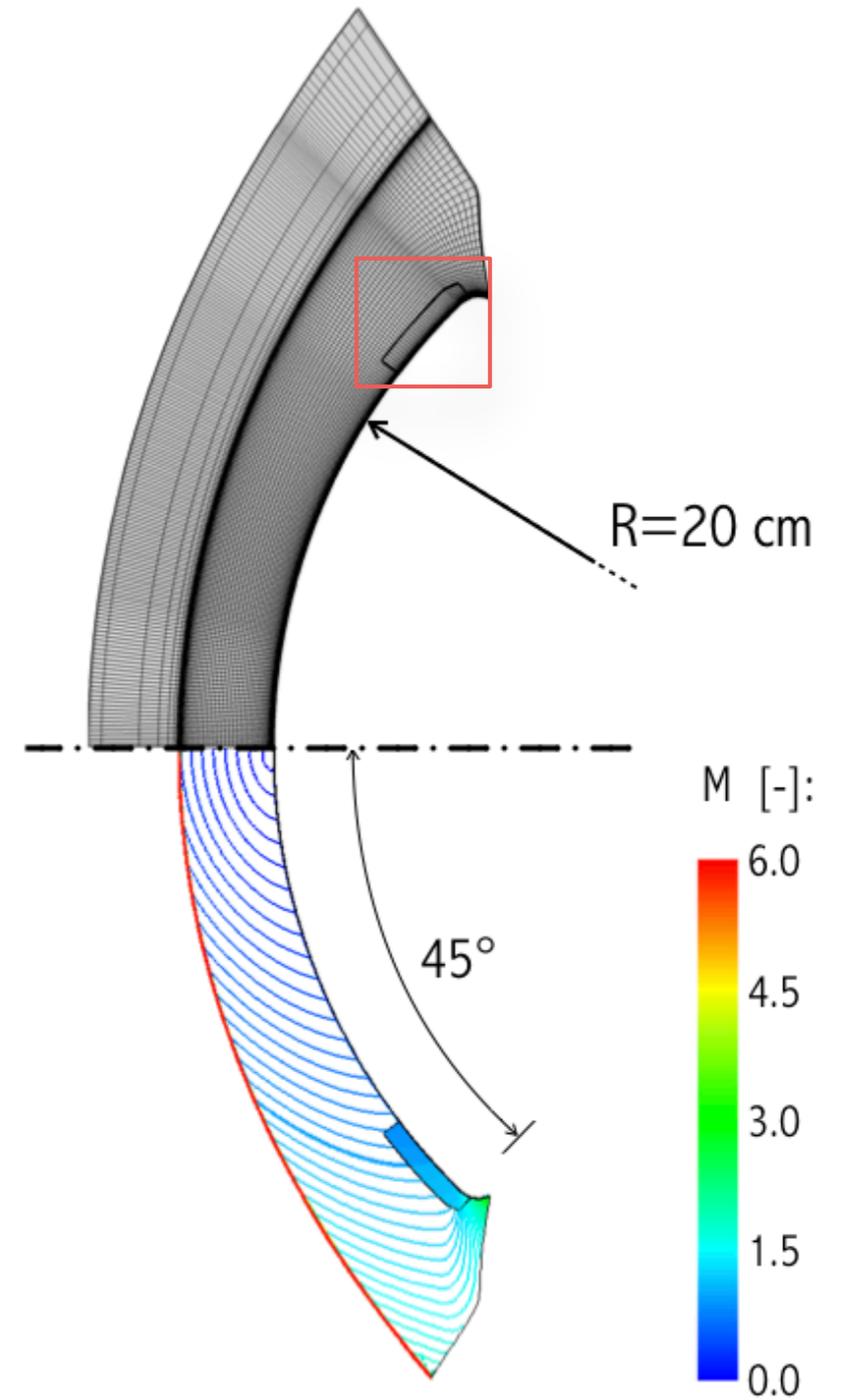
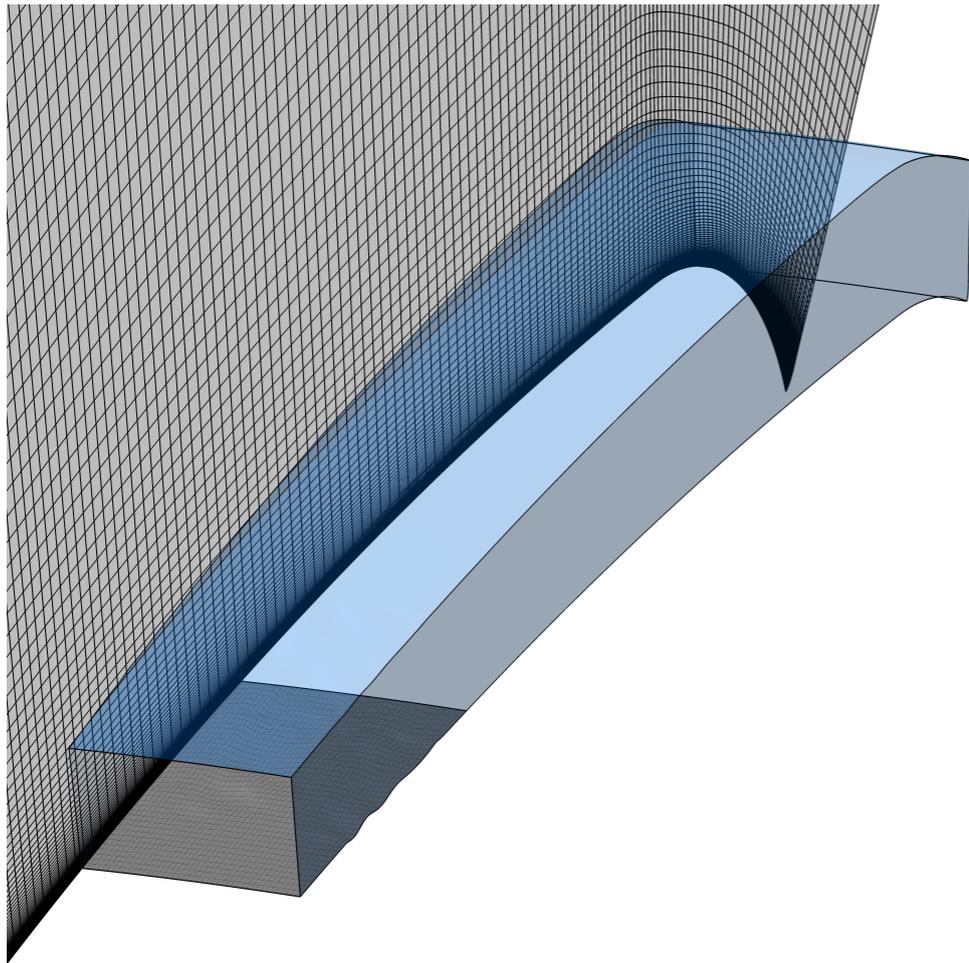
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TABLE 1. Simulation parameters - windtunnel conditions

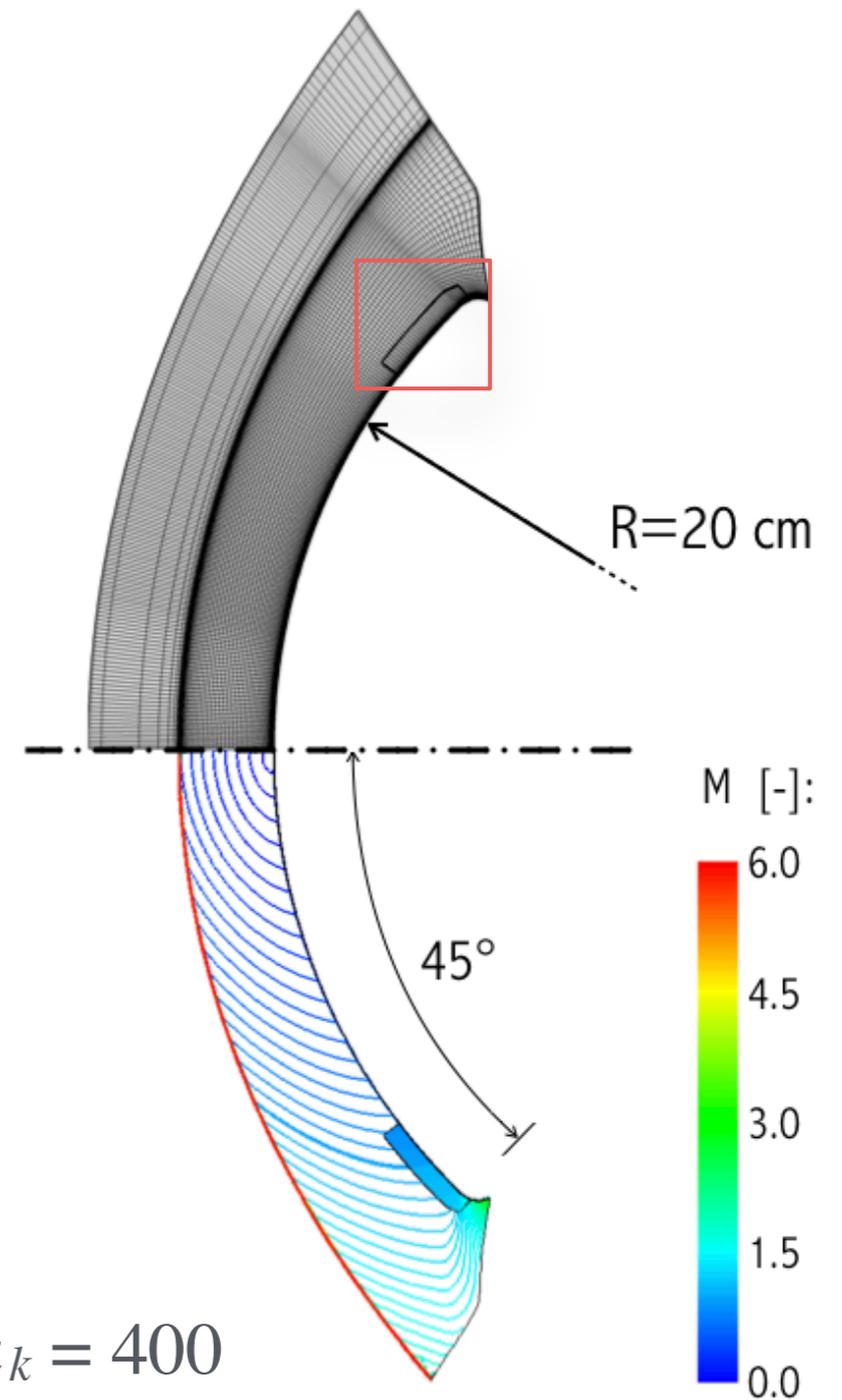
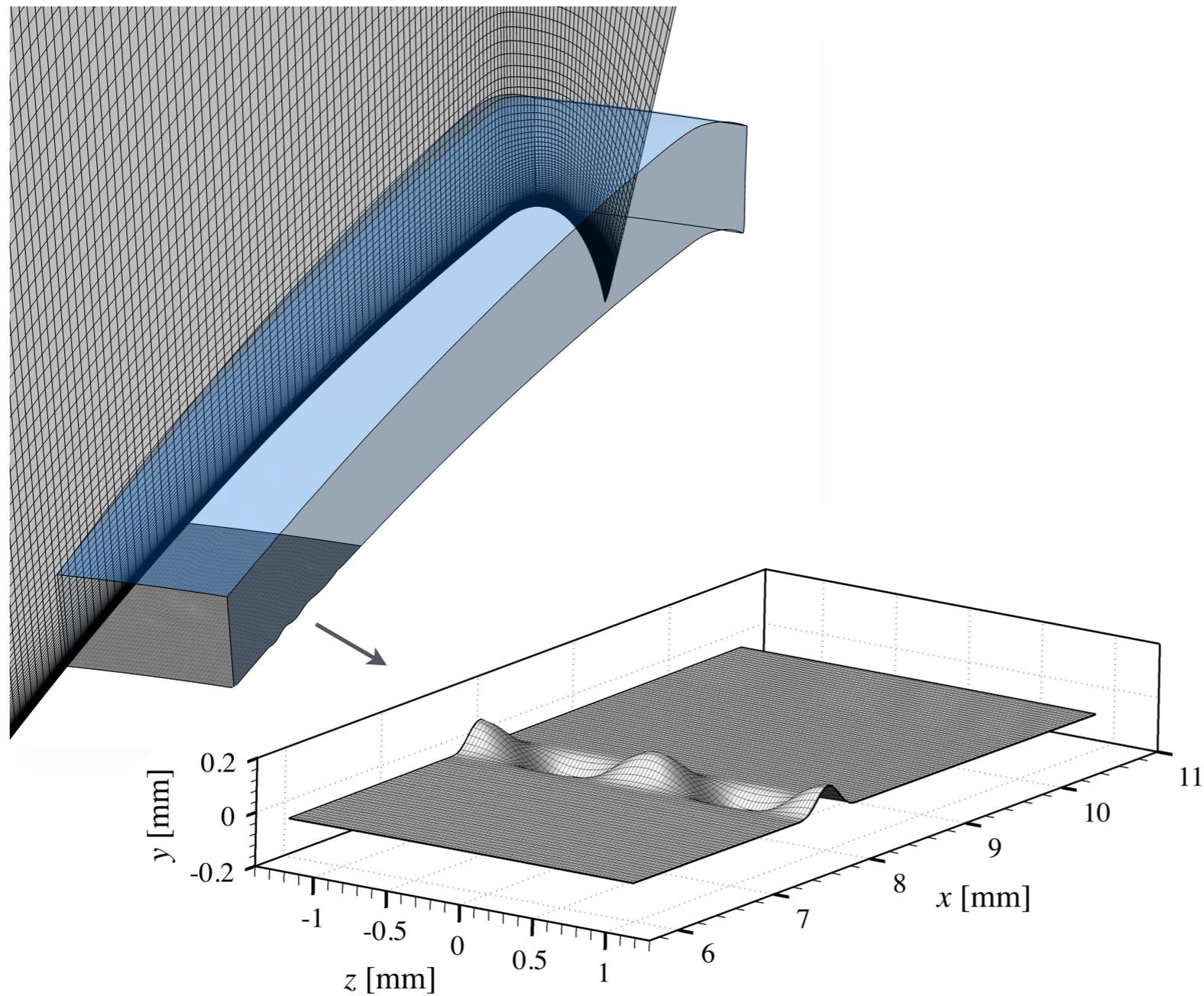
# Analysis of a “simple” Roughness



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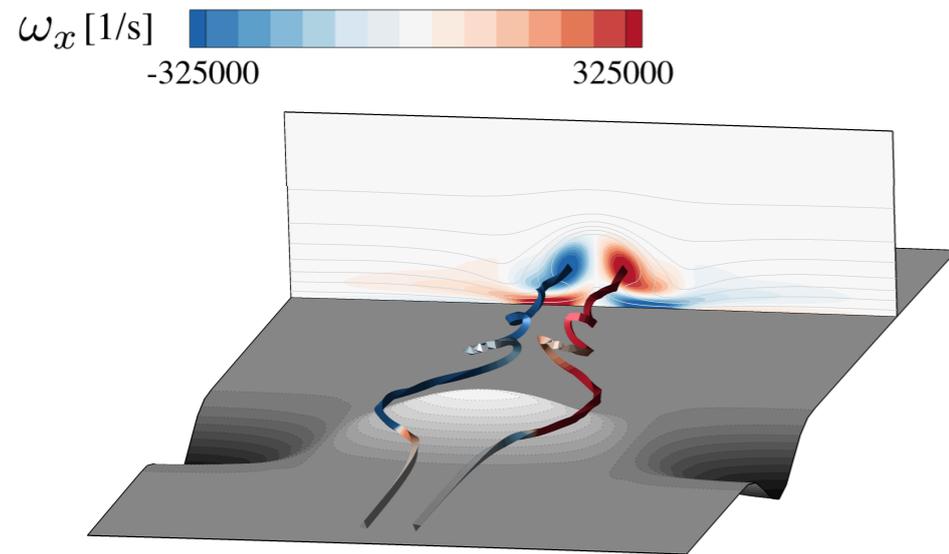


# Analysis of a “simple” Roughness



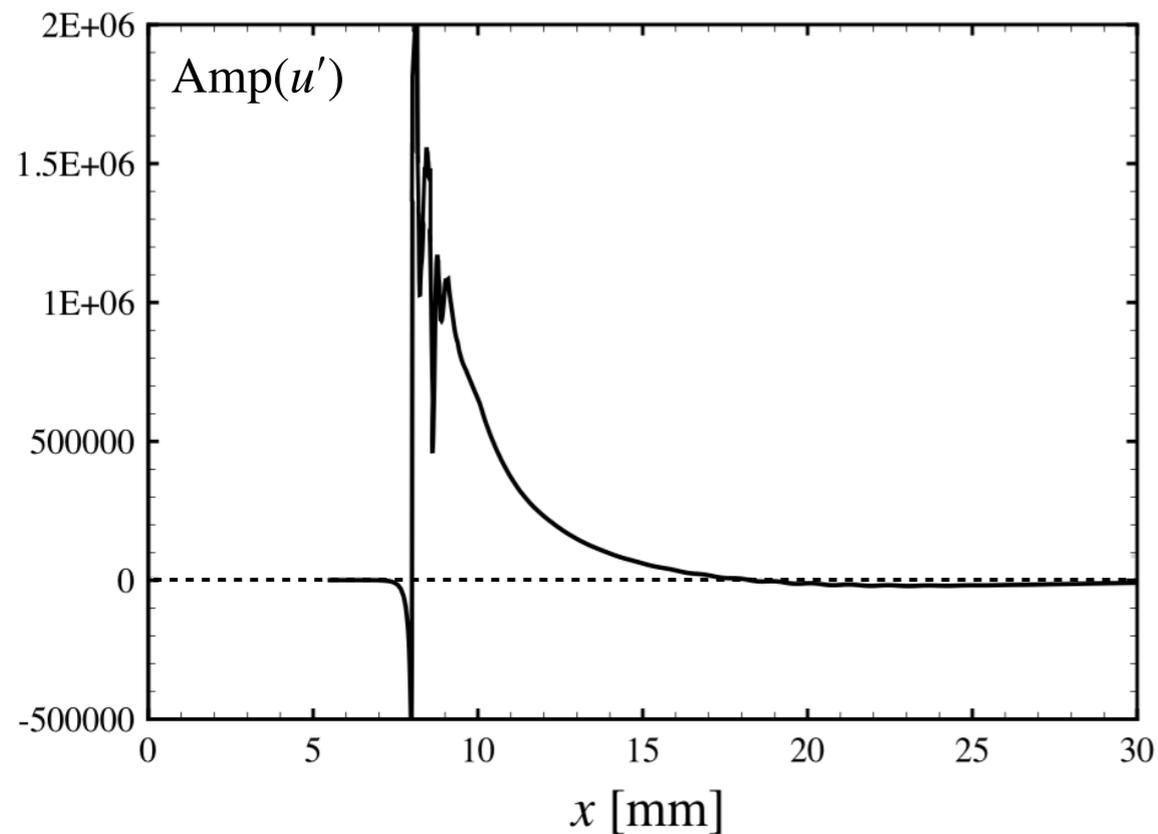
*simple rgh:*  $k = 100 \mu\text{m}$   $k/\delta = 0.35$   $Re_{kk} = u_k \rho_k k / \mu_k = 400$

# Analysis of a “simple” Roughness

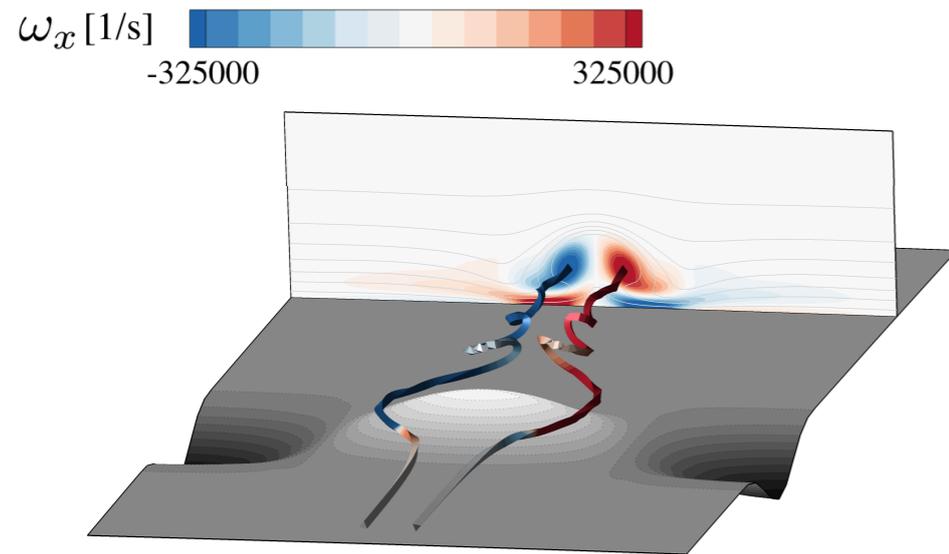


- Counter-rotating vortices originate in the roughness wake
- Roughness wake decays rapidly

Amplitude of the roughness wake

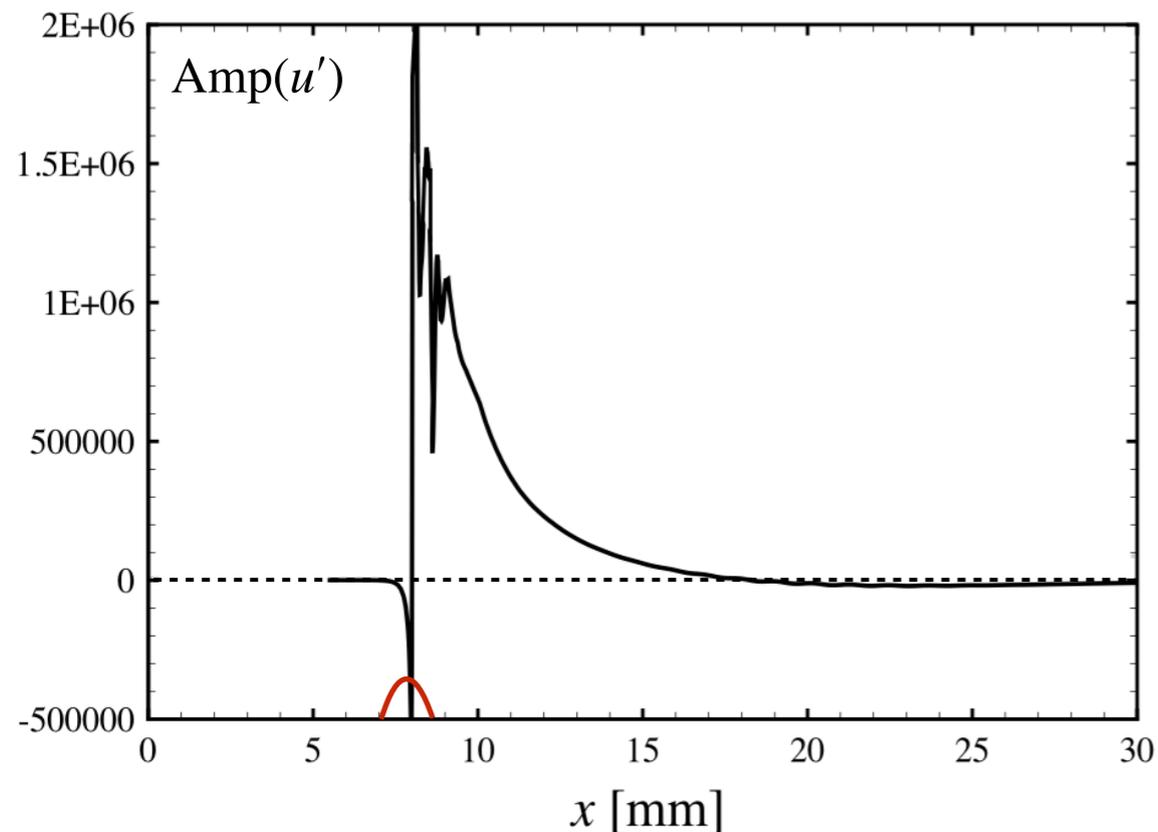


# Analysis of a “simple” Roughness

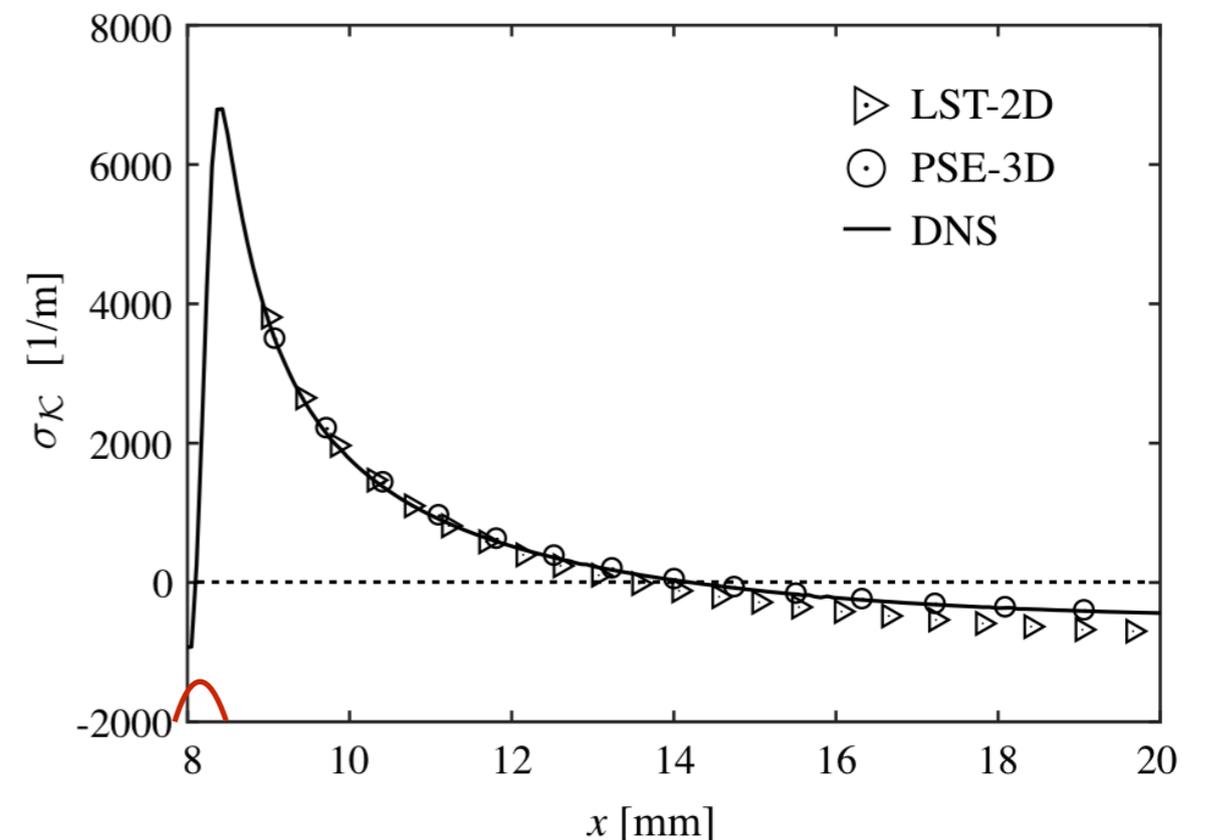


- Counter-rotating vortices originate in the roughness wake
- Roughness wake decays rapidly
- $N$ -factor =  $\log(A_{\max}/A_{\text{in}}) \sim 8$  (included roughness)

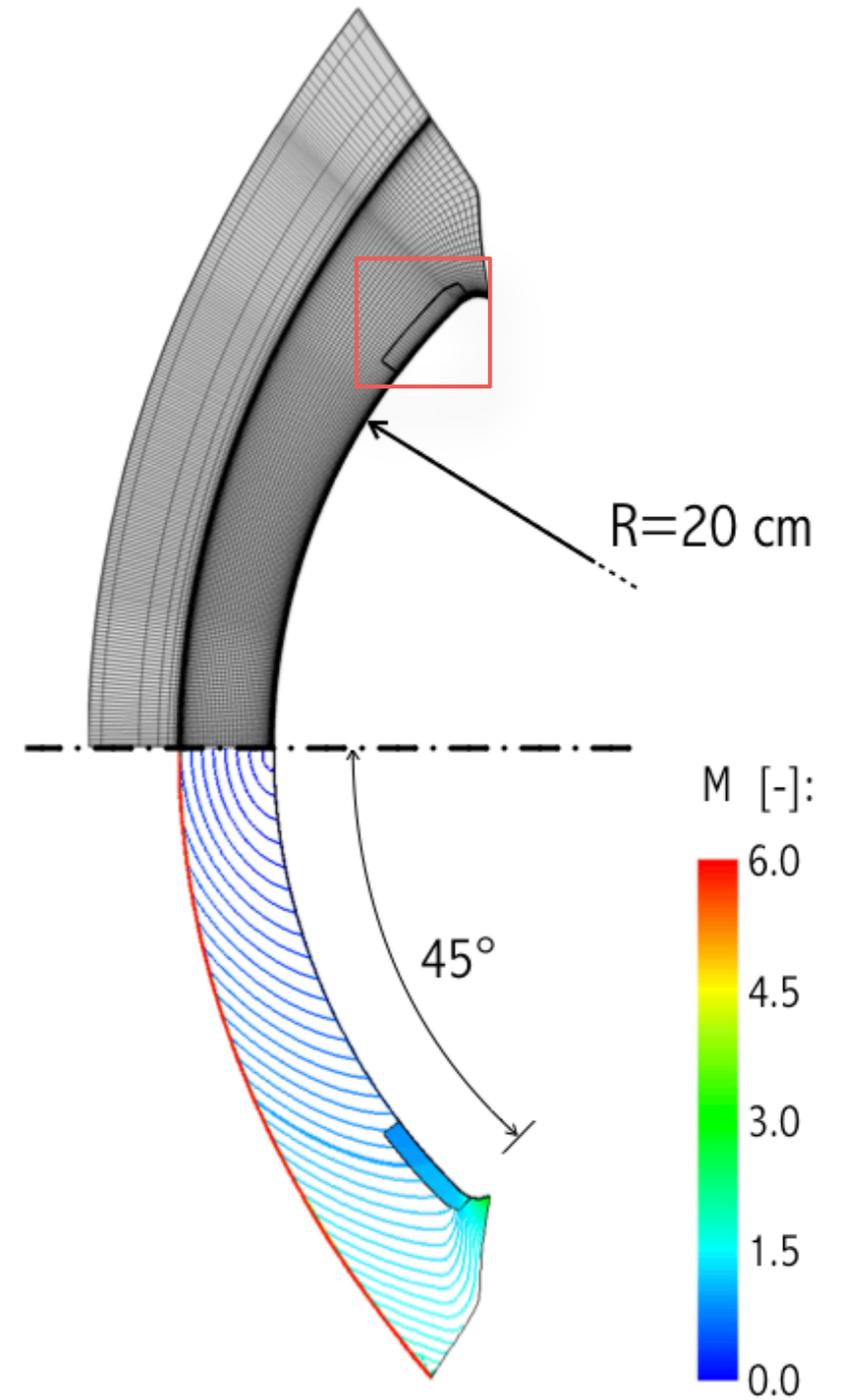
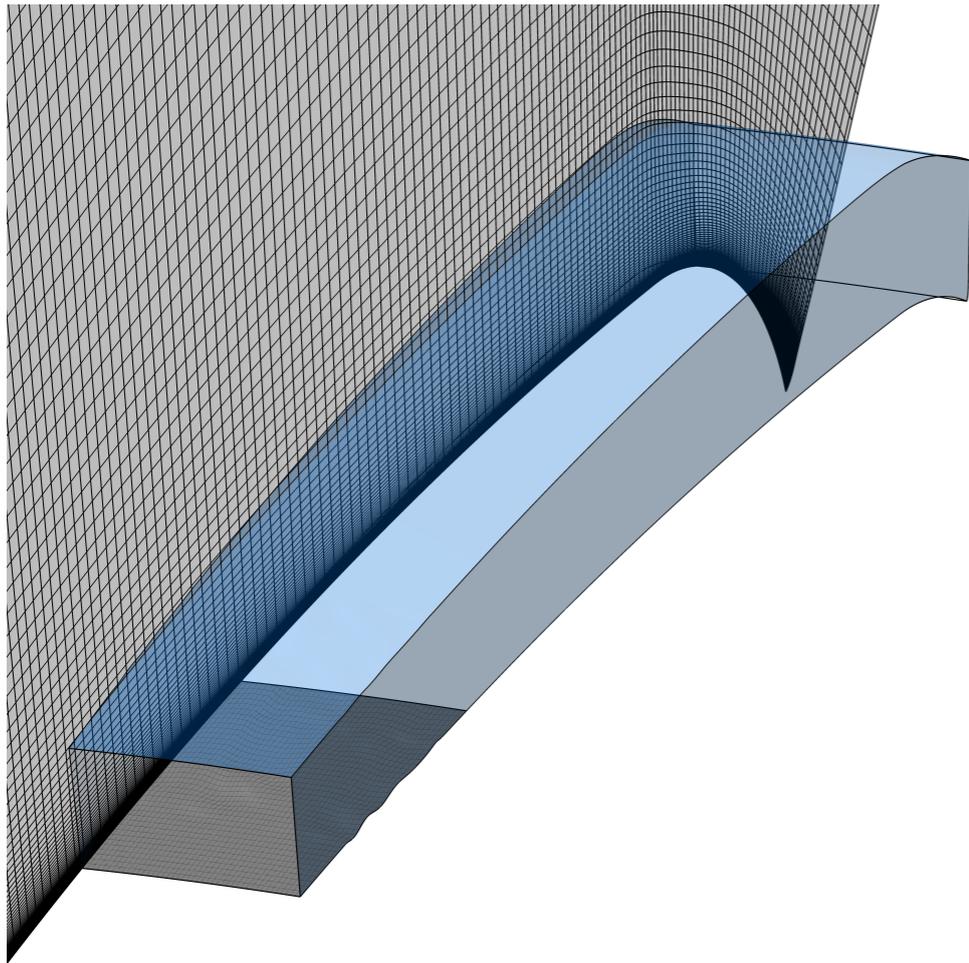
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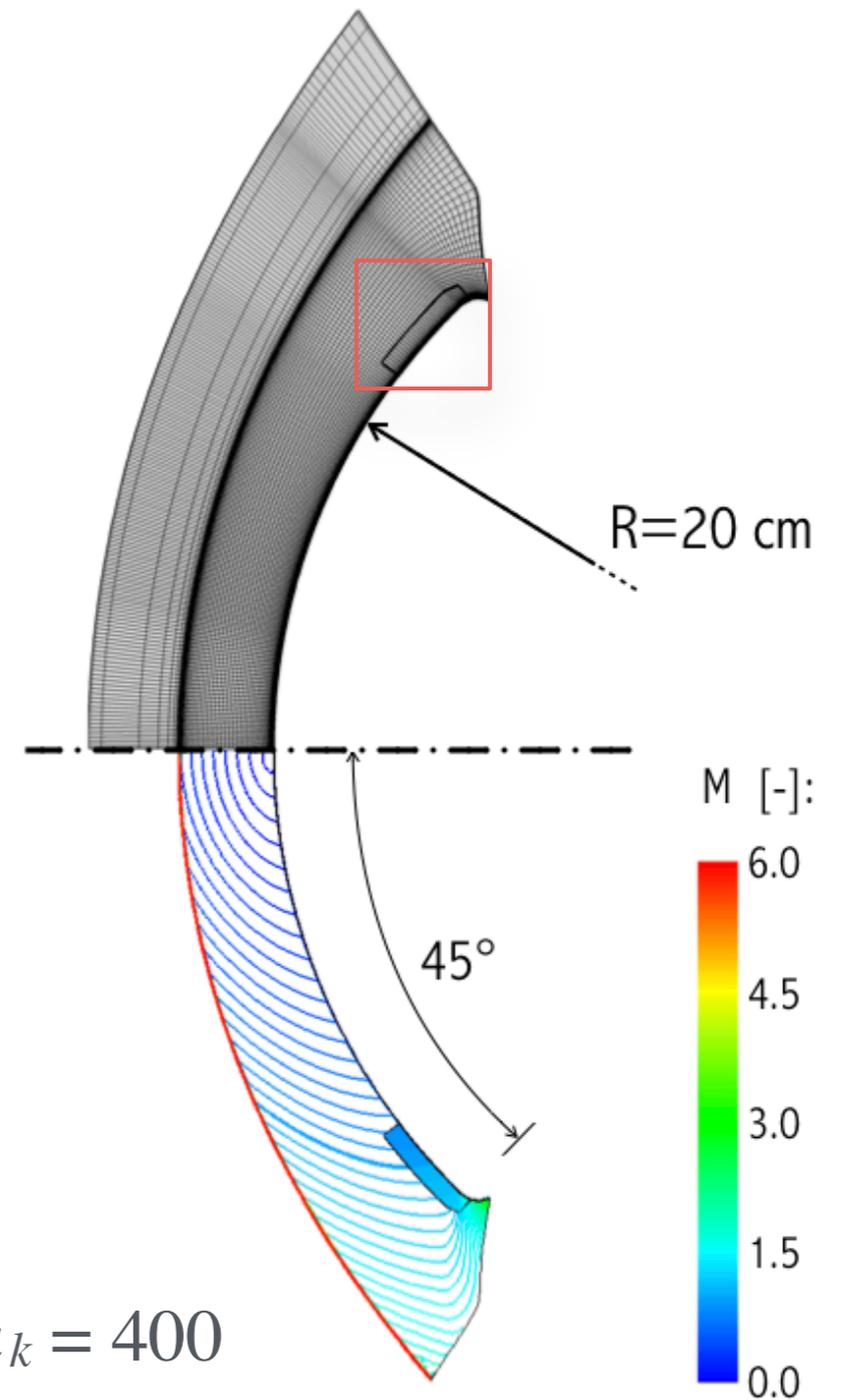
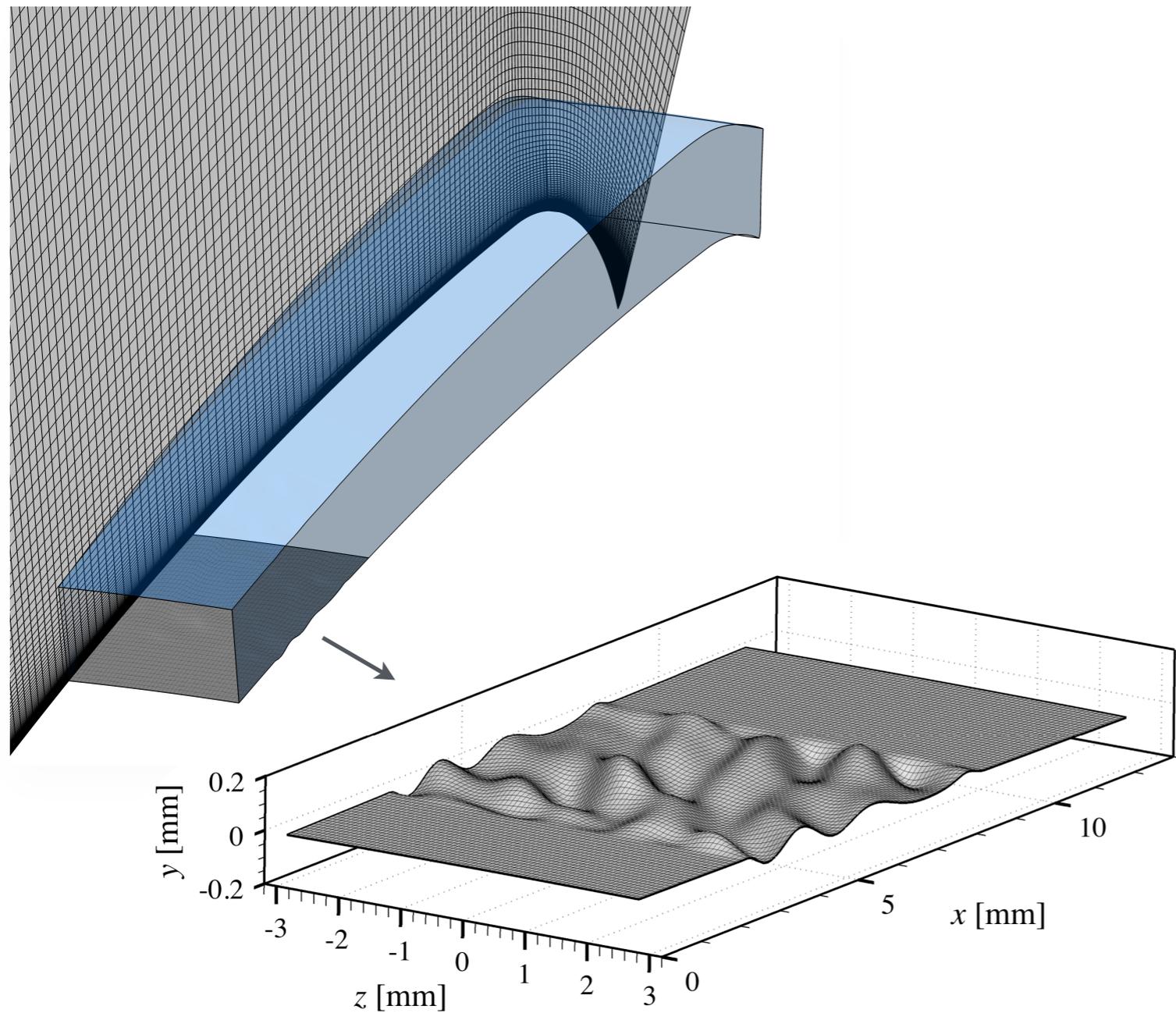
Growth rate (disturbance at 250 kHz)



# Definition of a *distributed* Roughness



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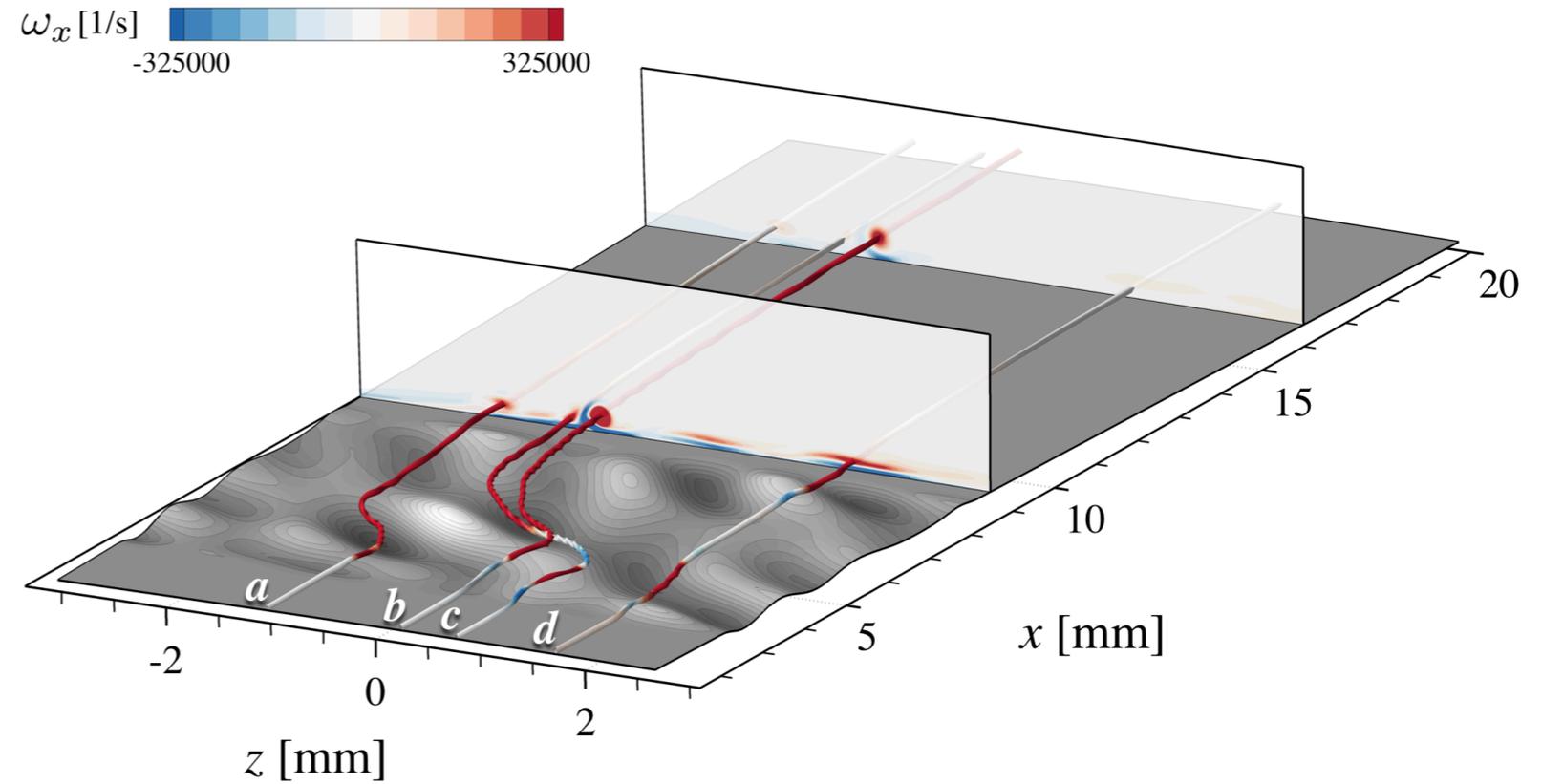


*distributed* rgh:  $k = 100 \mu\text{m}$   $k/\delta = 0.35$   $Re_{kk} = u_k \rho_k k / \mu_k = 400$

*simple* rgh:  $k = 100 \mu\text{m}$   $k/\delta = 0.35$   $Re_{kk} = u_k \rho_k k / \mu_k = 400$

# Steady Base Flow

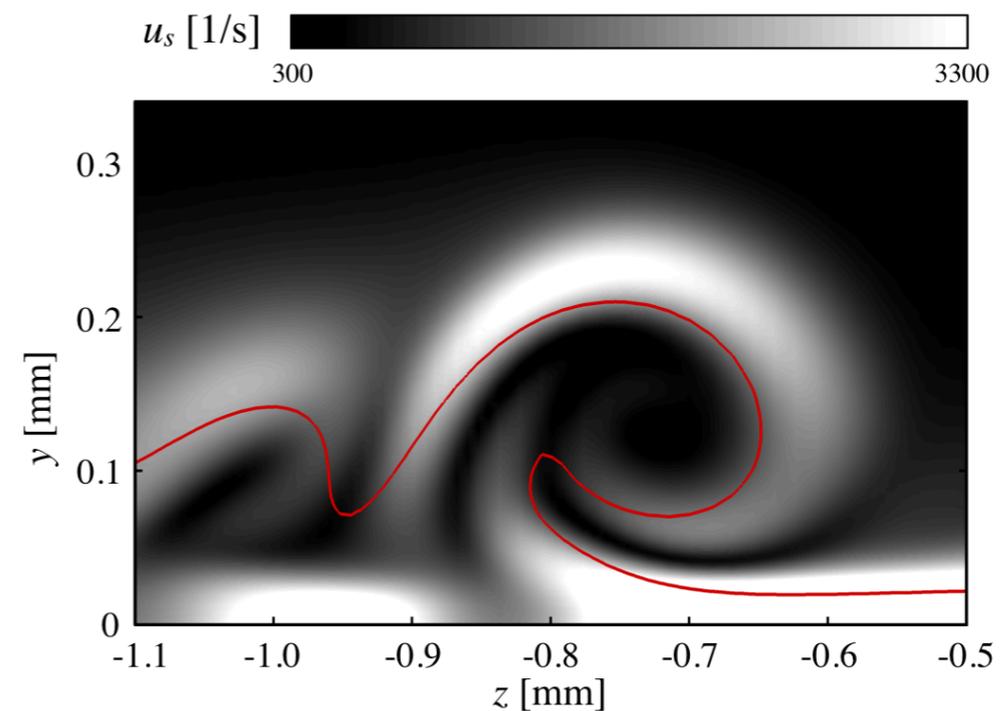
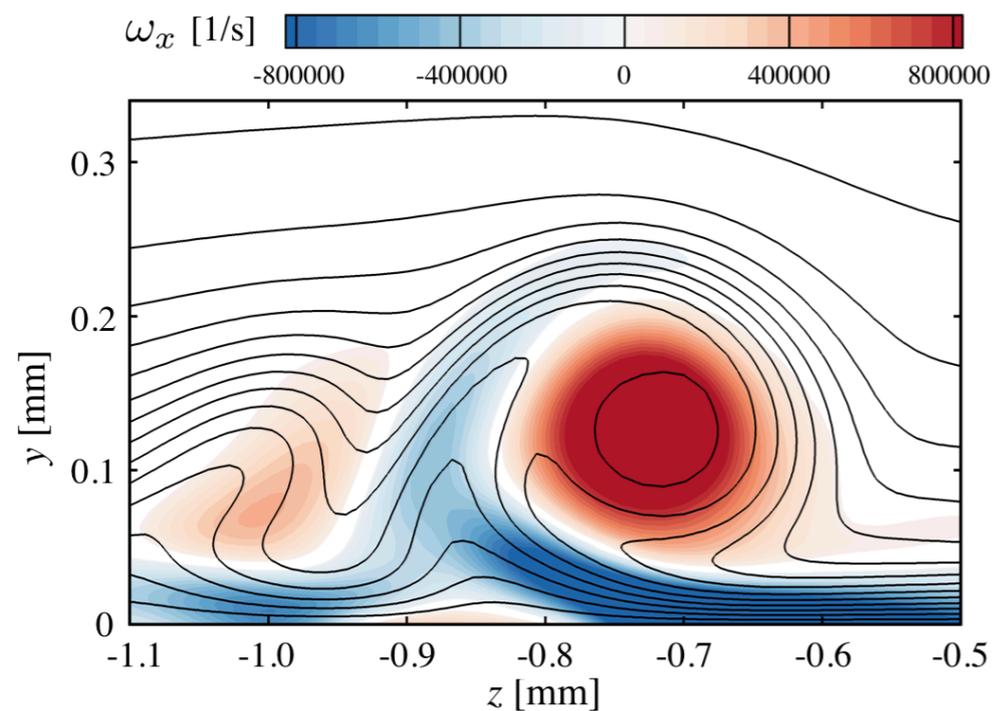
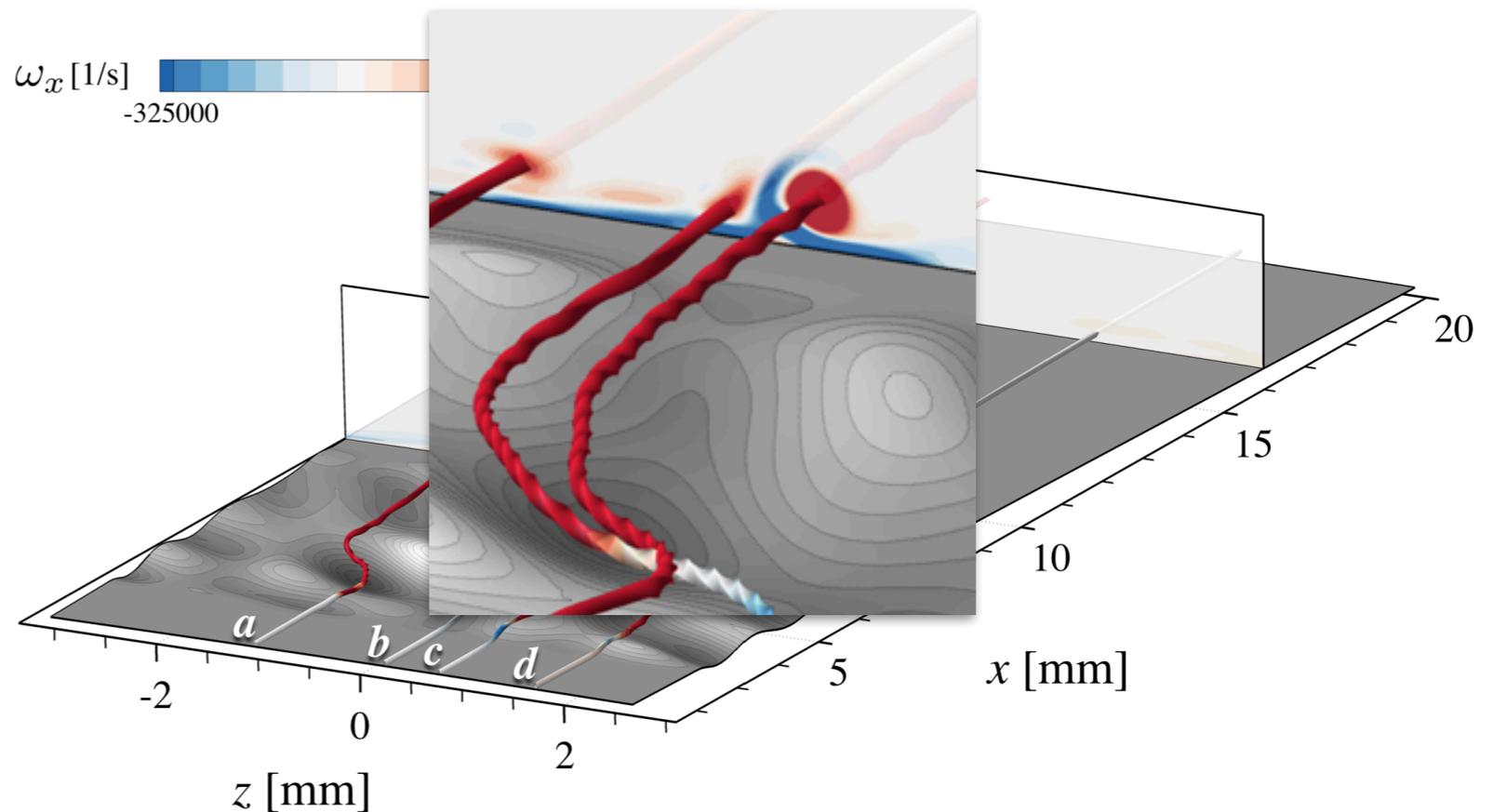
- Multiple vorticity regions in the roughness wake



# Steady Base Flow: Crossflow-type Vortex

Multiple vorticity regions in the roughness wake

- Formation of a crossflow-type vortex due to the spanwise velocity induced by the skewness of the roughness

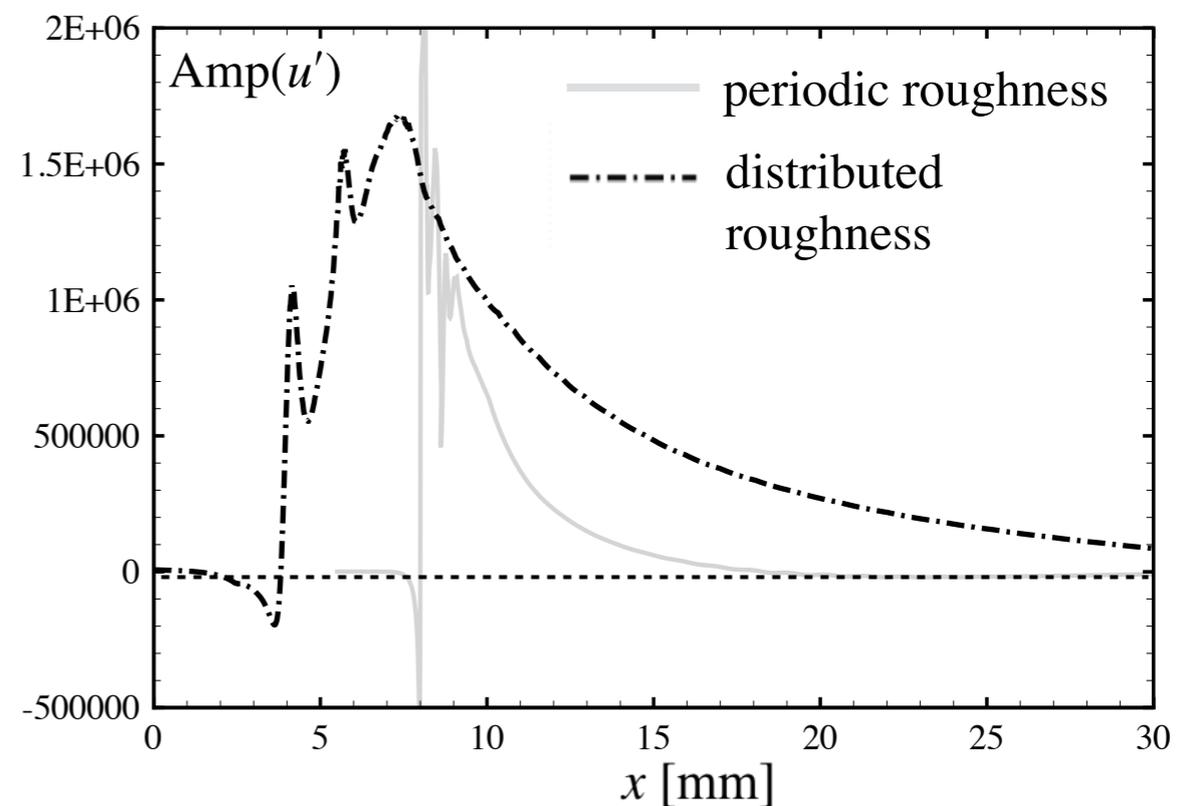
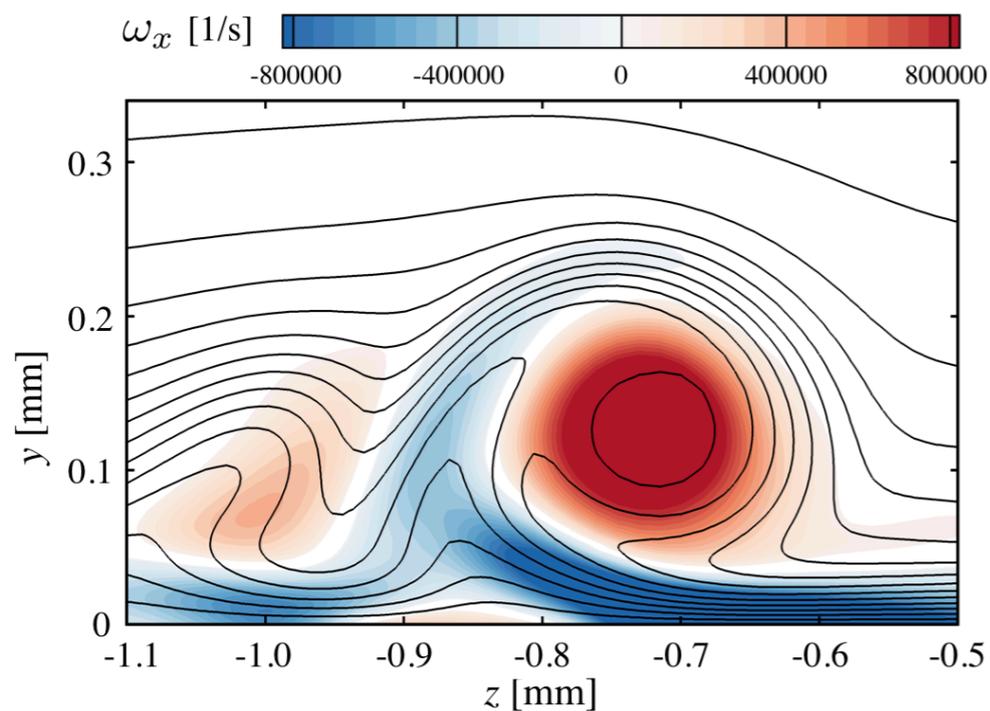
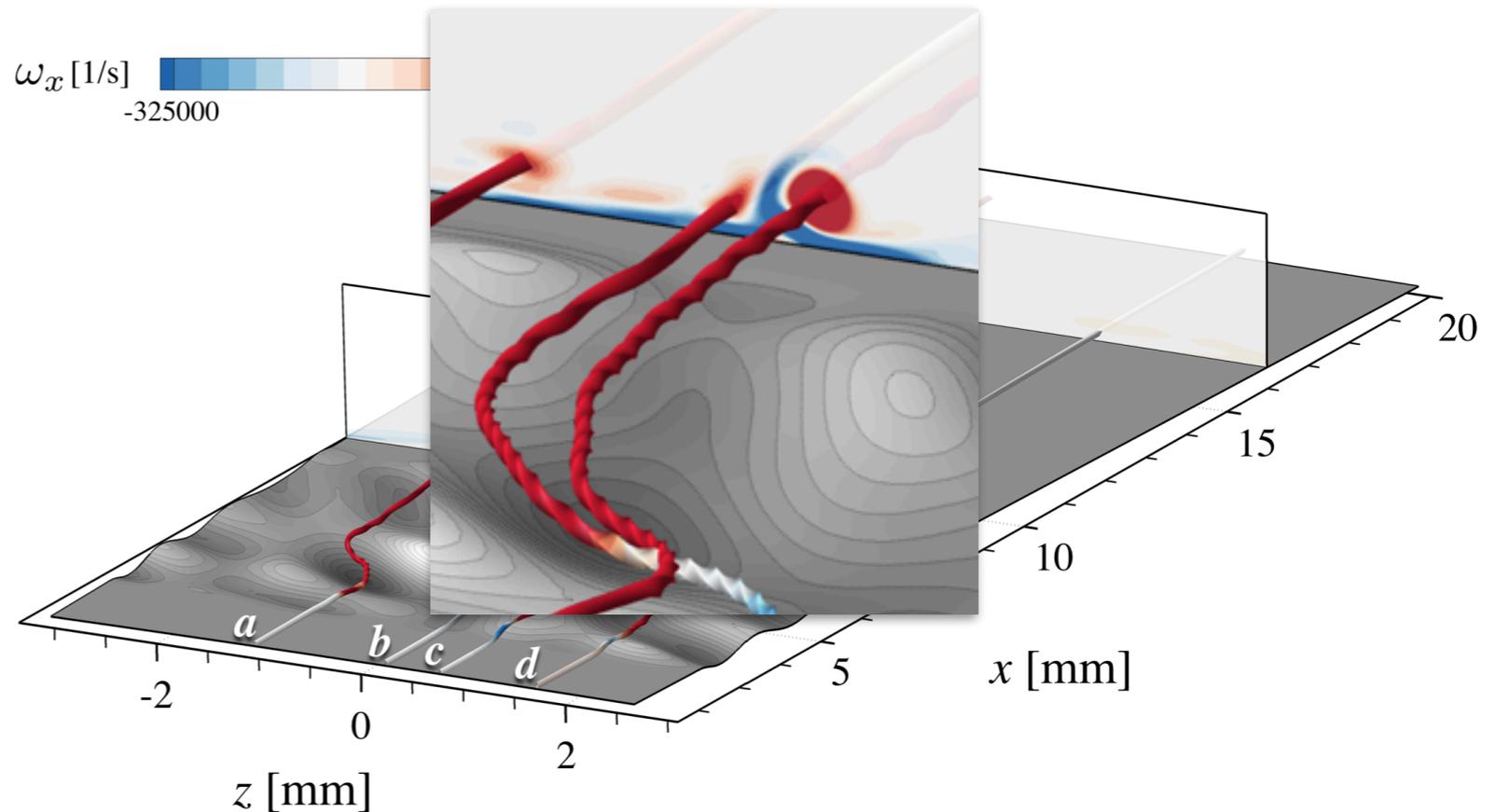


# Steady Base Flow: Crossflow-type Vortex

Multiple vorticity regions in the roughness wake

Formation of a crossflow-type vortex due to the spanwise velocity induced by the skewness of the roughness

- The crossflow-type vortex is very persistent in the accelerated boundary layer



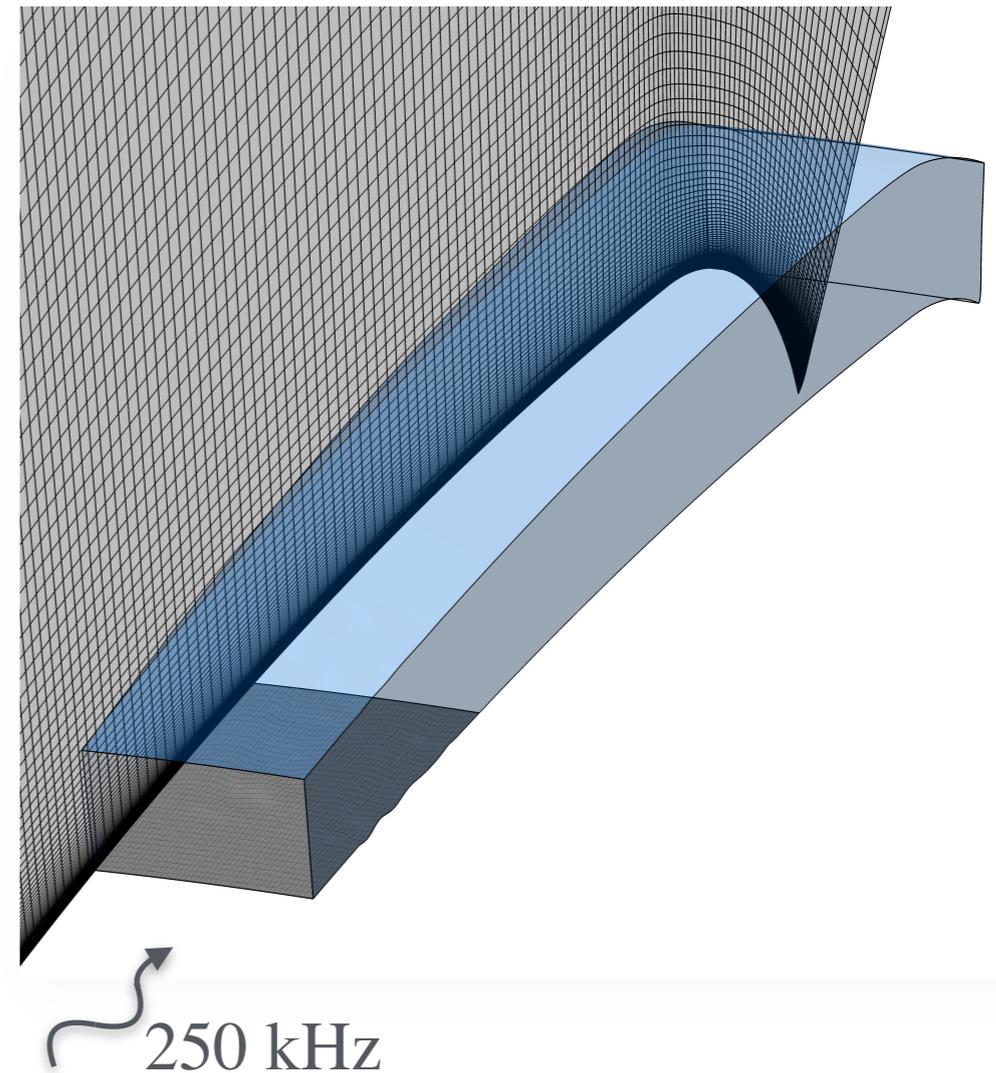
# DNS-based Stability Analysis

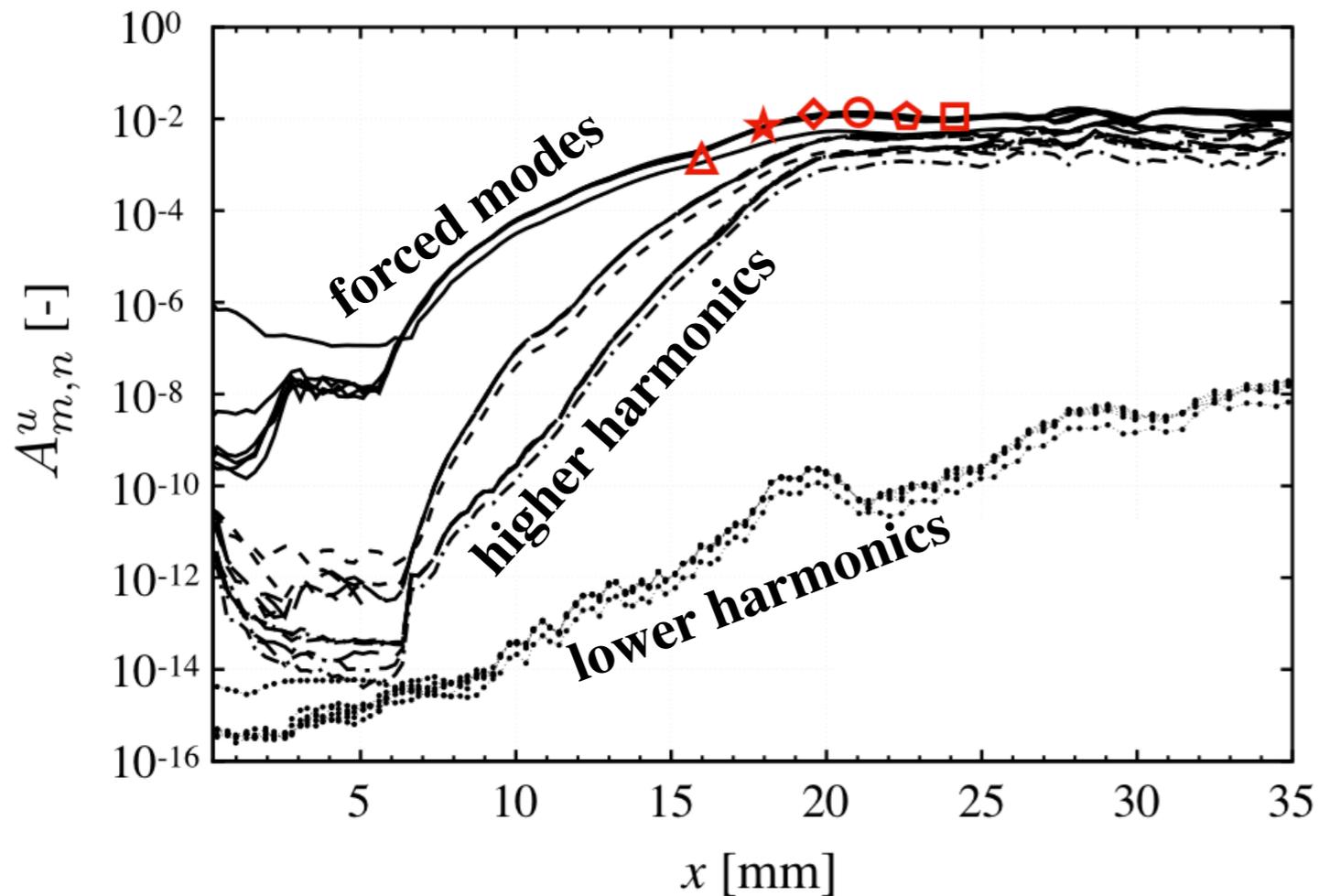
We force at the inflow

- small acoustic disturbances
- upstream of the roughness patch
- at 250 kHz (forced mode)

Analysis is carried out through

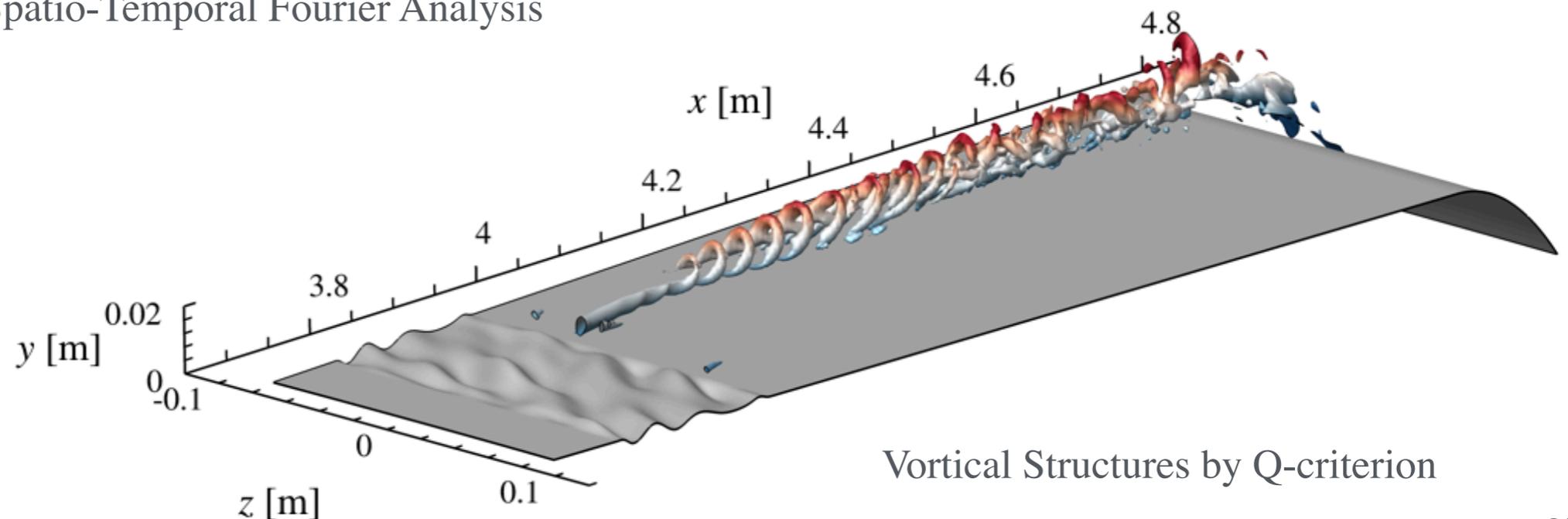
- spatio-temporal Fourier transform  
(spanwise wavenumber - frequency)





Results of the Spatio-Temporal Fourier Analysis

- harmonics of the forced frequency non-linearly driven in the roughness wake
- observed  $N$ -factor  $> 13$  (cf.  $N=8$  for single roughness,  $k$  and  $Re_{kk}$  being equal)
- small interaction with the roughness (forced modes remain dominant up to growth saturation)



Vortical Structures by Q-criterion

# Investigations under Windtunnel Conditions: most relevant results<sup>2</sup> so far...

- a. The skewness of protuberances as obtained in the presence of (pseudo-)random distributed roughness induces a spanwise component of the velocity which is not present in the original two-dimensional base flow. A crossflow-type vortex is generated.
- b. The crossflow-type vortex is significantly more persistent than the pair of counter-rotating vortices originated at symmetrical roughness elements, at same height and  $Re_{kk}$ .
- c. Accordingly, a stronger amplification of forced disturbances is found — A new type of roughness-induced crossflow-type transition mechanism was observed for the blunt-body configuration.
- d. Comparison with experiments: difficult (no experiments available for only a “patch” of distributed roughness), but there is an ongoing cooperation with TU Braunschweig, Germany.

<sup>2</sup> Di Giovanni & Stemmer: “Crossflow-type breakdown induced by distributed roughness in the boundary layer of a hypersonic capsule configuration”, *J. Fluid Mechanics*, 2018 (accepted)

## I. Wind-tunnel conditions ( $M = 5.9$ )

Spanwise periodic roughness elements

Random distributed roughness

Base Flow

Stability Analysis

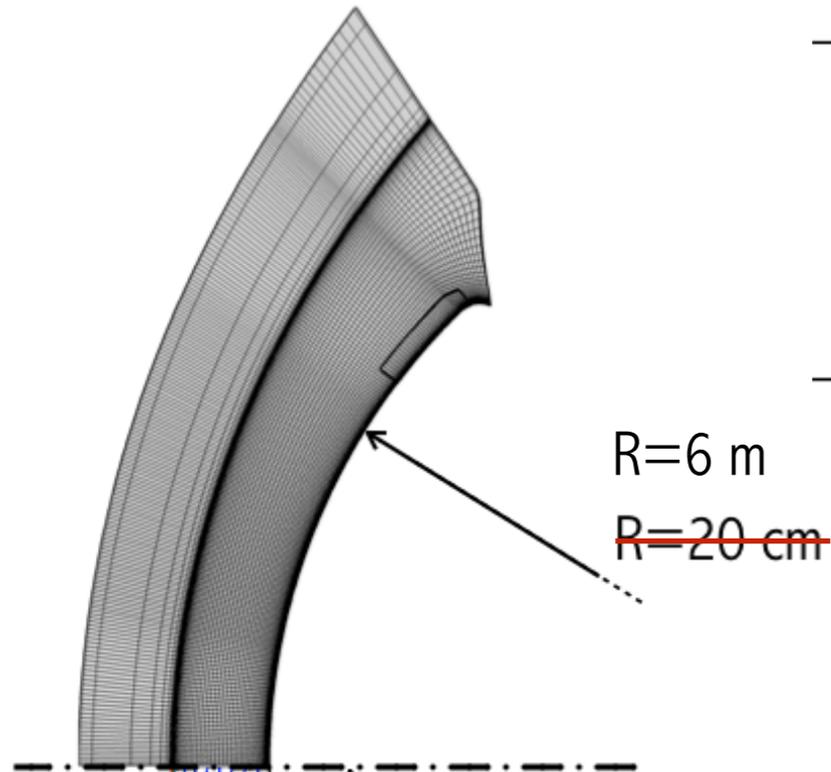
## II. Re-entry conditions ( $M = 20$ )

Random distributed roughness

Base Flow

Stability Analysis

# Simulations at Re-entry Conditions

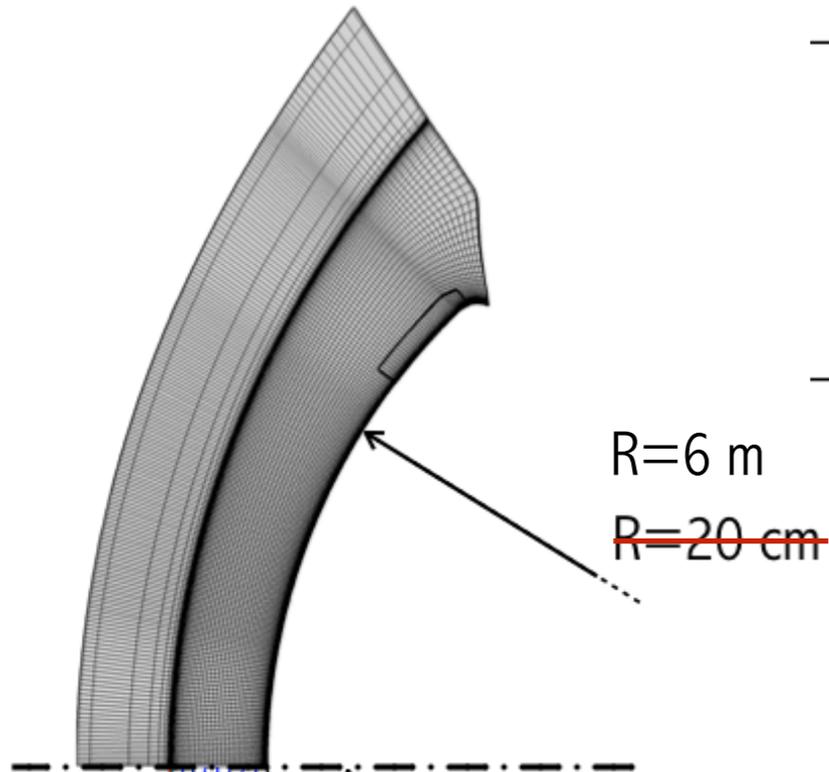


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Medium	$M$	$T_\infty$ [K]	$T_w$ [K]	$Re_\infty$ [1/m]	$R$ [m]
Air	20	253	1800	$2 \cdot 10^6$	6

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TABLE 2. Simulation parameters - re-entry conditions




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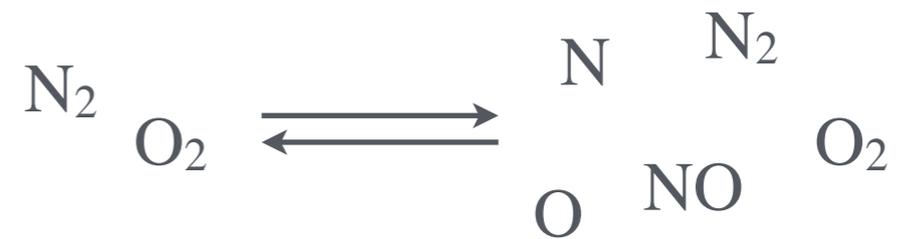
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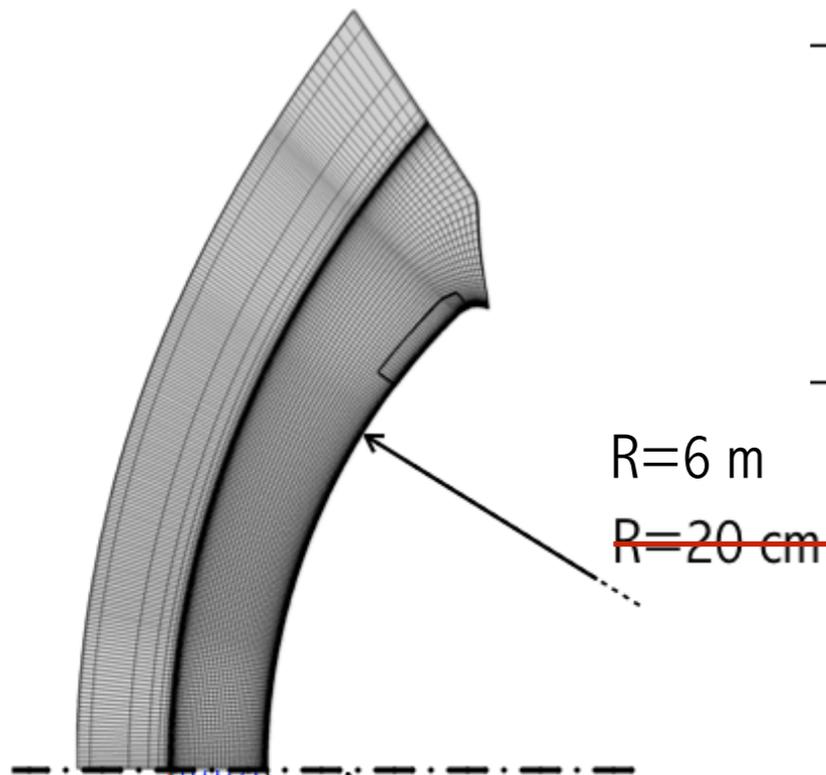
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**Different simulations are run with 3 different gas models:**

1. gas in chemical equilibrium (CEQ)  
( $T > 2000$  K)






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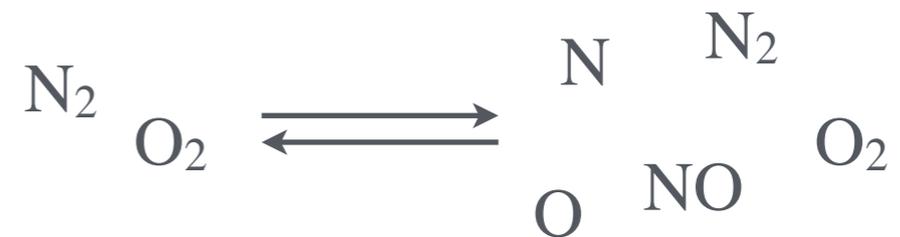
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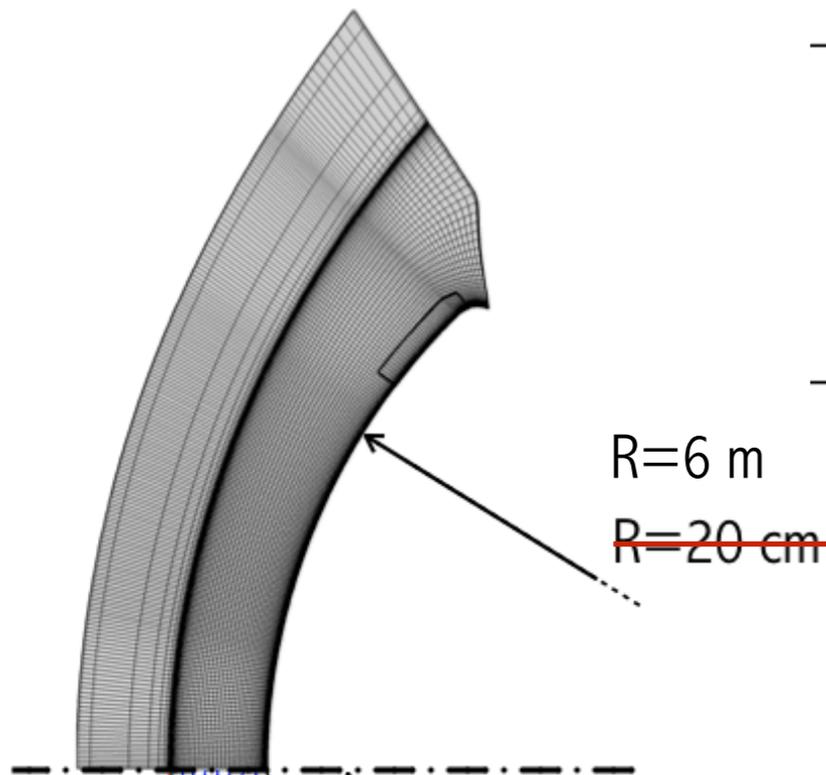
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2. gas in chemical NON-equilibrium (CNEQ)  
(timescale of reactions  $>$  timescale of convection)




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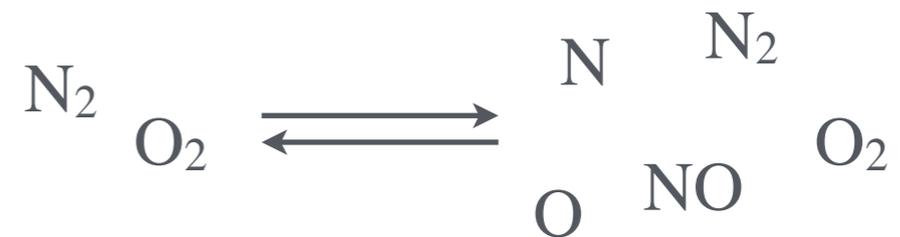
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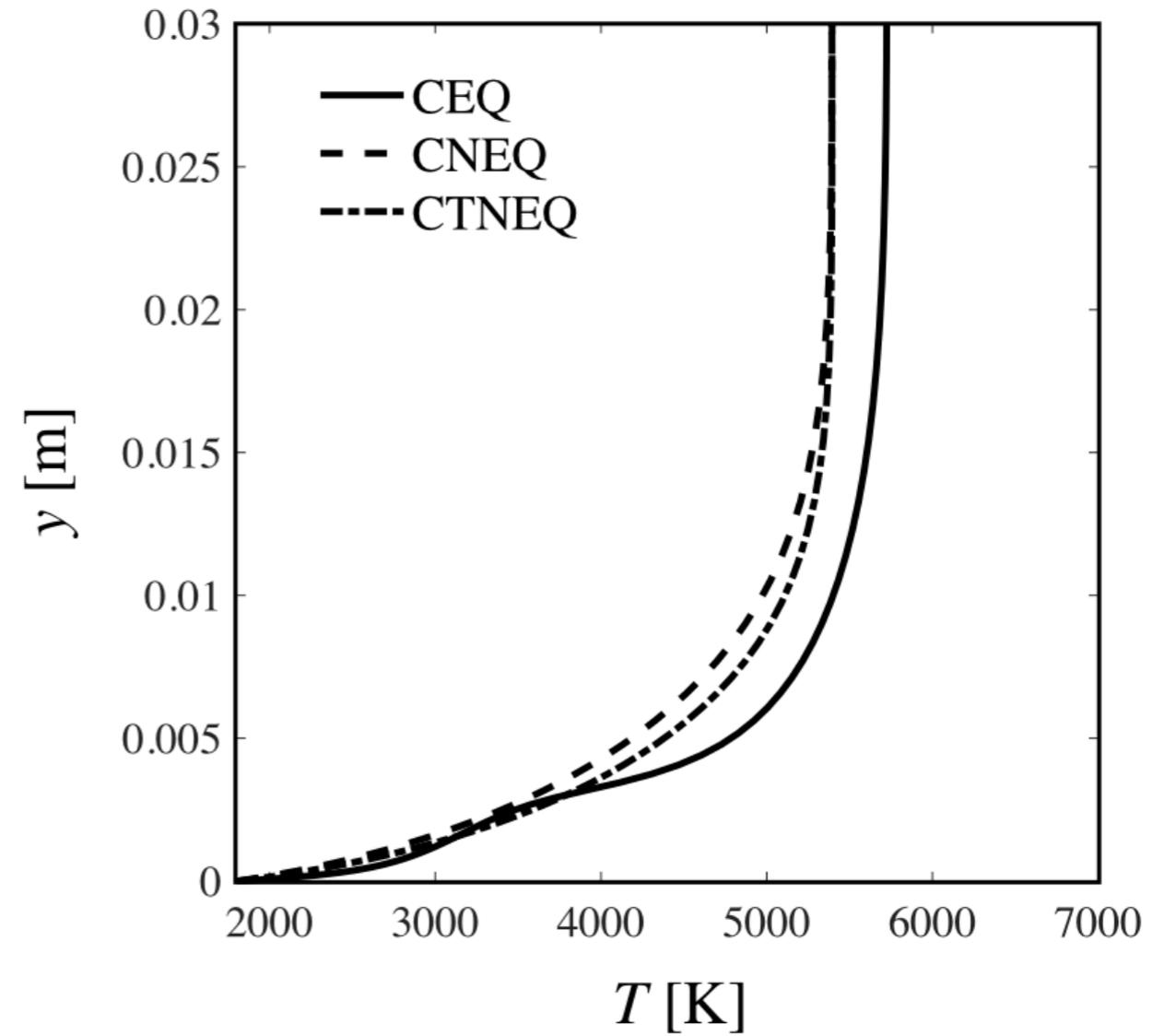
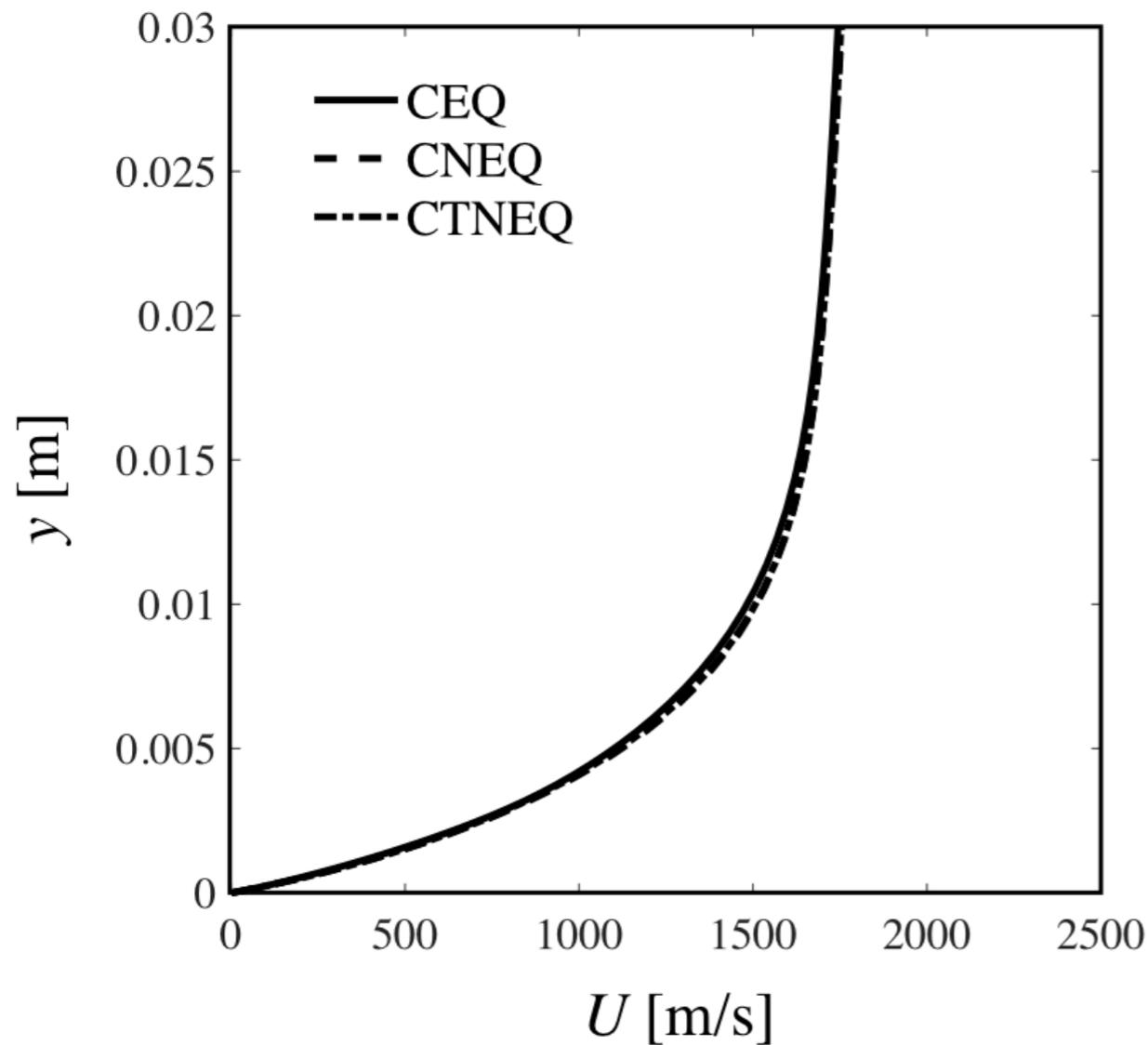
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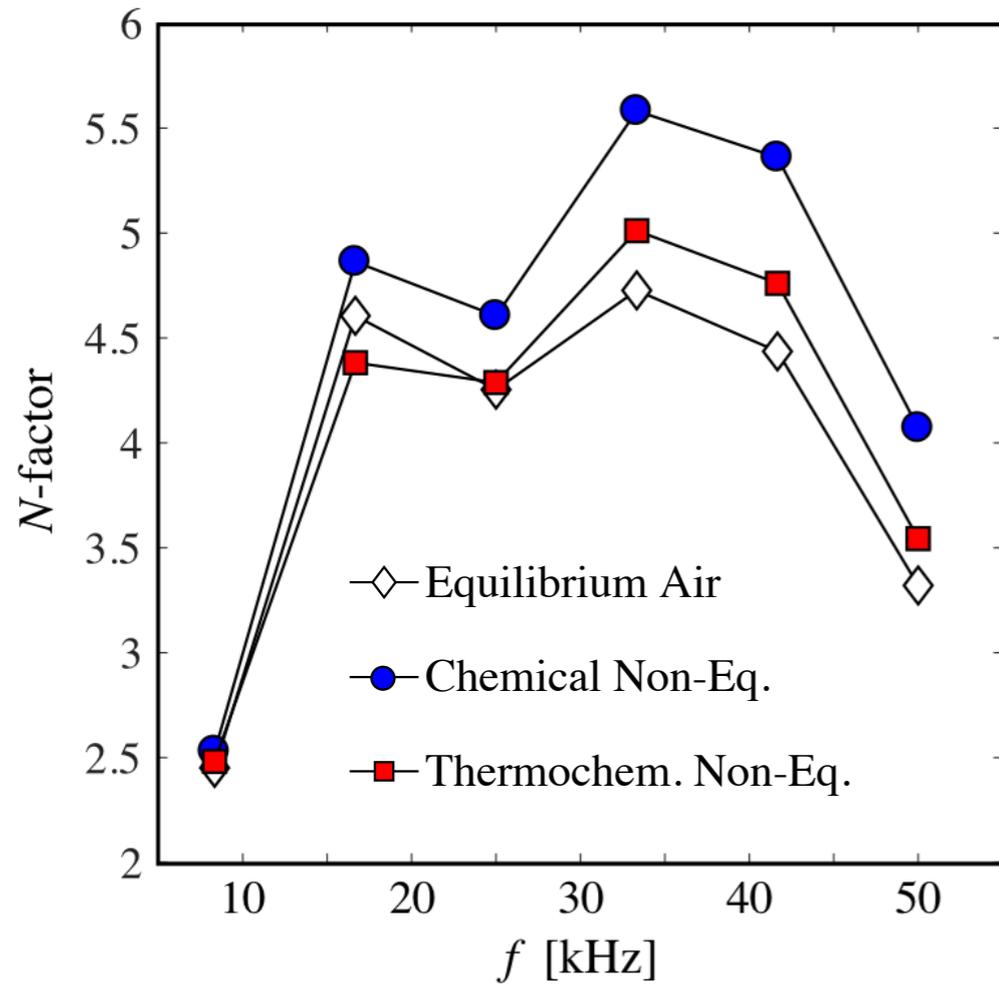
3. gas in thermal & chemical NON-equilibrium (CTNEQ)  
(timescale of vibration-energy change  $>$  timescale of convection)

# Effect of the Gas Modeling on the Boundary-Layer Profiles



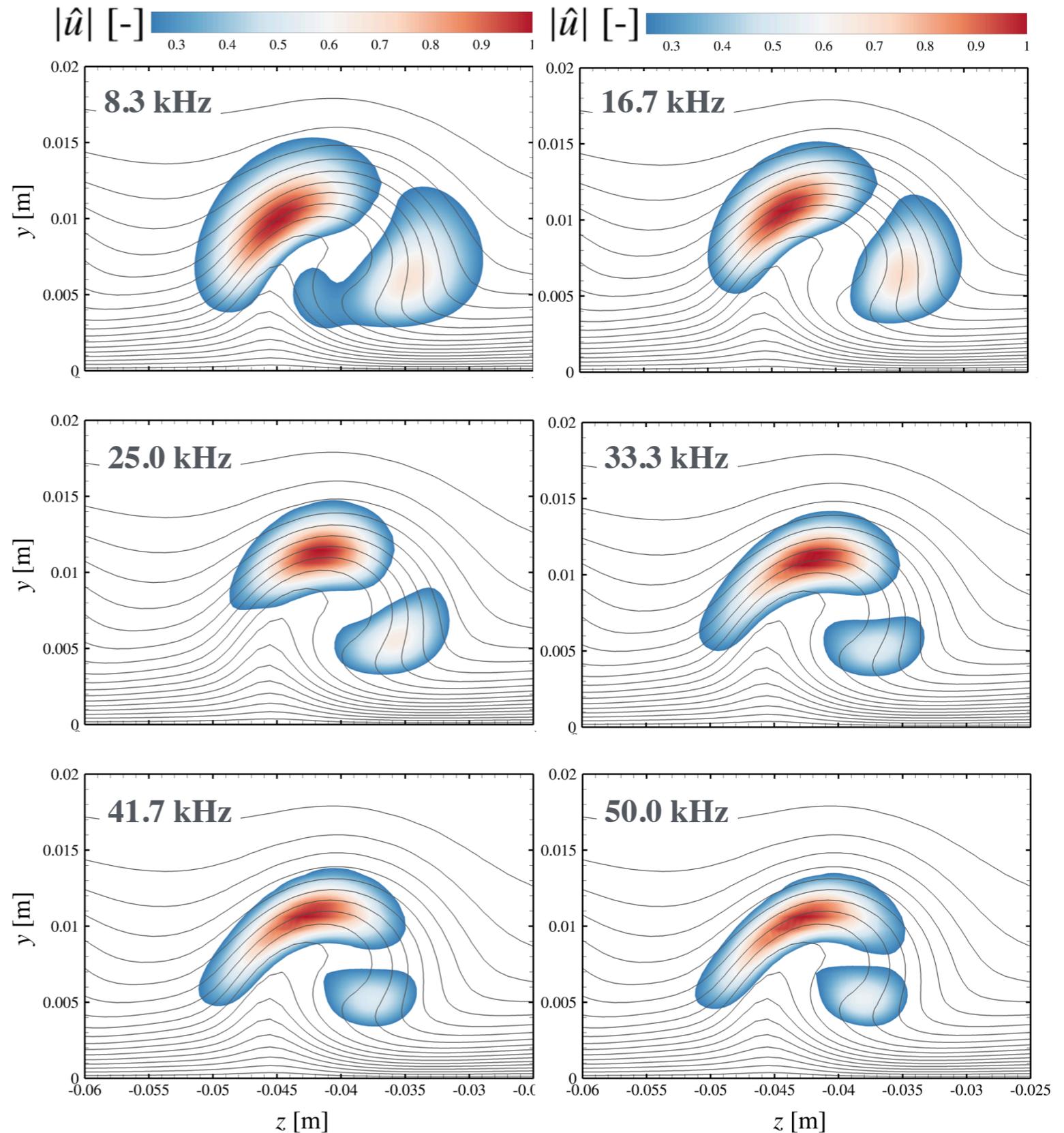
Velocity (left) and temperature (right) profiles at the roughness position for different gas models

# Modes of Instability



$$N = \int_{x_0}^{x_1} \sigma dx$$

$\sigma$  : Disturbance growth rate



# Investigations under Re-entry Conditions: Summary<sup>3</sup>

- a. Velocity profiles are not significantly affected by inclusion of *non*-equilibrium
- b.  $Re_{kk}$  in case of *non*-equilibrium becomes larger than the one in case of equilibrium for sufficiently high roughness
- c. Inclusion of chemical *non*-equilibrium has destabilizing effect
- d.  $y$ -mode at low frequencies;  $z$ -mode at high frequencies,
- f.  $y$ -mode more unstable (in the range of frequencies considered here)

<sup>3</sup> Di Giovanni & Stemmer: “Direct Numerical Simulations of roughness-induced transition in the boundary layer of a hypersonic spherical forebody under consideration of high-temperature gas effects”, AIAA 2018-4046 (2018)

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- d. *y*-mode at low frequencies; *z*-mode at high frequencies,
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## Current investigations

- a. Transition scenario with high-temperature gas effects
- b. Investigations on more distributed-roughness geometries

<sup>3</sup> Di Giovanni & Stemmer: “Direct Numerical Simulations of roughness-induced transition in the boundary layer of a hypersonic spherical forebody under consideration of high-temperature gas effects”, AIAA 2018-4046 (2018)